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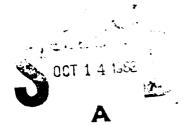


VERTICAL IMPACT TESTS OF A MODIFIED F/FB-111 CREW SEAT TO EVALUATE HEADREST POSITION AND RESTRAINT CONFIGURATION EFFECTS

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AUGUST 1982



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The voluntary informed consent of the subjects used in this research was obtained as required by Air Force Regulation 169-3.

This report has been reviewed by the Office of Public Affairs (PA) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.

FOR THE COMMANDER

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Director

Biodynamics and Bioengineering Division

Air Force Aerospace Medical Research Laboratory

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system or a conventional double shoulder strap - lap belt restraint harness and

Block 20 (continued).

were exposed to comparable impacts in different upper extremity bracing conditions and at different fore-aft headrest adjustments. Measured data included seat acceleration and velocity, head and chest translational acceleration components, tri-axial forces acting on the seat and footrest, forces acting in the restraint harness attachments, and displacements of various body segments. Parametric analysis of the test results was conducted using the Wilcoxon pairedreplicate rank test. With the headrest 2 1/4 inches forward of the plane of the seat back, there was increased forward and downward head rotation compared to the headrest 1 inch aft of the seat back plane. With the headrest 1 inch aft of the plane of the seat back, there was increased forward-translation of the head compared to the headrest 2 1/4 inches forward of the seat back plane. Subjects utilizing the hands-on-knees bracing position were found to carry a greater proportion of the load through the extremities to the footrest, thereby unloading the vertebral column, than subjects using the hands-in-lap position. Finally, the proposed, modified F/FB-111 crew seat and restraint system was found to react a greater proportion of the impact response through the harness compared to the conventional double shoulder strap - lap belt configuration. Additional impact tests with human volunteer subjects exploring fore-aft headrest adjustments between the extremes investigated in this study may be useful. The findings of the restraint harness configuration comparison may be clarified by additional vertical impact tests of the conventional harness with an added crotch strap.

PREFACE

This report was prepared by the Biomechanical Protection Branch, Biodynamics and Bioengineering Division of the Air Force Aerospace Medical Research Laboratory. The impact facilities and data collection equipment were operated by the Scientific Services Division of the Dynalectron Corporation under Air Force Contract F33615-79-C-0523. Mr. Harold F. Boedeker was the Engineering Supervisor for the Dynalectron Corporation.

The test fixture used during the experimental phase of the effort was designed and built by General Dynamics, Fort Worth Division. Photographic support was provided by the 4950th Test Wing, Technical Photographic Division. Special acknowledgement is given to Mr. Paul Creiger for operation of the high-speed motion picture cameras and to the many personnel who provided still photography coverage.

Anthropometric measurements of the test subjects were collected by Mr. Charles E. Clauser, Dr. Kenneth W. Kennedy, and Lt Col Maureen Lofberg of the Workload and Ergonomics Branch, Human Engineering Division of the Air Force Aerospace Medical Research Laboratory.

The authors wish to express their gratitude to the personnel of the Biomechanical Protection Branch who participated in the planning, preparation, and performance of the research program and in the preparation of this report. Special commendation is also given to the Air Force officers and airmen who volunteered to participate in the impact tests. The devotion, skill, and professionalism of the entire team of government and contractor personnel were vital to the successful and safe accomplishment of this evaluation.

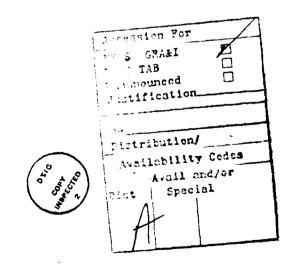


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SECTION 1

INTRODUCTION

A. BACKGROUND

A review of the operational F/FB-111 ejection data by Kazarian (1977) indicated that the vertebral fracture rate among survivors was 40.3% (25 of 62) for the period October 1967 to June 1977. The majority of these injuries was attributed to the retraction phase of the escape sequence. Twenty-nine percent (18 of 62) of the survivors were believed to have incurred hyperextension or combined hyperextension-hyperflexion vertebral fractures (Kazarian et al., 1979). Furthermore, the potential for negative shoulder strap angles (with respect to the reference aircraft waterline) was implicated as the cause of these hyperextension injuries. It was suggested that elevation of the inertia reel and reflection strap anchor points of the F/FB-111 shoulder harness would alleviate the hyperextension injuries presumed to occur during retraction and the smaller number of hyperflexion injuries presumed to occur during landing impact.

In order to reduce this relatively high vertebral fracture rate, a program to develop appropriate modifications to the F/FB-111 crew seat and restraint system was undertaken by the Life Support System Program Office of the Aeronautical Systems Division (ASD/AES). This redesign effort, based on the aforementioned injury mechanism assessment by Kazarian, had the following objectives: (1) eliminate the downward component of vertebral loading caused by the shoulder straps during retraction, (2) reduce the forward and downward rotation of shoulders and back on landing impact, and (3) extend the seat back to provide upper back support during powered inertia reel retraction. Following a feasibility study exploring possible approaches to improve the crew seat and restraint system, General Dynamics Corporation proposed hardware modifications to achieve the above redesign objectives. After the prototype modified system was fabricated, the Air Force Aerospace Medical Research Laboratory (AFAMRL) began an extensive demonstration test program with human subjects to evaluate the system. The objectives of this research program were to (1) assess the adequacy of the restraint as an impact protection device, (2) quantify the shoulder harness geometry for a range of subject anthropometry, and (3) uncover any areas of performance degradation.

This evaluation revealed a number of shortcomings in the proposed modification. The anthropometric study revealed that negative shoulder strap angles were still possible for some subjects in some seat configurations, despite the higher locations of the tie-down points of the shoulder straps in the modified system. As a result of the elevation of these anchor points, it was necessary to remove 2.34 inches from the lower aspect of the headrest to assure adequate clearance for the shoulder straps. An anthropometric study also indicated that this modified headrest significantly degraded head support. It was estimated that 38% of flyers would not have even marginal head support with the seat back at the 90° position, 75% would not have adequate support with the seat back reclined to 103° , and 94% would not have adequate support with the seat back reclined to 110° . Marginal head support requires that the helmet contact point be 1 inch above the lower aspect of the headrest. Data obtained from the impact test program established the modification as an adequate impact protection device, but also suggested that lateral and vertical impact protection

performance of the system had been degraded by the modification (Brinkley \underline{et} al., 1981).

This proposed, modified F/FB-111 restraint system, like the operational harness, incorporates a number of features which depart from standard USAF design practice. A number of these features permit the imposition of adverse spinal loading on the crewmember. For example, a maladjustment of the shoulder harness yoke assembly may limit torso erection and produce downward spinal loads during retraction of the shoulder straps by the powered inertia reel. Alternate, plausible mechanisms of vertebral fracture resulting from these design deviations, which were not addressed by the proposed modification, were clearly delineated during the original demonstration test program. At the same time, a re-evaluation of the operational ejection data (Hearon et al., 1981, 1982) failed to implicate negative shoulder strap angles as the vertebral fracture etiology and concluded that axial compression and flexion of the vertebral column on landing impact of the crew module was often the mechanism of vertebral fracture. The relative clinical benignity of the majority of these fractures, expressed in terms of the number of days the involved crewmembers were grounded or hospitalized, was also demonstrated. On the basis of the aforementioned shortcomings of the proposed modification, reassessment of vertebral fracture injury mechanisms, and the results of a subsequent human vertical impact test program in which the operational F/FB-111 crew seat and restraint system was compared to the proposed modification (Hearon et al., 1982b), the proposed modification was rejected.

The present study was conducted to clarify the test results obtained in the original demonstration test program of the proposed modification (Brinkley et al., 1981). For example, the initial vertical test series revealed statistically significant increases in nead acceleration in some test configurations which may have been attributed either to the crew seat headrest position or to the restraint configuration. Other findings may have been influenced by the use of upper extremity bracing (hands-on-knees) by the subjects in the initial test program. Therefore, a controlled experiment to assess the influence of headrest position, upper extremity bracing, and restraint harness configuration was designed.

The fore-aft headrest position in the F/FB-111 is adjustable in 1 inch increments, over a longitudinal distance of 6 inches, as shown in Figure 1. The most forward location of the headrest is such that the helmet-headrest contact plane is 2 1/4 inches forward of the seat back plane. This headrest position was dictated by a United States Navy requirement to provide adequate head support to maintain over-the-nose vision during carrier launches. The current USAF design specification for capsule emergency escape systems (MIL-C-25969B, 1970) indicates that the headrest should be located 1 inch aft of the plane of the seat back. The adjustable F/FB-111 headrest, therefore, represents a significant departure from standard design practice.

With the headrest in the full forward location, the seat occupant's head and neck are adversely flexed forward in the so-called "turkey vulture" position. (See Figure 2.) This preflexed position of the head and neck creates an additional moment acting on the vertebral column and causing a downward and forward rotation of the head and upper torso during vertical impacts, such as those experienced during ejection and landing impact of the crew module. In the initial demonstration test program of the proposed, modified F/FB-111 crew seat and

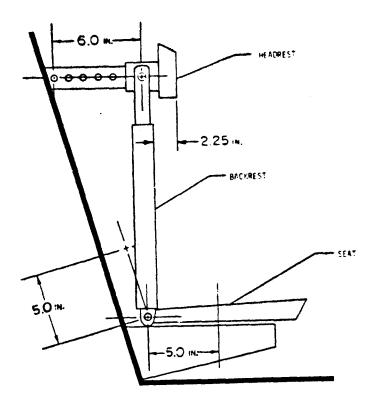


Figure 1. F/FB-111 Crew Seat Geometry with Headrest Forward. (Seat and seat back cushions are not shown.)

restraint system, forward head acceleration experienced during vertical impact tests increased as the seat back angle was erected from a reclined to an upright position (90° to the aircraft waterline). This forward head acceleration may have been less in the 90° seat back condition, if the headrest did not preposition the head so far forward of the plane of the seat back. The fundamental principles of impact protection dictate that head displacements and accelerations be minimized during whole body impact acceleration to minimize the risk of injury.

The earliest recommendation on headrest location for an ejection seat appears to be in a 1946 document which summarized the state-of-the-art of escape biotechnology at that time. The memorandum (Cofer et al., 1946) indicated that the headrest should be located so that the head will not move below it when the body moves downward relative to the seat during ejection. Furthermore, it was recommended that the headrest be adjustable in the fore-aft direction so that the head may be positioned with its center of gravity over or slightly forward of the longitudinal axis of the cervical vertebrae. This recommendation was based on the presumption that a more severe injury would be incurred by backward rotation of the head (hyperextension of the cervical spine) then by forward rotation of the head (hyperflexion). Later, human ejection tower tests using a T-2 catapult (Ames and Savely, 1948) were conducted to examine impact response in various headrest positions. In these tests, the fore-aft location of the headrest was varied over a range of 2 inches from 1/4 inch to 2 1/4 inches aft

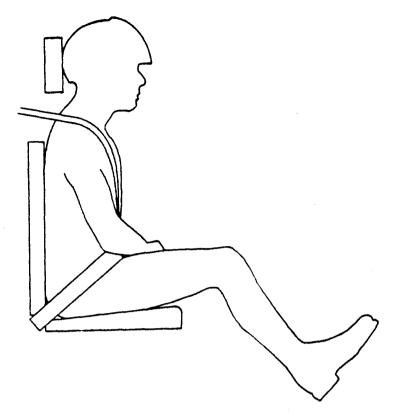


Figure 2. "Turkey Vulture" Position. The cervical spine is flexed due to the forward location of the headrest.

of the plane of the seat back. The study noted that hyperflexion occurred if the headrest was positioned too far forward and that hyperextension occurred if the headrest was positioned too far aft. It was stated that the risk of neck injury (muscle strain) during ejection could be minimized by the proper fore-aft position of the headrest. This position was noted to vary from subject to subject. In order to achieve the proper headrest adjustment, the subject's earlobe was aligned directly over the center of his shoulder.

The initial Aerospace Medical Research Laboratory recommendation regarding placement of ejection seat headrests was that the headrest should be adjustable, from 0 to 3 inches aft of the plane of the seat back, or fixed, 1 3/4 inches aft of the seat back plane. Finally, the USAF design specification adopted was that the plane of the headrest would be 1 inch aft of the plane of the seat back. This specification is the same for open ejection seat aircraft (MIL-S-9479B, 1971) as it is for encapsulated escape systems. However, of the escape systems currently used in the Air Force, the Martin-Baker, the ESCAPAC, the ACES II, and the F/FB-111 crew seat and restraint system all deviate from this design specification.

B. PROGRAM OBJECTIVES

The primary objectives of this research effort were to evaluate the effects of changes in (1) the headrest position, (2) upper extremity bracing, and (3) restraint harness configuration on human response to vertical impact. Specifically, the extreme forward adjustment position of the F/FB-111 headrest was compared to the more conventional aft position of the headrest. The hands-on-knees bracing technique, utilized during the initial demonstration test program of the F/FB-111 crew seat and restraint system, was compared to a position in which the hands were relaxed in the lap to preclude upper extremity bracing. Also, the proposed, modified F/FB-111 harness was compared to the more conventional double shoulder strap - lap belt configuration. The secondary objective of this test program was to provide data for ongoing research efforts to develop mathematical models to predict human impact response.

This report (1) describes the impact tests accomplished to meet the above program objectives, (2) presents analysis and interpretation of the collected data, (3) summarizes the results of the evaluation, and (4) provides recommendations which are supported by the test results.

SECTION 2

TECHNICAL APPROACH

A. EXPERIMENTAL DESIGN

The following null hypotheses were evaluated during this test program. First, human response to vertical impact with the headrest forward of the plane of the seat back is not significantly different from such response with the headrest aft of the plane of the seat back. Second, human response to vertical impact with subjects utilizing a hands-on-knees bracing technique is not significantly different from such response in the absence of upper extremity bracing. Third, human response to vertical impact in a proposed, modified F/FB-111 crew seat and restraint system is not significantly different from such response in a conventional double shoulder strap - iap belt restraint configuration.

TABLE 1. EXPERIMENTAL MATRIX

		HEADREST POSITION		
HARNESS TYPE	SUBJECT BRACING	25" FORWARD	1" AFT	
Modified F-111	Hands-On-Knees	А	В	
Modified F-111	Hands-In-Lap	C	D	
Conventional	Hands-In-Lap	ΕΕ	F	

The design matrix for this factorial experiment is shown in Table 1. All tests in the matrix were conducted in the F/FB-111 crew seat with the plane of the seat back parallel to the impact vector. This seat configuration was achieved by adjusting the headrest full forward and the seat pan full aft, as shown in Figure 1. Subjects were tested at the same seat elevation for each test in the experimental matrix. The full down seat position was selected for evaluation. However, those subjects with relatively small sitting heights did not have adequate helmet support in the full down seat position. Adequate helmet support was assumed if the approximate Frankfort horizontal plane (defined by the lowest points in the inferior orbital rims and the mid-point of the line connecting the highest points in the margin of the auditory meati) of the subject was in contact with the headrest. For those subjects, the seat was elevated until minimum helmet support, according to the above definition, was provided.

The above test conditions were selected for investigation based on the need to clarify previous results of tests conducted under similar conditions (Brinkley et al., 1981). For example, in the previous demonstration test program, forward head accelerations and vertical seat loads were significantly higher with the seat back angle at 90° than with the seat back angle at 103° or 110° . Selecting the 90° seat back angle condition for evaluation in this test program, therefore, allowed greater observability of the effects of variations in restraint configuration and subject bracing. Furthermore, controlling these seat adjustment parameters permitted a wider comparability among cells in the experimental matrix.

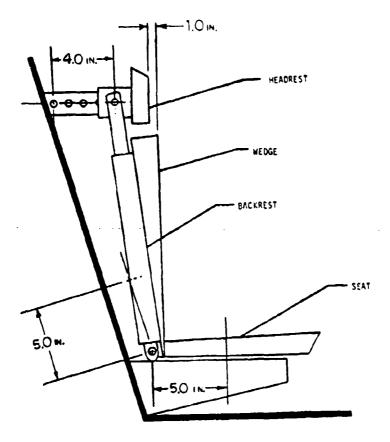


Figure 3. F/FB-111 Crew Seat Geometry with Headrest Aft (Seat and seat back cushions are not shown.)

As shown in Table 1, tests in cells A, C, and E of the experimental matrix were conducted with the headrest contact plane 2 1/4 inches forward of the seat back plane. Tests in cells B, D, and F of the experimental matrix were conducted with the headrest contact plane 1 inch aft of the seat back plane. The latter test conditions were achieved by placing a wooden wedge between the actual seat back and the F/FB-111 seat back cushion, thereby moving the effective seat back plane forward of the headrest. Thus, comparisons A-B, C-D, and E-F, revealed the differences in impact response due to variation in fore-aft headrest position. (See and compare Figures 1 and 3.)

For all tests in this series, subjects were instructed to brace their helmeted head against the headrest and their feet against the rudder pedals of the test fixture. For tests in cells A and B only, subjects were also instructed to brace their hands against their anterior thighs or knees, as had been done in the previous demonstration tests of the proposed, modified F/FB-111 crew seat and restraint system. However, for tests in cells C, D, E, and F, subjects were instructed to relax their upper extremities and to fold their hands loosely in their laps in order to preclude upper extremity bracing. Therefore, comparisons A-C and B-D revealed the differences in impact response due to this variation in subject bracing. (See and compare Figures 4 and 5.)



Figure 4. Hands-On-Knees Position

In cells A, B, C, and D of the experimental matrix, subjects were restrained by a proposed, modified F/FB-111 harness. In cells E and D of the experimental matrix, subjects were restrained by a conventional double shoulder strap - lap belt harness configuration. Therefore, comparisons C-E and D-F revealed the differences in impact response due to the change in harness configuration. (See and compare Figures 6 and 7.)

The four experimental level tests in the F/FB-111 harness were randomized for each subject. After these tests were completed, subjects were tested in condition E and then condition F of the experimental matrix. It was not practical to randomize the latter two test conditions with the other test conditions due to the time required to change harnesses on the test fixture.

All subjects participated in orientation exposures in cells C and D of the test matrix. The orientation exposure level was 8 G peak carriage acceleration with 23 ft/sec carriage velocity change. The experimental test level selected was 10 G peak carriage acceleration with 26 ft/sec carriage velocity change. These exposures are considered to be subinjury impact acceleration levels. They were chosen in order to minimize the potential for injury to the subjects. On the basis of prior experience, the risk of subject injury at the 10 G experimental level was acceptably low. At the same time, the forces acting on the subject at this exposure level are generally sufficient to overwhelm the variable forces



Figure 5. Hands-In-Lap Position

created by voluntary neck and torso muscle contraction, thereby producing a response suitable for comparative parametric analysis.

The sample of subjects selected to participate in this test program is comparable to a flying population in terms of age, sex, and anthropometry. Fifteen males and one female subject participated in this test program. The medical screening of all subjects prior to participation is more highly selective than a routine USAF Flying Class I evaluation. This results in a panel of volunteers who are expected to be supranormal in terms of impact injury tolerance (Hearon and Raddin, 1981). This difference in the populations of interest has a negligible influence on the significance of results of tests such as these, since all tests were conducted below the anticipated injury threshold, even for a normal population. Such a conservative approach to subject screening is necessary to assure subject safety.

Impact tests were conducted in all cells of the experimental matrix using an anthropomorphic dummy prior to initiating tests with volunteer subjects. As an additional safety precaution, a dummy test was performed each day prior to testing with human subjects. The controlled variables during these experiments were the carriage drop height, the seat horizontal and vertical adjustment, the headrest adjustment, the upper extremity bracing technique, the restraint



Figure 6. Proposed, Modified F/FB-111 Restraint Harness

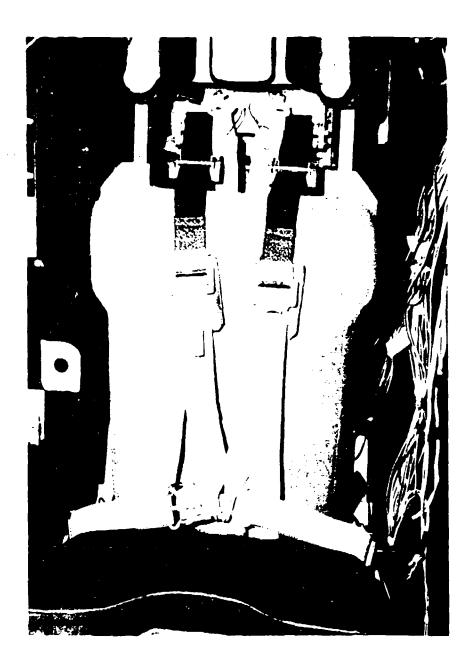


Figure 7. Conventional Double Shoulder Strap - Lap Belt Configuration

harness, and the subject population. The carriage drop height was 8.5 feet for the 8 G orientation tests and 11.0 feet for the 10 G experimental level exposures.

The observable variables which were measured during these experiments included the restraint harness geometry (e.g., shoulder strap angles), the restraint harness static preloads, the restraint harness loads during impact (e.g., shoulder strap and lap belt loads), the forces (horizontal, lateral, and vertical) in the seat and footrest, the triaxial translational acceleration components measured at the seat and at the subject's head and chest, and the displacements (with respect to the seat) of photometric targets fixed to the subject. The potential measurement error of accelerometers, load cells, strain gages, and other devices utilized to make these measurements is described in Appendix A.

Significant unobservable variables during these experiments included the motion of each vertebral body and the force distribution along the vertebral column during the impact event.

B. EVALUATION CRITERIA

The electronic measurements obtained during these experiments included the tension-time histories of the various restraint harness straps measured at their attachment points, the force-time histories of the loads measured at the seat and footrest, and the acceleration-time histories of the subject's head and chest and of the seat and drop carriage as well. The accelerometer arrays attached to the subjects were, in general, rotating measurement coordinate frames which measured translational acceleration components summed with translational components resulting from angular motions. One implication of this measurement technique is that, as the head rotated downward and forward, vertical acceleration of the head with respect to the laboratory reference frame partially transitioned from a Z axis (vertical) to an X axis (fore-aft) measured acceleration with respect to the head. This situation is illustrated in Fig. 8. Another implication is that separation of translational accelerations of the effective center of gravity and translational acceleration components resulting from rotational motions cannot be achieved with the three orthogonal linear accelerometers utilized in these experiments. The relevant equations have been summarized elsewhere (Simons et al., 1979). For the purposes of this test program, it was adequate to measure the mixed translational acceleration data and record rotational motion photometrically.

Evaluation of the entire measured acceleration-time histories of chest and head was accomplished by calculating Severity Indices (Gadd, 1966). These single parameters, which were derived by a weighted integral of the acceleration-time function taken over the interval of the impact (SI = $\int a^n(t)dt$, where n = 2.5), were used to compare the severities of impact responses. No exposure limit values were assigned to the chest or head acceleration Severity Indices. Instead, they were used only in a relative sense for purposes of comparison.

The Wilcoxon paired-replicate rank test (Wilcoxon & Wilcox, 1964) was the statistical technique selected to compare the peak values of specific measured parameters and to establish the statistical significance of observed trends in the data. Experimentally-measured parameters for each subject were arithmetically compared with the same parameters measured for the same subject in a

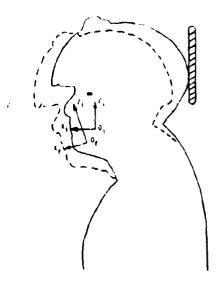


Figure 8. Rotation of the Accelerometer Array at the Head During Vertical Impact

different (but comparable) test condition, thereby establishing pair differences. When a sufficient number of pair differences for a specific parameter changed in the same direction for a variety of subjects, a trend was established as statistically significant by the Wilcoxon technique. The 90% confidence level was defined as the level of statistical significance for rejection of the null hypothesis, assuming a two-tailed test.

The advantages of employing this statistical technique are particularly noteworthy in these experiments. The technique is comparative and, therefore, is readily applied to the comparison of different headrest positions, upper extremity bracing techniques, or restraint harness configurations. Also, the method establishes each subject as his own control, thereby reducing the effects of biological variability on the data. In addition, a relatively small number of paired-replicates (5) is the minimum number required to permit a valid conclusion at the chosen significance level.

The disadvantages of the Wilcoxon technique, however, must also be considered. Although the trend (direction) of a statistically significant difference in a given parameter is indicated, the magnitude of that difference is not quantified by the technique. (The difference between the means of the two sets of parameters being compared may be easily computed, however.) The method is also less sensitive than, for example, the analysis of variance. As in any statistical technique, statistical significance can be computed, but practical significance must be judged.

Statistically significant trends in test parameters between two comparable test conditions were critical in this evaluation. Generally, trends in specific parameters differ in practical importance. In this test program, for example, there was limited interest in the loads reacted into the lap belt, since all tests were conducted in the Z axis with an unreclined seat back, thereby minimizing variation in lap belt reaction loads. The more crucial considerations

were the trends in the experimentally-measured seat reaction loads and the head and chest accelerations. At this time, the loads reacted at the seat are the best indirect measurement of the magnitude of vertebral column loading during impact.

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In the final analysis, the overall distribution of statistically significant trends in all test parameters being compared generally assumes greater importance than the trend of any single parameter. At times, a "beneficial" trend in one parameter may be accompanied by a "detrimental" trend in another. In this circumstance, a careful evaluation of the "trade-offs" among parameters is necessary, in order to accurately assess which test configuration is "best" or perhaps which is the lesser of two evils. It is conceivable that, in some circumstances, such a determination may not be possible.

For ethical and moral reasons, it is not possible to design and conduct impact experiments in the laboratory with human subjects at operational exposure levels where there is a known probability of injury. These tests, therefore, were performed at subinjury impact levels which have been demonstrated to be well within human tolerance and where the risk of injury is acceptably low. However, the levels were sufficiently high to overcome voluntary muscle resistance and approach the operational range. Increasing the magnitude of the impact accelerations could be expected to lead to increases in response until a nonlinearity occurs in the form of injury. The statistically significant trends reported herein for this experimental level cannot be extrapolated to operational levels for the purpose of predicting injury rates. However, the trends discovered at this experimental level should be valid with increasing levels of impact until the non-linearities associated with injury are encountered.

SECTION 3

TEST EQUIPMENT, METHODS, AND FACILITIES

A. VERTICAL DECELERATION TOWER

The AFAMRL Vertical Deceleration Tower (VDT), shown in Figure 9, was used for this impact test series. This facility consists of a 60 ft vertical steel tower, which supports a guide rail system, an impact carriage, a hydraulic deceleration device, and a test control and safety system. The impact carriage used to carry the test specimen can be elevated to a maximum height of 42 ft prior to release. After release, the carriage falls until a plunger attached to the carriage enters a water-filled cylinder located at the base of the tower. The deceleration profile produced as the plunger displaces the water in the cylinder is a function of the free fall distance, the carriage and test specimen mass, the shape and size of the plunger, and the diameter of the cylinder orifice.

A typical acceleration-time history recorded on the impact carriage during this test program is shown in Figure 10. The 10 G test level mean peak carriage acceleration for the entire vertical test series was 10.5 G with an estimated standard deviation of 0.14.

B. CREW SEAT, RESTRAINT SYSTEMS, AND SEAT INSERT

The operational F/FB-111 restraint system, shown in Figure 11, consists of a lap belt, double shoulder strap, and crotch strap configuration. The harness is attached to the crew seat at five points and to the inertia reel at two points. The shoulder strap geometry is unique in that the straps originate from the inertia reel, pass through the rollers attached to the shoulder strap yoke, and are attached to the top of the back rest on the opposite side of the seat. The intent of this cross-over geometry is to provide sideward impact protection. The lap belt is attached to the seat structure at the seat reference axis (the intersection of the plane of the seat back and the seat pan). The crotch strap (also referred to as the anchor strap or negative G strap) is attached to the front of the seat pan. The shoulder straps are attached to the shoulder strap yoke below the rollers above the chest strap adjustment buckles. The lap belt, crotch strap, and lower portion of the shoulder straps (chest straps) are constructed of 1 3/4 inch wide Terylene webbing. The shoulder straps attached to the inertia reel are made of 1.3/4 inch wide polyester webbing (Type I, MIL-W-25361).

Under Contract No. F33657-78-C-0651 with the Life Support System Program Office, the General Dynamics Corporation redesigned the F/FB-111 crew seat and restraint system. The proposed redesign consisted of (1) rerouting the inertia reel straps to raise the shoulder strap tie-down point of the inertia reel, (2) moving the cross-over (or reflection) strap attachment points up to the headrest support frame, and (3) increasing the height of the backrest. These proposed modifications are shown in Figure 12. Rerouting the inertia straps was accomplished by two sets of rollers attached to the inertia reel assembly. These rollers increased by 1.9 inches the height of the points through which the retraction loads would be applied to the crewmember and through which a portion of the inertia loads of the crewmember would be carried during crew module



Figure 9. AFAMRL Vertical Deceleration Tower and F/FB-111 Test Fixture Viewed from Below.

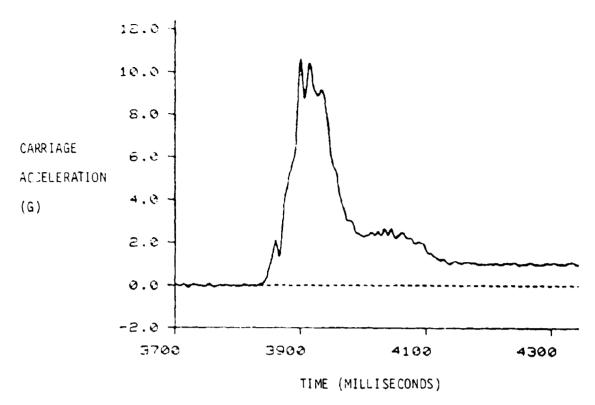


Figure 10. Typical Carriage Acceleration Profile at the Experimental (10 G) Test Level

acceleration in the escape sequence. The reflection strap attachments were mounted to anchor points at waterline 203.2 in the headrest support frame. These anchor points moved with the headrest during fore-aft adjustment. The height of the backrest was increased by 2 1/4 inches. A portion of this backrest extension on each side was recessed by 1 1/4 inches in order to provide clearance for the inertia reel straps when the seat was adjusted to its upper limit. For the same reason, 2.66 inches of the lower aspect of the headrest support surface was removed in the proposed modification. However, the restraint harness assembly itself was not changed in the proposed modification.

The other harness utilized in this test program was a standard USAF double shoulder strap - lap belt configuration (Figure 7). The shoulder straps were an adjustable Type MB-6 harness, constructed of 1 3/4 inches wide polyester Type I webbing, in accordance with specification MIL-H-5364D, 1972. In static tests, the webbing is capable of carrying an ultimate load of 3600 pounds. The lap belt was the HBU lap belt (without the automatic release buckle), constructed of 1 3/4 inches wide nylon webbing (Type XIII, MIL-W-4088H). The breaking strength of this material is 6500 lb.

Each restraint system was pretensioned prior to the impact experiment. The lap belt pretension was 20 ± 5 lb measured by strain gages mounted on the lap belt end attachment fittings. The total load acting on each shoulder strap was set at 14 ± 5 lb by measuring the loads at the end fittings of each reflection strap

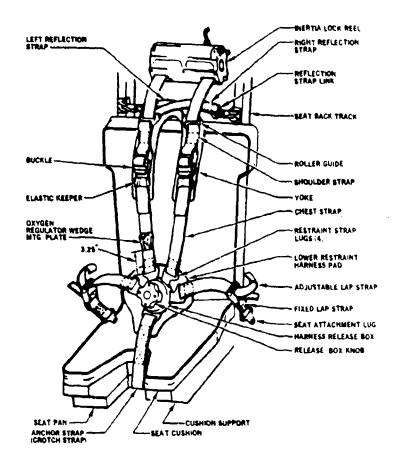


Figure 11. Operational F/FB-111 Restraint Harness

and using Lebow gages attached to the inertia reel straps. This preload procedure imposes a load on the subject which is lower than the maximum load (50 lb in each shoulder strap) expected during operational use of the F/FB-111 inertia reel. The conventional harness as well as the F/FB-111 harness was pretensioned in order to assure comparability of the pre-impact test conditions.

Previous tests of similar restraints in England (Reader, 1967) and at Holloman AFB (Zaborowski, 1965) resulted in subject complaints when preloads of 50 lb or greater per strap were imposed. In view of these reports, and since imposition of static preloads on the subject was required for relatively long periods of time (approximately 15 minutes) prior to the impact event, imposition of preloads of such magnitude was neither practical nor desirable. In addition, previous experience at AFAMRL has shown that significant variations in restraint performance do not occur unless the pretension is well below 20 lb. Therefore, the aforementioned pretensions were deemed adequate.

All tests in this program were conducted in a crew seat which was salvaged from an F-111 crew escape module. The seat was mounted to the vertical deceleration tower by a structure designed and fabricated by the General Dynamics Corporation. This test fixture, shown in Figure 13, supported the seat and the rudder pedal footrest. The seat was adjustable horizontally and vertically over 5 inches in 1 inch increments. The seat and rudder pedals were instrumented to measure the



Figure 12. Proposed Modifications to the F/FB-111 Restraint System

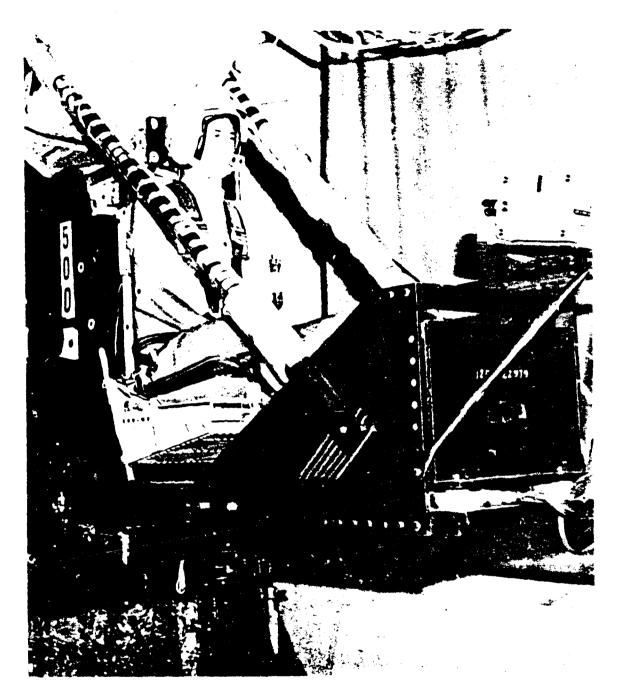


Figure 13. Test Fixture with Rudder Pedal Support Structure

loads reacted by the subject into these structures during the impact. The seat and test fixture are more completely described elsewhere (Brinkley et al., 1981).

The inertia reel was not used in this test program. It was replaced by a simple webbing clamp bar located at a position equivalent to the centerline of the actual reel.

The modified F/FB-111 headrest was used for all tests in this program. As previously noted, 2.66 inches of the lower aspect of the operational F/FB-111 headrest had been removed in the proposed modification. The headrest, which was adjustable over a horizontal distance of 6 inches in 1 inch increments, was moved to the full forward position to achieve the 90° seat back angle condition with the headrest 2 1/4 inches forward of the plane of the seat back. (The seat was adjusted to the full aft position. This configuration is shown in Figure 1.) To achieve the position with the headrest 1 inch aft of the plane of the seat back, the headrest was adjusted 2 inches aft and a seat insert was placed between the seat back and the seat back cushion. This wooden seat insert is shown in Figure 14. This 5.5° wedge was utilized to maintain a 90° seat back angle and the impact vector parallel to the plane of the effective seat back, as shown in Figure 3.

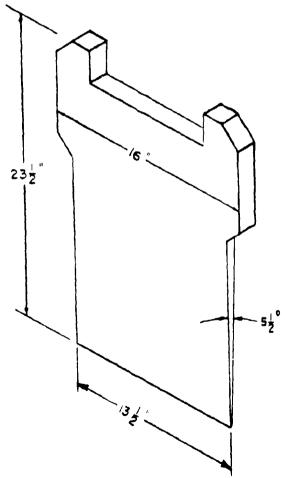


Figure 14. Seat Insert Used in the Headrest Aft Position

C. DATA ACQUISITION

Electronic data collected during the test program included impact carriage acceleration and velocity, test fixture loads and acceleration, subject head and chest acceleration, harness loads, and single-lead electrocardiograms. Detailed descriptions of the instrumentation, electronic data processing equipment, mounting procedures, and calibration techniques are provided in Appendix A. The following information summarizes the electronic instrumentation that was used to acquire the test data.

Carriage acceleration was measured using three miniature, piezoresistive accelerometers mounted to the structure of the VDT carriage. Vertical velocity was determined at the point of impact (the point where the carriage plunger contacted the water in the deceleration cylinder) by using a tachometer.

The test fixture was instrumented to measure the forces reacted into the seat, restraint, and footrest by the subject. Triaxial acceleration was measured on the seat structure to quantify the impact exposure. The seat structure included three load cells and three load links to measure the vertical and horizontal forces reacted through the structure. Forces were measured in the restraint system using strain gages bonded to the seat attachment hardware or Lebow belt load cells. Leg forces were measured by three triaxial load cells which were incorporated within the rudder pedal support structure.

Triaxial accelerometer arrays were used to measure acceleration on the head and chest of each subject. The chest accelerometer package was held tightly against the subject's sternum by a Velcro chest strap. The subject's head accelerometers were mounted on a dental bite block, which was held in the subject's mouth during the test. This technique has proven to be not only a safe means of providing intraoral/dental protection during impact, but also an effective way of minimizing movement of the accelerometer package relative to the subject's head during impact.

The electronic data obtained from the transducers described above were encoded into pulse code modulation digital format and then transmitted by telemetry to a word formatter. The word formatter reformatted the serial data into parallel data which was transmitted to a PDP 11/34 computer for recording and processing.

Photometric data were collected using two high-speed (500 frames per second), 16 mm Milliken cameras mounted on the impact carriage. One camera was mounted to the right of the subject perpendicular to the sagittal plane. The second camera was mounted above the footrest to provide a frontal view of the subject. The movements of the subject's helmet, head, shoulders, arms, and the chest accelerometer package were quantified by tracking the motion of fiducials attached to these sites. The fiducials which were attached to the subjects and to the test fixture consisted of a one-half inch diameter black circle printed on a one inch diameter white circle. The locations of the fiducials generally followed the guidelines provided in "Film Analysis Guides for Dynamic Studies of Test Subjects, Recommended Practice" (SAE J138, March 1980). More complete descriptions of the fiducial locations as well as the photometric instrumentation system are provided in Appendices A and D. Timing reference marks were recorded on the 16 mm film once every 0.01 sec. These reference marks were synchronized with the electronic instrumentation recordings.

A video camera was also used to document the tests. This camera and accompanying recorder operate at 120 frames per second with an effective shutter speed of 10 microseconds or less. Use of this system allowed the investigators to evaluate the kinematic response of each subject immediately after each test. This system is described in Appendix A.

Photographs of the test subject and equipment configuration were taken prior to each test. Items ϵi special interest were photographed as required.

D. TEST SUBJECTS

The test dummy used for this program was an Alderson Research Laboratories, Inc., model VIP-95 dummy (serial number 124), which was designed to represent a 95th percentile (weight) adult male. The dummy was originally built for $-G_X$ automotive crash testing, based on specifications furnished to Alderson by the National Highway Traffic Safety Administration. It was designed to reproduce the head-neck response of human cadavers in forward facing impacts, but was not designed to produce meaningful response dynamics in vertical impacts. This limitation was not a critical factor in the current study, since the dummy was used only to verify the structural integrity of the test apparatus prior to human testing. The dummy's joints were adjusted to a nominal one G value, in accordance with the U.S. Department of Transportation Federal Motor Vehicle Safety Standard No. 208.

All human volunteer subjects who participated in this test program were members of the AFAMRL Impact Acceleration Stress Panel. This panel is composed of volunteer active duty Air Force members whose primary duties do not involve participation as subjects. Sixteen subjects (15 males and 1 female) were utilized during this test program. There were no special technical qualifications or training requirements for subjects. However, all subjects were qualified to participate only after successfully completing an intensive medical screening evaluation (Hearon & Raddin, 1981). This evaluation was directed by the panel physician and consisted of medical history screening, physical examination, visual acuity testing, audiometry, blood pressure measurement, routine laboratory examination (blood work and urinalysis), standard 12-lead electrocardiogram, pulmonary function tests, electroencephalogram, treadmill exercise stress test, and x-rays, including chest, skull, and complete spine films. The x-rays were reviewed by the panel physician in consultation with a radiologist (and orthopedic surgeon, as necessary) to assure elimination of individuals with disqualifying radiographic findings. The female subject had a negative pregnancy test documented and underwent a pelvic exam by a gynecologist, to assure there were no gynecologic contraindications to her participation. Relevant abnormalities in any part of the medical evaluation led to elimination of the candidate or specialty consultation and further examination, as required. Annual requalification of panel members was accomplished with a limited medical evaluation. including a physical examination and other relevant medical tests.

The generic human use protocol under which these impact tests were conducted was AFAMRL Protocol No. 80-01, "Generic Impact Acceleration Protocol, 1980". This document presented a survey of available human biodynamic test data, established broad generic exposure limits for human impact testing, and described the generic medical risks associated with such tests. Following review by the AFAMRL Human Use Review Committee (HURC) on 10 January 1980, this protocol was

recommended for approval by higher authority. Subsequently, the protocol was approved by AFAMRL/CC and, as SGO R-80-001, it was approved by USAF/SG on 7 March 1980. The specific human use protocol under which these tests were conducted was AFAMRL Protocol No. 80-23, "Evaluation of the F/FB-111 Crew Seat and Restraint System Headrest Position", which was reviewed and recommended for approval by AFAMRL/HURC on 26 June 1980 and which was subsequently approved by AFAMRL/CC. Protocol 80-23, as a specific protocol, required local consideration and approval only, in accordance with AFR 169-3, "Use of Human Subjects in Research Development, Test, and Evaluation" (February 1979).

Ongoing informed consent was provided by all subjects during the test program. Prior to testing, subjects received a thorough briefing on the experimental procedures and potential medical risks of participation. The subjects signed a witnessed consent form attesting to the fact that a detailed briefing was received and summarizing its content. Throughout the test program, the medical investigator continued to stress that any subject was free to withdraw at any time for any reason.

Table 2 is a summary of selected anthropometric values for each subject. The mean and standard deviation computed from each set of dimensions compare favorably with the mean and standard deviation of the dimensions obtained from an anthropometric survey of USAF personnel conducted in 1967 and published in AFSC Design Handbook 2-2. Forty-nine anthropometric measurements were obtained from each subject. The mean, standard deviation, and range of selected group measurements are listed in Table 3.

E. EXPERIMENT SEQUENCE

The varying parameters for each test (such as headrest position, bracing position, and restraint configuration) were provided to the test conductor and other personnel at the beginning of each day of testing. The conduct of all human exposures was the responsibility of a qualified and experienced test conductor. The test conductor directed the activities of all other personnel in the test area in accordance with a detailed checklist.

The first test of each day was done with an anthropomorphic dummy using the equipment configuration and test level planned for the first human test of the day. If no abnormalities were detected, the test personnel proceeded with preparations for tests with volunteer subjects. High-speed motion picture cameras were loaded and mounted on the test fixture. Seat vertical and footrest adjustments were made to obtain the appropriate seat configuration based upon the test plan and the anthropometry of the individual test subject. Video recording equipment was readied to permit immediate review of the test by the investigators. The accelerometer packages were then oriented in their respective reference planes and reference zero values were sampled using the data acquisition system.

Subject preparation was concurrent with preparation of the test fixture and instrumentation. Prior to each impact exposure, the subject provided a brief interval medical history and was physically examined. Emphasis was placed on neck or back symptoms, medications, abnormalities of recent sleep patterns, or recent overindulgence in food or alcoholic beverages. No subject was exposed

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TABLE 2. INDIVIDUAL SUBJECT ANTHROPOMETRY SUMMARY

SUBJECT NUMBER	WEIGHT (1b)	STATURE (in)	SITTING HEIGHT (in)	MID-SHOULDER SITTING HEIGHT (1n)
D-1 E-1 F-3 F-2 G-3 G-2 K-1 M-7 M-10 M-11 M-13 R-1 R-2 R-3	203 186 167 159 164 117 169 162 133 140 145 169 201 143 146	73.6 73.2 68.6 67.1 67.1 62.9 67.1 66.1 65.7 65.7 69.5 73.0 70.9 68.1 66.2	39.7 38.3 36.4 37.5 34.8 33.3 35.7 35.2 34.4 36.1 35.7 37.3 38.4 35.9 35.2	28.0 26.8 25.5 26.3 25.0 23.2 24.8 24.0 23.9 24.8 25.4 26.3 26.3 26.3
S-3	167	69.6	36.6	25.6
MEAN STD DEV	161 23.2	68.4 3.05	36.3 1.64	25.3 1.25

TABLE 3. COLLECTIVE SUBJECT ANTHROPOMETRY SUMMARY

ANTHROPOMETRIC MEASUREMENT	MEAN	STD DEV	RANGE
Weight Stature Cervicale Height Trochanteric Height Tibiale Height Chest Circumference Waist Circumference Buttock Circumference Acromion-Radiale Length Radiale-Stylion Length Sitting Height Mid-Shoulder Sitting Height Buttock-Knee Length Knee Height, Sitting Head Length Head Breadth Head Circumference Hip Breadth, Sitting	161	23.2	117 - 203
	68.4	3.05	62.9 - 73.6
	58.7	2.87	55.5 - 63.8
	35.8	2.21	32.3 - 39.9
	17.5	1.04	15.8 - 19.5
	37.6	1.38	35.6 - 40.0
	33.5	2.75	29.6 - 39.0
	37.9	2.43	33.7 - 42.9
	12.7	0.62	11.7 - 13.7
	10.3	0.72	8.5 - 11.3
	36.3	1.64	33.3 - 39.7
	25.3	1.25	23.2 - 28.0
	23.7	1.18	21.9 - 26.3
	21.3	1.30	19.6 - 23.5
	7.7	0.26	7.2 - 8.2
	6.0	0.18	5.6 - 6.4
	22.4	0.59	21.5 - 23.3
	14.3	0.88	12.5 - 15.7

with symptoms which may have obscured detection of test-related injury or which may have indicated predisposition to such injury.

All subjects wore orange, cut-off, long underwear to allow mounting of camera targets and instrumentation. Male subjects wore athletic supporters. The female subject wore a bathing suit. Each subject was instructed to void prior to entering the test area.

A disposable dental bite block (made of Optosil placed over a stainless steel frame) was molded for the subject prior to each impact test. An electrically-isolated accelerometer array was then mounted on the metal frame of the bite block. During this test program, the metal frame was modified with a metal arm which extended from the mouth of the subject to permit the mounting of a photometric target on a styrofoam block. This modification was implemented to permit more precise quantification of subject head displacement and to directly couple the electronic and photometric data obtained during the impact. The modified metal frame was utilized primarily during tests in cells E and F of the experimental matrix.

The medical instrumentation of each subject was standardized as follows. Three stick-on EKG electrodes were placed on the subject, one on the upper posterior aspect of each arm and a third on the right lateral chest, sixth intercostal space, mid-axillary line. The snap-on lead from each of these electrodes was plugged into a telemetry transmitter, which, in turn, was strapped to the left upper extremity of the subject. Continuous remote transmission of a single-lead EKG to a portable EKG machine located near the VDT was assured prior to each impact. Sitting and standing tracings were obtained immediately pre-impact (and post-impact) and a continuous tracing was obtained during test countdown and impact. Coincident with EKG recording, pretest (and post-test) sitting and standing blood pressure determinations were made for each subject by the medical technician using a sphygmomanometer. These pressures were recorded on the appropriate EKG tracing.

The subject was then fitted with the appropriate size USAF HGU-26/P flight helmet. After mounting the test fixture platform, the subject was asked to exhale and the chest accelerometer array was secured against his chest with a Velcro strap. The subject was then seated in the proper, upright position and the restraint harness was fitted and tightened. The F/FB-111 harness was fitted according to the procedure described in the F/FB-111 Technical Order. The shoulder straps were pre-tensioned to 14 ± 5 lb and the lap belt straps were pretensioned to 20 ± 5 lb. Stick-on photometric targets were placed on the subject at pre-determined locations (see Appendix D) and the positions of these targets relative to one another and to targets mounted on the test fixture were measured. Finally, the shoulder strap angles (relative to a reference horizontal) were measured.

The final pretest activity consisted of documentation of the test configuration by still photographs, measurement of subject blood pressure, evaluation of the electrocardiographic tracing by the medical monitor, and final safety checks of the test equipment and facility by the designated safety monitor. The test carriage was then elevated to an intermediate height while the water brake was filled with water. Finally, the carriage was raised to the specified drop height and the subject was directed to assume the specified upper extremity

bracing position. The test area was cleared, a countdown was initiated, and the carriage was allowed to fall onto the water brake to produce the desired impact.

The subject was provided with a foot switch which was connected to the control system of the VDT in such a way that the carriage could not be released unless the switch was depressed. In this manner, the subject was required to consciously provide his ongoing informed consent throughout the immediate pre-impact period (including the countdown) until carriage release, in order for the test to proceed. After carriage release, of course, it was no longer possible to abort the test.

A physician monitor, who was responsible for assuring subject safety during testing, was present for each test and reserved the right to cancel any test at any time for any reason. Such reasons may have included a recent history of neck or back strain, pretest pre-syncope, pretest arrhythmia, or any other condition of the subject, equipment, or procedure which was deemed by the monitor to place the subject at undue risk. The medical monitor was provided a finger-operated switch similar in function to the subject's switch. It had to be depressed prior to carriage release in order for the test to proceed. Agreement of both the subject and the medical monitor that the test should proceed was thus assured.

During testing, an ambulance crew was alerted and standing by within one-half mile of the test facility. In addition, emergency medical equipment was arranged in the test area for use by the physician monitor in the event of an emergency. This equipment included a defibrillator, oxygen equipment, intubation equipment, IV solutions and equipment, appropriate emergency drugs, backboard, harness cutters, and bandages.

Following the impact exposure, the subject was released from the harness. The physician monitor assured that the subject was uninjured. Post-test blood pressures and EKG (single-lead) were obtained and a brief post-test physical examination was accomplished. The subject was then provided with contacts to obtain later medical care as required or to ask questions relating to his participation. Impact exposures for each subject occurred no more frequently than once in any five-day period to allow time for detection of any occult injury.

The tests conducted at the experimental level in cells A, B, C, and D were randomized for each subject. After completing those 4 exposures, the subject was exposed in test condition E and then in test condition F. It was not practical to randomize cells E and F with the other cells due to the time required to change from the F/FB-lll harness to the conventional harness.

Two deviations from the test plan are noteworthy. First, the electronic data was lost in test #313, an 8 G orientation test in cell C for subject K1. This occurred due to a malfunction in the data acquisition system. This exposure was repeated for the subject as test #341. Second, subject R2 was inadvertently exposed to the same test conditions twice (test #347 and test #359). One of the two tests (test #359) was randomly selected for use in data analysis.

SECTION 4

TEST RESULTS AND ANALYSIS

A. OVERVIEW

The electronically measured and computed data obtained in this test program are summarized in Table B-1 in Appendix B. This table presents the arithmetic mean and standard deviation of each parameter in each cell of the experimental matrix. Typical analog data sets from each cell of the matrix and data summaries of each test at the experimental level are also presented in Appendix B.

A statistical analysis of these electronic test results was performed using the Wilcoxon paired-replicate rank test. The means and standard deviations of each parameter in each comparison are summarized in Tables C-1 through C-7 in Appendix C. Statistically significant trends in the measured and computed response parameters for each comparison are summarized in Tables 5, 10, and 12. In these tables, the arrow designates a statistically significant change in a parameter at the 90% confidence level for a two-tailed test. The arrow also indicates the direction of the trend from the cell smaller in magnitude. The number indicates the percentage increase in the parameter means. Wilcoxon computations from each parameter comparison yielding a statistically significant result are also presented in Appendix C.

The impact test conditions were controlled by using the same carriage plunger for all tests and by maintaining a constant drop height for all tests done at a specified test level. A drop height of 8.5 feet corresponded to an 8 G orientation exposure and a drop height of 11.0 feet corresponded to a test at the 10 G experimental level. All subjects experienced 8 G orientation tests in the C and D test conditions prior to participating in tests at the experimental level. Orientation tests were conducted principally to familiarize subjects with test procedures. The means and standard deviations of carriage acceleration, seat acceleration, and carriage velocity change for each cell of the experimental matrix are indicated in Table B-1 (Appendix B). During this test program, the peak carriage acceleration ranged from 10.3 G to 11.0 G, the peak seat acceleration ranged from 10.1 G to 11.0 G, and the carriage velocity change ranged from 25.3 ft/sec to 26.0 ft/sec.

The Wilcoxon analyses of these parameters revealed statistically significant differences in the peak seat acceleration in comparison C-D (Table 5) and the carriage velocity change in comparison A-C (Table 7). These differences in impact test conditions, attributable to variations in rail friction on the VDT, represented, at most, a 1% increase in the measured parameter. These small variations in test conditions do not appear to have biased the trends of the other measured parameters.

Two noteworthy modifications of the electronic data were made during data processing. Tare tests of the fixture were performed in order to assess the influence of the seat pan and footrest weights on the supporting load cells. Then, the product of the weight on each load cell and the instantaneous carriage acceleration was subtracted from the load cell data acquired during the human tests. In this manner, the recorded data was corrected for the seat pan and footrest weights. Second, the head acceleration data were correlated with the photometric data in order to assess the influence of subject headstrikes on the

headrest during the rebound phase of the impact. Acceleration spikes, particularly in the +X axis, at times exceeded the peak head acceleration recorded during the initial response phase. When this occurred, the electronic data base was modified by removing the late spike so that the recorded maximum was that which occurred during the initial impact response phase. In this way, it was assured that only initial impact response values were compared in the statistical analysis.

The photometric data analysis was limited to the data collected from the lateral camera mounted on the test fixture. The analysis, therefore, assumed that subject motion would be primarily in the X-Z plane. The maximum horizontal and vertical head displacements of subjects were obtained by tracking helmet-mounted and subject-mounted (on the cheek, e.g.) fiducials during the impact. The locations of these fiducials are specified in Figures D-1 and D-2 in Appendix D. Maximum head displacement data, summarized in Table D-1, could not be obtained for all tests in this series due to difficulties encountered in tracking fiducials during the photometric data processing. Problems in this area were related to the photometric targets becoming obscured by a portion of the test fixture or being washed out by the lighting in the impact area. Typical photometric data obtained during this test program are also presented in Appendix D.

Wilcoxon analyses of the maximum horizontal and vertical head displacements obtained at comparable target locations in comparable tests were performed. Summaries of these data are provided in the body of this report in Tables 4, 9, and 11. In these Tables, the asterisk indicates a statistically significant trend at the 90% confidence level and the number indicates the percent increase in the parameter means. The arrow indicates the direction of the trend.

B. HEADREST POSITION EFFECTS

The influence of fore-aft headrest adjustment on human impact response was assessed in comparisons A-B, C-D, and E-F. The experimental test conditions are defined in Table 1 and the fore and aft headrest adjustments are shown in Figures 1 and 3. The Wilcoxon comparisons of the pertinent photometric and electronic data are shown in Tables 4 and 5.

Analysis of the photometric data revealed that the maximum horizontal head displacement increases with the headrest at the forward adjustment, regardless of subject bracing and restraint configuration. The maximum vertical head displacement measured at the helmet decreases with the headrest in the forward position, whereas the maximum vertical displacement measured at the cheek increases with the headrest in the forward position. The latter findings were statistically significant in comparisons A-B and E-F, but were not significant in comparison C-D, although the trends were in the same direction. These findings (Table 4) are consistent with the interpretation of increased forward and downward head rotation with the headrest in the forward position.

A number of observations based on a review of the high-speed films may be made. Several subjects, including E1, F3, and G3, had difficulty placing their helmeted heads against the headrest in the aft position without some degree of extension of the cervical spine. It is not known whether or not this difficulty may be correlated with subject anthropometry. Also, it was possible to categorize the head motion of subjects during impact into five types, as summarized

TABLE 4

PHOTOMETRIC DATA:

SUMMARY OF STATISTICALLY SIGNIFICANT TRENDS FROM THE WILCOXON COMPARISONS AND PERCENT INCREASE IN PARAMETER MEANS

MATRIX CELL RESTRAINT HARNESS BRACING POSITION	F-111 Knees	B F-111 Knnes	C F-111 Lap	D F-111 Lap	E Conv Lap	F Conv Lap
HEADREST POSITION	Forw (n =	Aft 10)	Forw (n =	Aft 6)	Forw (n =	Aft 8)
HORIZONTAL DISPLACEMENT UPPER HELMET	127 <-	*	93 <-	*	106 <-	*
LOWER HELMET	65 <-	*	82 <-	*	39 <-	*
CHEEK VERTICAL DISPLACEMENT	76 <-	*	66 < -	*	49 < -	* *
UPPER HELMET	1 .	-> 12		-> 3	ł	-> 23
LOWER HELMET CHEEK	15 <-	-> 10 *	31 <-	-> 11	* (-	-> 11 17

This table summarizes the results of three separate comparisons of photometric data (A-B, C-D, and E-F) by means of the Wilcoxon paired-replicate rank test. The 90% confidence level for a two-tailed test was chosen as the level of statistical significance. An arrow designates a trend or change in a parameter between two test conditions and also indicates the direction of the trend from the smaller to the larger parameter mean. The number indicates the percentage increase in the parameter means. A statistically significant trend is indicated by an asterisk.

ELECTRONIC DATA:

SUMMARY OF STATISTICALLY SIGNIFICANT TRENDS FROM THE WILCOXON COMPARISONS AND PERCENT INCREASE IN PARAMETER MEANS

MATRIX CELL RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	A B F-111 F-111 Knees Knees Forw Aft (n = 14)	C D F-111 F-111 Lap Lap Forw Aft (n = 13)	E F Conv Conv Lap Lap Forw Aft (n = 12)
CARRIAGE ACCELERATION CARRIAGE VELOCITY SEAT ACCELERATION CHEST ACCELERATION -X axis		> 1	27
+X axis +Z axis Resultant CHEST SEVERITY INDEX HEAD ACCELERATION	> 10	136 <	68 <
-X axis +X axis +Z axis Resultant HEAD SEVERITY INDEX STRAP LOADS	> 89	5 <	> 9
Reflection Straps Inertia Reel Straps Total Shoulder Straps Total Lap Belt Crotch Strap	17 <		† †
SEAT PAN LOADS -X axis +Z axis Resultant FOOTREST LOADS		8 <	
-X axis +Z axis Resultant		> 10	

SEE APPENDIX C

Table C-1 Table C-2

Table C-3

This table summarizes the results of three separate comparisons of electronic data (A-B, C-D, and E-F) by means of the Wilcoxon paired-replicate rank test. The 90% confidence level for a two-tailed test was chosen as the level of statistical significance. An arrow designates a statistically significant trend or change in a parameter mean between two test conditions and also indicates the direction of the trend from the smaller to the larger parameter mean. The number indicates the percentage increase in the parameter means. The actual means used to compute these percentages are listed in Tables C-1, C-2, and C-3 in Appendix C. A dagger (†) indicates that no comparison was possible, since the conventional harness does not have reflection straps or a crotch strap.

TABLE 6
CLASSIFICATION OF TYPES OF HEAD MOTION

MARD 1" AFT E) (CELLS B, D, F)
. E) (CELLS B. D. F)
) (n = 39) 2
3
5
8

Total n = 76, since photometric data was not available for all tests.

in Table 6. Cervical spine flexion presumably occurred when there was either forward and downward head rotation or forward translation of the head. On the other hand, cervical spine extension presumably occurred when there was either forward translation followed by rearward rotation of the head or only rearward rotation of the head. Grouping the responses in this way allows application of the Yates chi-square test to evaluate the correlation between cervical spine flexion or extension and headrest position. A pertinent 2 X 2 contingency table is shown in Table 7: Assuming equivalent populations and a standard confidence limit, <= 0.05, the null hypothesis that the rate of cervical spine flexion with the headrest forward is not increased can be rejected. The 2 X 2 contingency shown in Table 8 may also be derived from the data provided in Table 6. Applying the same assumptions, in this case, the null hypothesis that the rate of cervical spine extension with the headrest aft is not increased can be rejected. These correlations between forward adjustment and flexion and between aft adjustment and extension are consistent with the results of analysis of the digitized photometric data presented above.

The head acceleration findings are summarized in Table 5. There was a small but statistically significant increase in the vertical head acceleration with the headrest in the forward position in the C-D comparison. Relatively large statistically significant increases in head acceleration measured along the -X axis were found with the headrest forward in all three comparisons. As indicated in Section 2B, the -X head acceleration measurement is actually a reflection of vertical head acceleration due to the forward rotation of the head during impact. In addition, statistically significant increases in +X axis head acceleration were observed with the headrest aft. In comparison A-B, this increase was 89% and, in comparison C-D, this increase was 114%. No statistically significant trends were observed in resultant head acceleration.

These acceleration findings are consistent with the aforementioned photometric data. With the headrest 1 inch aft of the plane of the seat back, subject head motion is primarily translational, as evidenced by increased acceleration in the +X axis. With the headrest 2 1/4 inches forward of the plane of the seat back, subject head motion is primarily rotational, as evidenced by increased head acceleration in the -X axis (which reflects a vertical component of acceleration). These acceleration findings are strong enough to be significant at the 95% confidence level for the two-tailed test. Furthermore, since these

TABLE 7

CERVICAL SPINE FLEXION AS A FUNCTION OF HEADREST POSITION

		HEADREST 2	₹" FORWARD
		NO	YES
CERVICAL	NO	34	15
SPINE FLEXION	YES	55	22

TABLE 8

CERVICAL SPINE EXTENSION AS A FUNCTION OF HEADREST POSITION

		HEADRES	T 1" AFT
		110	YES
CERVICAL SPINE	NO	26	10
EXTENSION	YES	11	29

trends in head acceleration components are in opposite directions, their effects are counterbalancing as evidenced by the absence of statistically significant changes in resultant head acceleration.

The practical significance of the few other statistically significant trends in these three headrest position comparisons is questionable. There were no consistent statistically significant trends in other parameters in all three comparisons. The absence of statistically significant changes in vertical and resultant seat loads indicates that adjustments in headrest position did not influence the magnitude of the total vertebral column loading during vertical impacts.

C. UPPER EXTREMITY BRACING EFFECTS

The influence on human impact response of upper extremity bracing was assessed in comparisons A-C and B-D. The hands-on-knees position (Figure 4) was compared to a position in which the hands were relaxed in the lap to preclude upper extremity bracing (Figure 5). The Wilcoxon comparisons of the pertinent photometric and electronic data are shown in Tables 9 and 10.

Analysis of the digitized photometric data revealed that the maximum horizontal and vertical displacements of the head were increased in the hands-in-lap position compared to the hands-on-knees position. As shown in Table 9, the statistically significant increases in head displacement were found in the

TABLE 9
PHOTOMETRIC DATA:

SUMMARY OF STATISTICALLY SIGNIFICANT TRENDS FROM THE WILCOXON COMPARISONS AND PERCENT INCREASE IN PARAMETER MEANS

MATRIX CELL RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	A F-111 Knees Forw	C F-111 Lap Forw	B F-111 Knees Aft	D F-111 Lap Aft
HORIZONTAL DISPLACEMENT UPPER HELMET LOWER HELMET CHEEK VERTICAL DISPLACEMENT		= 7) -> 80 -> 59 -> 41	*	10) -> 68 -> 31 -> 32
UPPER HELMET LOWER HELMET CHEEK	• •	-> 11 -> 2 -> 27	* *	-> 10 -> 11 -> 12

This table summarizes the results of two separate comparisons of photometric data (A-C and B-D) by means of the Wilcoxon paired-replicate rank test. The 90% confidence level for a two-tailed test was chosen as the level of statistical significance. An arrow designates a trend or change in a parameter between two test conditions and also indicates the direction of the trend from the smaller to the larger parameter mean. The number indicates the percentage increase in the parameter means. A statistically significant trend is indicated by an asterisk.

TABLE 10
ELECTRONIC DATA:

SUMMARY OF STATISTICALLY SIGNIFICANT TRENDS FROM THE WILCOXON COMPARISONS AND PERCENT INCREASE IN PARAMETER MEANS

MATRIX CELL	AC	BO
RESTRAINT HARNESS	F-111 F-111	F-111 F-111
BRACING POSITION	Knees Lap	Knees Lap
HEADREST POSITION	Forw Forw	Aft Aft
	(n = 14)	(n = 13)
CARRIAGE ACCELERATION		1 ' '
CARRIAGE VELOCITY	> 0.4	ŀ
SEAT ACCELERATION		t 1
CHEST ACCELERATION		1
-X axis	> 33	> 36
+X axis		1 "
+Z axis	> 9	
Resultant		1
CHEST SEVERITY INDEX	> 13	
HEAD ACCELERATION	13	
-X axis	}	1 .
+X axis	1	1
+Z axis	1	
Resultant	1	4 <
	! !	4 4
HEAD SEVERITY INDEX	1 1	
STRAP LOADS		
Reflection Straps		> 18
Inertia Reel Straps	> 18	> 31
Total Shoulder Straps]	> 28
Total Lap Belt	1 1	i l
Crotch Strap		į
SEAT PAN LOADS	[1
-X axis	> 8	[
+Z axis	> 5	> 4
Resultant	> 6	> 4
FOOTREST LOADS	1	1
-X axis	39 <	30 <
+Z axis	16 <	13 <
Resultant	29 <	21 <
	 	
CEE ADDENDIV C	Table C 4	Table C E

SEE APPENDIX C

Table C-4

Table C-5

This table summarizes the results of two separate comparisons of electronic data (A-C and B-D) by means of the Wilcoxon paired-replicate rank test. The 90% confidence level for a two-tailed test was chosen as the level of statistical significance. An arrow designates a statistically significant trend or change in a parameter mean between two test conditions and also indicates the direction of the trend from the smaller to the larger parameter mean. The number indicates the percentage increase in the parameter means. The actual means used to compute these percentages are listed in Tables C-4 and C-5 in Appendix C.

B-D comparison only. In both comparisons, the increases in maximum horizontal head displacement were relatively larger than the increases in maximum vertical head displacement.

Analysis of the head acceleration data revealed no statistically significant changes in the A-C comparison. (See Table 10.) However, in the B-D comparison, a relatively small (4%) increase in vertical and resultant head acceleration was observed in the hands-on-knees position. These findings are consistent with the relatively smaller head displacements in the hands-on-knees position observed in the photometric data. The head acceleration findings are certainly attributable to the use of upper extremity bracing, but, in this study, they are observed for the aft headrest adjustment only.

Statistically significant increases in the -X axis chest acceleration (toward the seat back) were observed for the hands-in-lap position in both comparisons A-C and B-D. With the headrest forward (i.e., in the A-C comparison) statistically significant increases in vertical chest acceleration and the chest Severity Index were also observed for the hands-in-lap position. The latter findings, however, were not significant at the 95% confidence level. These findings are consistent with the intended purpose of the hands-on-knees bracing posture, which includes stabilization of the upper torso during impact.

The statistically significant increases in shoulder strap loads in the hands-inlap position suggest a greater inertial response of the upper torso compared to the hands-on-knees position. These findings are stronger with the headrest aft (in the B-D comparison), being significant at the 95% confidence level. No changes in lap belt or crotch strap loads were observed as a function of upper extremity bracing.

The vertical and resultant seat loads were increased in the hands-in-lap position compared to the hands-on-knees position, regardless of headrest position. Although the magnitudes of these changes are relatively small, their practical significance is of considerable importance. This is true because seat loads represent the best indirect measurement of vertebral column loading during impact. The significance of these findings will be further discussed in Section 5 of this report.

In both comparisons, statistically significant increases in the horizontal, vertical, and resultant footrest loads were seen in the hands-on-knees position compared to the hands-in-lap position. These trends are related to the seat load trends, which are in the opposite direction. The tandem footrest and seat load findings are consistent with the intended purpose of the hands-on-knees brace. Using this bracing technique, force is carried through the upper and lower extremities to the footrest as the seat is inloaded.

D. RESTRAINT CONFIGURATION EFFECTS

The influence on human impact response of the restraint harness configuration was assessed in comparisons C-E and D-F. The proposed, modified F/FB-111 restraint configuration (Figure 6) and a standard or conventional double shoulder strap - lap belt configuration (Figure 7) were compared. The Wilcoxon comparisons of the photometric and electronic data are summarized in Tables 11 and 12.

Analysis of the photometric data revealed a statistically significant increase in maximum horizontal head displacement measured at the low helmet fiducial in the conventional harness compared to the F/FB-111 harness with the headrest aft (comparison D-F). Also, statistically significant increases up to 31% were seen in maximum vertical head displacement measured at the helmet and cheek fiducials in the conventional harness compared to the F/FB-111 harness in the D-F comparison. No statistically significant changes were seen with the headrest in the forward adjustment location (C-E comparison). Therefore, the statistically significant trends in the photometric data indicated that higher head displacements, particularly in the vertical direction, were experienced in the conventional harness.

However, the electronic data (Table 12) revealed statistically significant increases in vertical and resultant head acceleration in the conventional harness compared to the F/FB-111 harness in both comparisons C-E and D-F. Similar statistically signifiant trends were found in the head Severity Index. These findings are consistent with the interpretation of degraded performance in the conventional harness.

In comparison D-F, statistically signficant increases in +X chest acceleration and the chest Severity Index were observed in the conventional harness compared to the F/FB-111 harness. These findings are also indicative of degraded performance in the conventional harness with the headrest in the aft position. In the C-E comparison, it was interesting to observe a statistically significant increase in chest Severity Index, while the mean resultant chest acceleration was actually larger in the C condition than in the E condition. Since the chest Severity Index is a function of the area beneath the chest resultant - time curve, in the absence of higher peak accelerations in the conventional harness, the measured duration of the chest acceleration response must be greater in the conventional harness. Inspection of the data revealed that this in fact was the case.

Statistically significant increases in the shoulder strap loads by an average of 44% were seen in the F/FB-111 harness. On the other hand, statistically significant increases in the lap belt loads (21%) were observed in the conventional harness. These findings, which were independent of headrest position, indicate that loads are carried very differently in the two harnesses. This is probably related to the unique geometry of the F/FB-111 harness shoulder straps and the presence of the crotch strap.

TABLE 11

PHOTOMETRIC DATA:

SUMMARY OF STATISTICALLY SIGNIFICANT TRENDS FROM THE WILCOXON COMPARISONS AND PERCENT INCREASE IN PARAMETER MEANS

MATRIX CELL RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	C F-111 Lap Forw	Ē Conv Lap Forw	D F-111 Lap Aft	F Conv Lap Aft
HORIZONTAL DISPLACEMENT UPPER HELMET LOWER HELMET CHEEK	33 <- 36 <- 24 <-		(n 10 <- *	= 9) > 21 > 8
VERTICAL DISPLACEMENT UPPER HELMET LOWER HELMET CHEEK	 0	-> 21 -> 21	* *	-> 31 -> 23 -> 12

This table summarizes the results of two separate comparisons of photometric data (C-E and D-F) by means of the Wilcoxon paired-replicate rank test. The 90% confidence level for a two-tailed test was chosen as the level of statistical significance. An arrow designates a trend or change in a parameter between two test conditions and also indicates the direction of the trend from the smaller to the larger parameter mean. The number indicates the percentage increase in the parameter means. A statistically significant trend is indicated by an asterisk.

TABLE 12
ELECTRONIC DATA:

SUMMARY OF STATISTICALLY SIGNIFICANT TRENDS FROM THE WILCOXON COMPARISONS AND PERCENT INCREASE IN PARAMETER MEANS

C F-111 Lap Forw	E Conv Lap Forw		D F-111 Lap Aft	F Conv Lap Aft
(n =	13)		(n =	12)
				-> 34
1			Ab cal	-> 26
	-> 11 -> 12			-> 16 -> 15
İ			•-	-> 32 †
	-> 21			-> 21
	-> 6			-> 15 -> 5 -> 6
	-> 5			
	F-111 Lap Forw (n =	F-111 Conv Lap Forw Forw (n = 13) > 16 10 <> 24 + + 40 <> 21 +> 6> 6> 6> 18> 5	F-111 Conv Lap Lap Forw Forw (n = 13) > 16 10 <> 21> 24 + 40 <> 21 +> 6> 6> 6> 5	F-111 Conv Lap Forw Forw Aft (n = 13) > 16 10 <> 11> 12> 24 + 40 <> 21 +> 6> 6> 18> 5

SEE APPENDIX C

Table C-6

Table C-7

This table summarizes the results of two separate comparisons of electronic data (C-E and D-F) by means of the Wilcoxon paired-replicate rank test. The 90% confidence level for a two-tailed test was chosen as the level of statistical significance. An arrow designates a statistically significant trend or change in a parameter mean between two test conditions and also indicates the direction of the trend from the smaller to the larger parameter mean. The number indicates the percentage increase in the parameter means. The actual means used to compute these percentages are listed in Tables C-6 and C-7 in Appendix C. A dagger (†) indicates that no comparison was possible, since the F/FB-111 harness has reflection straps and a crotch strap and the conventional harness does not.

In both comparisons C-E and D-F, statistically significant increases in seat loads were found in the conventional harness compared to the F/FB-111 harness. The increase in the resultant seat load was 6% in both comparisons. These findings are indicative of increased vertebral column loading in the conventional harness and are, therefore, consistent with the interpretation of degraded impact protection in the conventional harness.

Horizontal, vertical, and resultant footrest loads were significantly increased in the conventional harness in the C-E comparison only. Although these findings must be a function of the restraint configuration, the absence of similar findings in the D-F comparison suggest that they may also be related to the forward position of the headrest as well.

Except for the vertical footrest load finding, all trends in both the C-E and D-F comparisons were statistically significant at the 95% confidence level.

E. MEDICAL FINDINGS

The subjective and objective medical findings from this test program are summarized in Table 13. The relatively large number of subjects experiencing cervical pain at the time of impact in test condition F is noteworthy. All six of these subjects experienced some degree of cervical spine extension during the impact. As previously noted, there was a strong correlation between aft headrest adjustment and the tendency for cervical spine extension. This tendency was particularly strong in test condition F, probably due to the relatively poor upper torso restraint provided by the conventional harness and the subjects' efforts to brace helmeted head on the headrest. At this writing, three of the six subjects who experienced cervical pain in this test condition have voluntarily terminated their participation in impact acceleration stress experiments. The termination spine x-rays of these subjects were within normal limits.

TABLE 13
SUMMARY OF SUBJECTIVE AND OBJECTIVE MEDICAL FINDINGS

	TEST L	EVEL (CELL OF	MATRIX)
MEDICAL FINDING	8G (C,D)	10G (A-E)	10G (F)
	(n = 33)	(n ≈ 70)	(n = 12)
Cervical Pain	0	4	6
Paresthesias	4	0	1
Abrasions	0	0	1
Contusions	0	1	0
Muscle Strains	2	1	0

Subject attrition during this test program was not unusual. Two of the sixteen subjects who participated in the program, El and M7, were disqualified from further participation as a result of presumed muscle strains. Subject M7 incurred a mid-thoracic paravertebral muscle strain during an 8 G impact in test condition D. Since the subject had planned to voluntarily terminate his participation six weeks from that time, he was disqualified from further participation. Subject El incurred a moderately severe paracervical muscle

strain during a 10 G test in test condition D. Post-injury cervical spine films were negative for fracture, but the subject was disqualified from further participation when his injury did not promptly resolve. In retrospect, both of these subjects, in addition to subjects D1, F3, and G3, by virtue of having rounded shoulders, had difficulty placing their heads on the headrest in the aft position.

None of the adverse medical effects described above were believed to have any long-term clinical significance. The impact test conditions investigated in this study were believed to be well within human tolerance.

SECTION 5

DISCUSSION

A. HEADREST POSITION EFFECTS

Adjustment of the headrest 2 1/4 inches forward of the plane of the seat back causes an increase in forward and downward head rotation. This is evidenced by an increase in maximum horizontal head displacement, an increase in maximum vertical head displacement measured at the cheek, and a decrease in maximum vertical displacement measured at the helmet. The increase in head rotation is also evidenced by an increase in head acceleration in the -X axis. Adjusting the headrest 1 inch aft of the plane of the seat back is associated with, in many cases, forward translation of the head and extension of the cervical spine. The forward translation is evidenced by an increase in head acceleration in the +X axis. Extension of the cervical spine was noted particularly in test condition F and was presumably due to the relatively ineffective upper torso restraint provided by the shoulder straps. These findings are summarized in Tables 4 and 5.

The similarity between these test results and the findings of previous human impact tests conducted nearly 40 years ago is remarkable. Savely and Ames (1946, 1948) conducted a test program using a T-2 catapult on a 30-foot ejection tower. Vacuum tube accelerometers were used to measure accelerations. These investigators observed that the location of the center of gravity of the head prior to a vertical impact is apparently responsible for the degree and the direction of neck bending during the event. It was presumed that this neck bending was due to the fore-aft position of the headrest. In the initial studies, since the fore-aft position of the headrest was not adjusted, the position of the head relative to the seat back plane was determined by the "conformation" of the subject. A subject with rounded shoulders found it necessary to extend his neck in order to place his head on the headrest. In subsequent human impact tests, the fore-aft position of the headrest was varied through a range of 2 inches from 1/4 inch to 2 1/4 inches aft of the seat back plane. Neck flexion was noted if the headrest was too far forward and extension was noted if the headrest was too far aft. The proper headrest adjustment to prevent either flexion or extension was found to vary from subject to subject. Only neck muscle strains were noted as adverse medical effects in this test series.

The cervical spine fractures and dislocations incurred operationally in open ejection seats from January 1971 to December 1978 was recently summarized (Kazarian et al., 1980). These accident investigation data were provided by the Air Force Inspection and Safety Center. During the eight-year period evaluated there were 595 ejections. Eleven major injuries and six fatal injuries were the result of cervical spine trauma. Five of the nonfatal injuries were attributed to ejection force, all occurred in the C5-C7 range, and all were assigned a hyperflexion injury mechanism. Seven major or fatal injuries were believed to have been caused by a hyperextension injury mechanism. Five of these were presumed to have been caused by aerodynamic forces (windblast), one was presumably caused by parachute opening shock, and another was of unknown etiology. If these data are accurate, it would appear that bony cervical injuries have not occurred as the result of hyperextension during ejection. This may be true because the headrest, regardless of fore-aft adjustment, effectively limits the

amount of cervical extension possible during vertical impact. These operational ejection data were not correlated with fore-aft headrest position.

In addition to these bony injuries, a variety of soft tissue cervical injuries undoubtedly occurred during this operational ejection experience. Hyperflexion of the cervical spine may cause injury to the posterior ligamentous structures, such as the posterior longitudinal ligament, the ligamentum flavum, and the interspinous and supraspinous ligaments. Hyperextension of the cervical spine may cause injury to the anterior ligamentous structures, such as the anterior longitudinal ligament. Tears of the anterior longitudinal ligament as a result of hyperextension injuries are often evidenced by anteroinferior avulsion fractures of the involved vertebral body (Burke, 1971). Anterosuperior chip fractures of the cervical vertebral bodies are generally the result of hyperflexion injury (Dolan, 1977).

In the present study, adjusting the headrest 1 inch aft of the plane of the seat back apparently predisposed subjects to cervical extension during impact. This assertion has been substantiated by the Yates chi-square analysis in Section 4B. A worrisome finding was that nine of the ten subjects reporting cervical pain during impacts in this test series experienced some degree of cervical extension during the event. The headrest was adjusted aft in nine of these same ten cases. Two subjects (El and M7), for whom the soft tissue injury threshold was exceeded, also experienced cervical extension during the impact. Subjects with rounded shoulders found it necessary to slightly extend the neck in order to reach the headrest in the aft adjustment position. In view of all these findings, it is apparent that, for some subjects, adjustment of the headrest 1 inch aft of the plane of the seat back places the seat back too far aft.

On the other hand, adjusting the headrest 2 1/4 inches forward of the plane of the seat back apparently does increase the forward and downward rotation of the head. Such a forward headrest location is also detrimental to rearward visibility in high-performance, fighter aircraft. Although the threshold for cervical injury may be higher in flexion than in extension, the basic principles of impact protection dictate that head displacement and acceleration be minimized in order to reduce the probability of injury. The forward headrest location investigated in this study would not be consistent with the goal of minimizing head displacement and acceleration.

The optimal fore-aft headrest adjustment may vary from subject to subject. However, if the fore-aft headrest location must be fixed, an adjustment between the two extremes investigated in this study may be indicated to minimize head acceleration and the potential for extension or flexion of the cervical spine. Therefore, further vertical impact tests with human subjects at various fore-aft headrest adjustments between the extremes investigated in this study are recommended to clarify this issue.

B. UPPER EXTREMITY BRACING E'FECTS

Human response to vertical impact in the hands-on-knees position was compared to human response in the hands-in-lap position. Use of the hands-on-knees position produced significant decreases in -X chest acceleration and vertical and resultant seat loads as well as significant increases in footrest loads. These findings, summarized in Table 10, are consistent with the intended purpose of the hands-on-knees brace, which is to create alternate pathways to transmit loads. In this position, greater loads are carried through the extremities to the footrest and the vertebral column is unloaded. The increased vertical and resultant head accelerations seen in the hands-on-knees position in the B-D comparison do not mitigate these findings. This is true because head accelerations well in excess of those reported in this study have been tolerated in other human impact tests without difficulty (Brinkley et al., 1977; Carter, 1959; Lombard, 1951).

The potential operational significance of the experimentally determined trends in seat loads is noteworthy. As previously indicated, the seat loads indirectly provide a measure of vertebral column loading. Since excessive axial loading is a well known cause of vertebral fracture during ejection, it is reasonable to assume that a reduction in this loading could have a beneficial effect operationally, in terms of decreasing the rate of vetebral fracture. The modest reduction in seat loads observed by using the hands-on-knees position experimentally could be beneficial if used operationally in, for example, the F/FB-111 crew module prior to landing impact.

Utilizing the upper extremities to carry loads as a means of unloading the vertebral column is not a new impact protection concept. In his review of the early impact test literature, Cofer et al. (1946) reported that the Germans had conducted catapult tests with and without the arms positioned on armrests adjusted to the appropriate height. In a test without armrest support, a vertebral fracture was reported at a maximum catapult acceleration of 28 G (velocity change not specified). It was concluded that higher impact acceleration levels could be tolerated with armrest bracing than without. This work was corroborated by subsequent human impact tests in which forces exerted by the upper extremities on armrests were quantified (Savely and Ames, 1946).

Since use of the hands-on-knees position has been demonstrated to decrease vertebral loading, as evidenced by reduced seat loads, by carrying a greater proportion of the load through the extremities to the footrest, it is recommended that consideration be given to employing this hands-on-knees technique operationally. This could be done in situations in which crewmembers were able to anticipate impending vertical impacts.

C. RESTRAINT CONFIGURATION EFFECTS

In this study, human response to vertical impact in a proposed, modified F/FB-111 restraint harness was compared to such response in a conventional double shoulder strap - lap belt configuration. Use of the conventional harness was accompanied by increases in vertical and resultant head acceleration and head Severity Index, increases in the chest Severity Index, increases in lap belt loads and seat loads, and decreases in shoulder strap loads. These findings were true regardless of headrest adjustment. With the headrest forward of the plane of the seat back (comparison C-E), footrest loads were also increased in the conventional harness. With the headrest in the aft position, chest acceleration in the +X axis was increased in the conventional harness. These findings are summarized in Table 12.

These results indicate that the F/FB-111 harness reacts a greater proportion of the inertial load through the harness than the conventional harness. The statistically significant increases in vertical and resultant seat loads in the conventional harness are noteworthy. These statistically significant findings are probably due to the unique geometry of the F/FB-111 harness, which incorporates reflection straps, a shoulder harness yoke, and a crotch strap. Further vertical human impact studies should be accomplished in the conventional harness with an added crotch strap in order to help clarify these experimental findings.

SECTION 6

SUMMARY

A. PROGRAM OBJECTIVES

This test program was designed to achieve the following objectives (Section 18).

- 1. Evaluate human response to vertical impact with the headrest 1 inch aft of the plane of the seat back compared to the headrest adjustment 2 1/4 inches forward of the seat back plane.
- 2. Evaluate human response to vertical impact in the hands-on-knees bracing position compared to the hands-in-lap position in which upper extremity bracing is precluded.

ميكون يه سده ممكسيا الله فلافظاف فيالك تعال كالمناطات مالات

- 3. Evaluate human response to vertical impact in a proposed, modified F/FB-111 restraint harness compared to response in a conventional double shoulder strap lap belt restraint configuration.
- 4. Obtain human impact data for use in the development of current and future mathematical models intended to predict human response to impact.

B. TEST PROGRAM

- 1. A factorial experimental design was used in order to achieve the above program objectives. All tests were conducted with the vertical centerline of the seat back parallel to the impact axis (Section 2A).
- 2. The Vertical Deceleration Tower (VDT) was utilized to provide experimental level $+G_7$ impacts of 10 G (26 ft/sec). (Section 3A).
- 3. The seat utilized in this program was a crew seat salvaged from a F/FB-111 crew module. The proposed, modified F/FB-111 restrain: harness utilized was provided by General Dynamics. Instrumentation was provided by AFAMRL (Sections 3B and 3C).
- 4. Human volunteer subjects were medically qualified and utilized in accordance with applicable human use regulations (Section 3D).
- 5. Relevant accelerations, velocities, and forces were measured electronically. Appropriate physiological data were obtained. Subject motion was documented by high-speed cameras (Sections 3C, 3D, and 3E).
- 6. One-hundred and fifteen human impact tests were conducted from July to October 1980. Thirty-three cf those experiments were at the 8 G orientation level and eighty-two of the tests were conducted at the 10 G experimental level (Sections 3D and 3E).
- 7. The Wilcoxon paired-replicate rank test was utilized in data analysis to establish the statistical significance of test results (Section 2B).

C. TEST RESULTS

- 1. All accelerations, velocities, and forces measured in these test conditions were considered to be well within human tolerance (Section 4E .
- 2. At least four of the sixteen subjects who participated in this test program experienced physical difficulty reaching the aft headrest location. These subjects were required to slightly extend the cervical spine in order to place helmet on headrest prior to the experiment (Section 4B).
- 3. In the fore-aft headrest adjustment comparison, maximum horizontal head displacement was increased with the headrest 2 1/4 inches forward of the plane of the seat back. Maximum vertical head dis-placement measured at the cheek was also increased. A statistically significant increase in head acceleration in the -X axis was seen with the headrest forward. With the headrest aft, a statistically significant increase in head acceleration in the +X axis was observed in tests conducted in the F/FB-111 harness. These findings were consistent with increased forward and downward head rotation with the headrest forward and increased forward-translation of the head with the headrest aft (Sections 4B, 5A).
- 4. In the upper extremity bracing comparison, statistically significant decreases in -X chest acceleration and resultant seat loads as well as statistically significant increases in footrest loads were observed in the hands-on-knees position compared to the hands-in-lap position. With the headrest aft, small but statistically significant increases in vertical and resultant head acceleration were also observed in the hands-on-knees position. These findings are consistent with the interpretation that the hands-on-knees position unloads the vertebral column and carries a great proportion of the load through the extremities to the footrest (Sections 4C, 5B).
- 5. In the restraint harness comparison, statistically significant increases in resultant head acceleration, head Severity Index, lap belt and seat loads and statistically significant decreases in shoulder strap loads were observed in the conventional harness compared to the F/FB-111 harness. These findings indicated that the F/FB-111 harness reacts a greater proportion of the impact response through the harness itself compared to the conventional double shoulder strap lap belt configuration (Sections 4D, 5C).
- 6. Subtolerance human impact tests can be an effective tool in the investigation of impact protection systems and voluntary bracing techniques.

D. RECOMMENDATIONS

1. Additional impact tests with human volunteer subjects exploring fore-aft headrest adjustments between the extremes investigated in this study may be useful (Section 5A).

The state of the s

- 2. Consideration should be given to utilizing the hands-on-knees bracing position operationally prior to anticipated vertical impacts in order to help unload the vertebral column. For example, the technique may be useful as a post-ejection bracing procedure in the F/FB-111 prior to landing impact of the crew module. Before such a recommendation may be confidently made, however, a direct comparison of human impact response in the hands-on-knees position to response in the currently recommended crossed-arms position will be required (Section 5B).
- 3. The findings of the restraint harness configuration comparison may be clarifed by additional vertical human impact tests of the conventional harness with an added crotch strap (Section 5C).

APPENDIX A

DATA ACQUISITION EQUIPMENT AND METHODS

Prepared by

Harold F. Boedeker Wesley M. Waldron

Dynalectron Corporation
Scientific Services Division

INTRODUCTION

Under Contract F33615-79-C-0523, Dynalectron was requested by the Air Force Aerospace Medical Research Laboratory/Biomechanical Protection Branch to instrument a test fixture fabricated by General Dynamics Corporation and collect data under test conditions for the F/FB-111 Crew Seat and Restraint System Head Rest Position evaluation program. The testing was conducted in one axis of acceleration on the Vertical Deceleration Tower Test Facility located at the Air Force Aerospace Medical Research Laboratory, Building 824, Area B, Wright-Patterson Air Force Base. The following is a discussion of the equipment and techniques used in acquiring and processing data that describes the kinematic and inertial responses of the human body. Installation and sensor specifications are also included in the discussion.

DATA MEASUREMENT DEVICES

This evaluation program was instrumented using thirty-seven transducers. The Digital Instrumentation Requirements sheets of Figures A-1 through A-3 contain the pertinent data for each channel.

SUBJECT INSTRUMENTATION

Each subject was instrumented with six accelerometers. These accelerometers were configured in groups of three to create two triaxial measuring packages. Each package was mounted to indicate accelerations in the X, Y and Z axes. Figure A-4 shows the coordinate system utilized and the corresponding output polarity for an applied acceleration.

The accelerometer package used to measure head accelerations was designed to be inserted into the subject's mouth. It consisted of three Endevco accelerometers, Model 2264-200, mounted to a plastic block with dimensions of 7/16 x 7/16 x 7/16 inches. This assembly was covered with a medical grade silicone rubber sealant to provide electrical isolation. The three accelerometer cables were routed to one end of the block. Next, a dental bracket that had been custom fitted to the subject's mouth was mounted to the block. The approximate weight of the completed package was 50 grams. When the dummy subject was used the dental bracket was removed and the package was mounted to a bracket at the approximate center of the dummy's head. Specifications for the accelerometers used in this package are shown in Figure A-5.

The accelerometer package used to measure chest accelerations was designed to be attached externally to the subject's chest. It consisted of three Endevco accelerometers, Model 2264-150, mounted to an aluminum block that measured approximately $5/8 \times 5/8 \times 3/4$ inches. This

assembly was inserted into an aluminum protection shield that was attached to a length of Velcro fastener strap. In use, the completed package was placed over the subject's sternum while the Velcro strap was wrapped around the subject and fastened. Specifications for the accelerometers used in this package are shown in Figure A-6.

HARNESS INSTRUMENTATION

During this evaluation program, a proposed, modified F-111 harness was used as well as a conventional harness. Figure A-7 shows the test fixture, seat and F-111 harness. Figure A-8 shows the test fixture, seat and conventional harness. The output polarity of each load cell corresponds to an applied load in accordance with the coordinate system shown in Figure A-9.

A total of seven load cells were used to instrument the F-111 harness. Two of the transducers used were Lebow automotive belt load cells, Model 3419. These load cells monitored the load applied to the left and right inertia reel straps as shown in Figure A-10. Specifications for these load cells are shown in Figure A-11.

The five remaining load cells utilized the restraint harness hardware. Four 350 ohm resistive strain gages were bonded to each piece of harness hardware and wired in a bridge configuration. Figure A-12 shows the strain gage placement and wiring diagram. Figure A-10 shows the two reflection straps and Figure A-13 shows the lap and crotch strap units.

The conventional harness was instrumented using four load cells as shown in Figure A-14. Two of the transducers used were Lebow automotive belt load cells and two were harness hardware load cells.

SEAT PAN INSTRUMENTATION

The seat pan instrumentation measured both acceleration and load. The acceleration measurements were performed using three Endevco accelerometers, Model 2264-200. The accelerometers were mounted to a plastic block, $3/4 \times 1 \times 1$ inch, to form a triaxial package. This package

was secured to the seat pan assembly to indicate accelerations in the X, Y and Z axes as shown in Figure A-15. Figure A-4 shows the coordinate system utilized and the corresponding output polarity for an applied acceleration. Figure A-5 shows the specifications for the accelerometers used in this package.

The load measurements were made utilizing two types of load cells to fit the physical size limitations of the seat pan. Z-axis load measurements were taken using three Strainsert Flat Load Cells, Model FL2.5U-2SKPT. These cells were used in a three point mounting configuration as shown in Figure A-15. Specifications for these load cells are shown in Figure A-16. The X-axis and Y-axis loads were measured using load links specifically designed for this application by General Dynamics. These load links were instrumented with resistive strain gages as shown in Figure A-17. Each load link had four resistive arms with 2 arms active. Each end of the load links housed a swivel ball to eliminate cross-axis load effects on the measurements. The output polarity of each load cell corresponds to an applied load in accordance with the coordinate system shown in Figure A-9.

FOOT REST INSTRUMENTATION

The foot rest assembly, as shown in Figure A-18, was instrumented using three GSE load cells, Model T-10952C. These triaxial load cells were capable of measuring 2500 lb in the Z-axis and 500 lb in both the X and Y-axes. Figure A-19 illustrates the location and orientation of these load cells. The output polarity of each load cell corresponds to an applied load in accordance with the coordinate system shown in Figure A-9.

CARRIAGE INSTRUMENTATION

For acceleration measurements the carriage was instrumented with a triaxial accelerometer package. This package consisted of three accelerometers mounted to a $3/4 \times 1 \times 1$ inch block. The accelerometers used were all Endevco transducers with the following Model numbers and axis measurements; 2262A-200 for Z-axis, 2264-200 for Z-axis, 2264-200 for Z-axis.

Specifications for these accelerometers are shown in Figures A-20, A-5 and A-6 respectively. This package was securely mounted to the underside of the carriage. Figure A-4 shows the coordinate system utilized and the corresponding output polarity for an applied acceleration.

Carriage velocity measurements were obtained by means of a velocity wheel running against the rail. This unit consisted of a Globe Industries tachometer, Model 22A672, and a wheel mounted on its shaft. The wheel was aluminum with a rubber "0"-ring around the circumference. To insure continous rail contact the wheel assembly was spring loaded against the rail. The wheel was calibrated to output voltage as a function of velocity.

CALIBRATION

Strainsert Load Cells were calibrated on a periodic basis at the Precision Measurement Equipment Laboratories (PMEL), Wright-Patterson Air Force Base. The PMEL returns each device with a certificate providing current sensitivity and linearity data. Factory calibration data for the GSE Triaxial Load Cells were used for this evaluation program.

All accelerometers, load links, Lebow belt load cells and harness hardware load cells were calibrated at the AFAMRL/BBP Laboratory, Wright-Patterson Air Force Base. These calibrations were performed prior to (pre) and upon completion of (post) the evaluation program. This calibration data is shown in Figures A-21 and A-22.

Accelerometers were calibrated by using the reciprocity method to determine accelerometer frequency and phase characteristics as well as sensitivity. This method utilized a shaker table to which a "standard" accelerometer and the accelerometer to be calibrated were mounted. This "standard" accelerometer is calibrated yearly to standards traceable to the National Bureau of Standards. The sensitivity was determined by comparing the outputs of the standard and test accelerometer at 100Hz and 40G. The frequency and phase response was determined by driving the shaker table with a random noise generator and analyzing the output data by

Fourier Analysis via the PDP 11/15 and Time Data unit. The natural frequency and the dampening factor of the test accelerometer were both determined from this information.

The load cells mentioned previously in this section were all calibrated on a special test fixture. The sensitivity and linearity of each load cell was obtained by comparing its output with the output of a "standard" load cell output placed under an identical tension load. This "standard" load cell is calibrated on a yearly basis by standards traceable to the National Bureau of Standards.

SEAT GEOMETRY

The seat geometry drawings in Figure A-23 and A-24 show the polarity of the various output signals. Included in the drawings are the location dimensions for each fixed load cell and the variables introduced by the seat height and seat pan adjustment.

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•	dest dest	Endevco 2264- 150	188	2.416 mt/9	10.00	3/0	8/2	<u>-</u>	10.35g	120		305K +into gnd		
-	Chest 2		2820	2.577 aV/9	10.00	09	22/2	¥	38.809	120		155K - Into gnd		
•	Left Lap	MicroMea: EA06-125 RZ-350	613	14.93 uV/16	00.01	3	100		833 1b	120	<u>`</u>	39.5K - Into gnd		Used all tests through 406. Deck additional notes for subsequent use.
•	Right Lap		\$1.	13.71 uV/16	10.00	3	ĮŠ.	= -	41 706	320		40k - Into gad		Used all tests through 406. Check additional notes for subsequent use.
5	eN-6 Strap	1	143377	1.933 uV/16	10.00	3 01	01	<u>=</u>	1617 1b	120		470 K -Into gnd		Test 308 only Gain at 402
=	Left Seat Pan	Strainser 112.50- SPKT	£-162£	8.040 uV/1b	11,00.00	=	12	=	1547 3b	120				
21	Right Seat Pan		3294-4	7.988 uV/16 (tenston)	21 20 21	2	Q.	\ <u>-</u>	1557 16	130				
13	Seat Pan	•	3294-6	8.033 w/Jb	80.08	72	201	1-	1553 16	120		,		
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Cosput See .	ter start () lage 3 of 3	8 -3; off Q I for addit	tonal note	S On CORVE	Computer start B-3; off Q+1 See" Page 3 of 3 for additional notes on conventional harness use	mess use.								

Figure A-1 - Digital Instrumentation Requirements

		DIG	DIGITAL INS	INSTRUMENTATION)	REQUIREMENTS	ENTS							2-
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2	*Right Nicro-Meas ReflectionEA-06-125 Crean N7-150	Micro-Meas EA-06-125	01-3	¥.23 eV/16	0.00	3/2	8/2	<u>-</u>	729 16	82	8.0	20K -1ato gnd		
2	nertta 3	1600 3419-1.5K	, X	*8.03 uV/1b	0.00	91	200	<u>-</u>	74 16	120		•	•	Test 308 only Sens. 0 8.01 uV/lb
=	fight nertia kel Strap		×	J	s/	38 /	200	¥ \	969 1b	120	\cdot	•	•	Test 308 only Sens. 0 7.40 wy/lb
2	Sad Link	11cro-Mes. 3-26-262	98	10.80 uV/16	00.00	3 8	ğ _=	₹	576 1b	82		106K • Into gra	•	
62	Cod Lick	•	28	10.05 4/7b		61	20 CI	¥ /-	41 619	2,5		SSK - Into gra	•	
2	ced X	.10952C	ã	27.64 uV/1b	0.00	3	22 001	<u>-</u>	41 b0e	120		1	_	
ۃ	eft Foot oad Y		ã	28.61 uV/1b	0.00	3 3	3	<u> </u>	874 1b	120		•	•	
æ	eft foot 04d Z		ã	16.93 cr/?b	0.00	3 2	3/2	=	2953 16	120		•		
2	Pight Foot		200	8.5% 8.7%		3 8	30.	¥	862 16	120			•	
2	ight foot	•	79	28.78 E4/78	00.00	3/2	8 2	-	988 19	120			•	
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~	cen foot		68	28.08 47.75	6.00	3	80	<u>-</u>	930 38	120		•	•	
8	20 ~ Coot		8	36.50 eV/16	8.0	3	62 81	¥ \	3030 1b	120		•	•	
	Acterence page 3 of 3	e 3 of 3												•
اُ														101, 04

Figure A-2 - DIGITAL INSTRUMENTATION REQUIREMENTS

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×	Seat x	Endevco 2264-200	BW63	2.569 m//g	18.00 22	28	2	-_	19.469	82		397K -Into gnd	1.47K	"Test 308-340 SN. BMS, Sens. 0 2,990
я	<u>3</u> -		1 748		33	33	3	\ <u>*</u>	15.249	22		125K -Seto gnd	1.47K	
*	ž~		69463	6/Am	20.00 20.00	3	3/2/2	-\	17.77	22		512x -Into gnd	1.63K	
×	Center Load Link	A-06-062- J-350	\$	10.27 uV/16	75.00 35	3 ×	200	-\	91 909	28		62K • Into gad		
×	Carriage	Endevco 2264-200	BX49	2.561 114/9	10.00 X	3 %	8 8		19.52	120		127K - Into and	1.47K	
7	2.5 Volt Bias		•		10	88	12	- /	Z.5 Volt	360		٠		
2	10 Wolt Exc.		•	•	94	081	7.	- /	S Volt	360	0.0	•	•	10 Wolt divided by 2 atten.
	iert Lap	A-06-125 7-350	-15 Specto	14.10 uV/16	10.00	3	102	-/	dt 588	120	2.50	47K -Into gn	٠	Check additional notes for tasts used
6	Right Lap	•	Picads 91-	15.28 uV/16	10.00	6 09	6 102	- / =	814 16	120	2.50	19K -Into ged		Check additional notes for tasts used
iest (est	Conventional Harness Use: Left Lap SH.15, Chan B and Tests; H-G Strap, left and Tests: 407-416; 429-439;	One 8 a. Chan 8	Conventional Harness Use: Left Lap SM:15, Chan B and Right Lap SM:16, Chan Tests; H-6 Strap, left and right reflection stra Tests; 407-416; 429-439; 441-449.	ap SM. 16. (eflection s	Chan 9 used straps not	9 used in following ips not used in following	eing illaeing							
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Figure A-3 - DIGITAL INSTRUMENTATION REQUIREMENTS

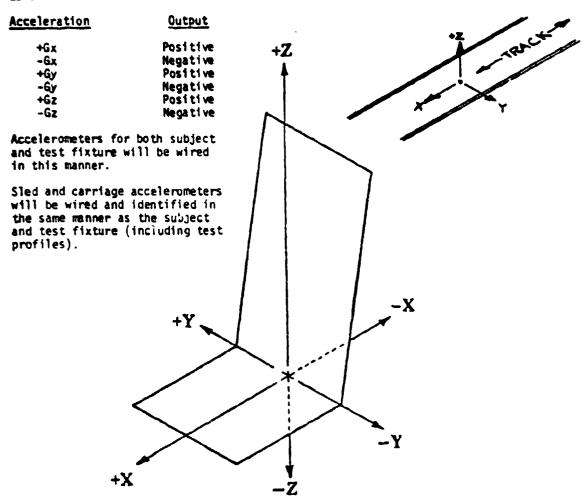
ACCELEROMETER COORDINATE SYSTEM

ACCELERATION

Accelerometers will be oriented and wired to provide an output corresponding to the applied acceleration. Use this table as a reference:

BARE SLED AND MACHINE TESTS

Accelerometers will be oriented to provide outputs to agree with track coordinate system with polarities as noted in test log.



AMRL BBP COORDINATE SYSTEM (Left Hand Rule)

Figure A-4

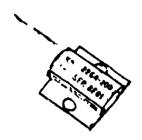
MODEL 2264-200

±200 g One gram **MINIATURE PIEZORESISTIVE ACCELEROMETER**

The Model 2264-200 is a very low mass, piezoresistive accelerometer designed for modal studies, flutter testing and similar applications requiring good low frequency response and minimum mass loading.

With only a small amount of damping, the Model 2284-200 has no phase shift over its useful frequency range of steady state to 1200 Hz. Protection against overranging results from the high environmental rating of ± 1000 g peak. The accelerometer can be operated over a temperature range of 0°F to 150°F (- 18°C to 66°C).

The 2264-200 utilizes Plezite® Element Type P-11 gages in a half bridge direuit providing a low imperiance nominal output of 500 mV full scale at 10 Volts de excitation.



SPECIFICATIONS FOR MODEL 2364-200 ACCELEROMETER

DYNAMIC

RANGE-200 g to +200 g

SENSITIVITY (at rated excitation)1. . 2.5 mV/g, nominal; 2.0 mV/g, minimum

HOUNTED RESONANCE FREQUENCY .

..... \$700 Hz, nominal AMPLIFICATION FACTOR, Q......10, maximum, at resonance and 75°F

TRANSVERSE SENSITIVITY 3% maximum

LINEARITY AND HYSTERESIS1 # 2% of reading, maximum, 0 to 150 g;

THERMAL SENSITIVITY SHIFT. ... ±40 mV max. at 0°F and 150°F (-18°C and 85°C), ref. 75°F (24°C)

WARMUP TIME1 minute

ELECTRICAL

EXCITATION

THERMAL ZERO SHIFT ± 40 mV max., at 0°F and 150°F (-18°C and 66°C)

INSULATION RESISTANCE! 10M LI minimum at 100 V de

stitleges may be used but should be specified at time of order. Use ENDEVCOV Model 4203 Power Sweety, or Mindel 4470 Signal Conditioning as distinction source. *Due to self heating of the plezorogetive ele-ments the measured resistance is sensitive to the applied voltage =2.5% of reading, maximum, 0 to 200 g.

NOTES

Measured between all leads lied together and

A STATE OF THE PARTY OF THE PAR

Massared with pickey stay, accountsion.

The shack measurements, werement pulse duration for half sine or tribinously pulses should exceed 1.5 milm-conds to avoid excessive high tre-dward frequing (See Endeuco Prezensiative Accelero Teser Manual.)

Unit a Caldrand at 100 V dc. Lawer accitation

ENVIRONMENTAL

ACCELERATION LIMIT'

(in any direction)

国的现在分词,我们就是这个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们

Static: ±1000 g.
Sinusoidal: ±1000 g pk.
Shock: ±1000 g pk, 1.5 millisecond duration or tonger.
CAUTION: Keep protective sleeve on accelerameter until roady to use.

TEMPERATURE

Operating: 0°F to 150°F (- 18°C to 66°C) Non-Operating: -65°F to 200°F (-54°C to 93°C)

HUMIDITY ALTITUDE

Epoxy Sealed Not Affected

Figure A-5 - Accelerometer Specifications

MODEL 2264-150

±150 g One gram

MINIATURE PIEZORESISTIVE **ACCELEROMETER**

The Model 2264-150 is a very low mass, piezoresistive accelerometer de signed for model studies, flutter testing and similar applications requiring good low frequency response and minimum mass loading.

With only a small amount of damping, the Model 2284-150 has no phase shift over its useful frequency range of steady state to 1200 Hz. Protection against overranging results from the high environmental rating of ≈ 1000 g seek. The accelerometer can be operated over a temperature range of 0"F to +150"F.

The 2264-150 utilizes Plezne® Element Type P-11 gages in a half bridge circuit providing a low impedance numinal output of 375 MV full scale at 10 Volta de excitation.



TWO TIMES ACTUAL SIZE

SPECIFICATIONS FOR MODEL 2264-150 ACCELEROMETER (According to ANS) and ISA Standards)

FUNDE	. – & w g xp → & v u g
SENSITIVITY (at rated excitation).	. 2.5 mV/g, nominel; 2 0 mV/g, minimum
MOUNTED RESONANCE	•
FREQUENCY	.4700 Hz, nominal
AMPLIFICATION FACTOR, Q	10, maximum, at resonance and 75°F
FREQUENCY RESPONSE	
(reference 100 Hz)	±10% max., 0 to 1200 Hz
	at +75°F (24°C)
TRANSVERSE SENSITIVITY	
LINEARITY	±2% of reading, maximum, 0 to 150 g;
	£2.5% of reading, maximum, 0 to 200 g.
THERMAL SENSITIVITY SHIFT	. ±10% max, at 0°F and +150°F.
	ref, +75°F
WARMUP TIME	. 1 minute
ELECTRICAL	
EXCITATION	10 0 V de
	17000 ± 20%, at +75°F (24°C)
ZERO MEASURAND OUTPUT	
ZERU BELASURANU UUTEUL	. Taking at max. #1 T/3 f

MSULATION RESISTANCE 10M D minimum at 100 V dc

temperature range

HOTES

ndy stare acceleration

Pla phash measurements, minimum pulse duration for held done or triagguer pulses should exceed 1.8 materials to every accessive high frequency ringing (See Ensevice Prairiespetare Accessive Manual).

Equipments (sound)

Albet to enthrolled at 10 0 V dc. Lamer spriblion
variages may be used but should be abecified at
time of order Use ENDEVCOP Model 4200 Power
Bapoly. ESS & riseasce. or Model 4200 Signal
Conditioning as provided a source.

"Due to call frequency of the preparations ele-ments, the measured recipiance is sensitive to the applied voltage

ENVIRONMENTAL

DVNAMIC

ACCELERATION LIMIT

 \pm 1000 g pk shock pulse, one millisecond duration or longer. CAUTION: Keep protective sietee on accelerometer until ready to use.

TEMPERATURE

Operating: 0°F to 150°F (-18°C to 66°C)
Non-Operating: -65°F to 200°F (-54°C to 93°C)

HUMIDITY

Epoxy Sealed

Figure A-6 - Accelerometer Specifications

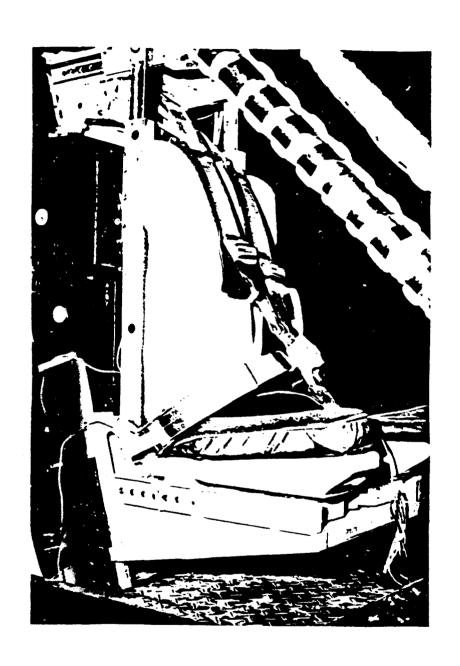


Figure A-7 - HARNESS ASSEMBLY (PROPOSED, MODIFIED F-111)

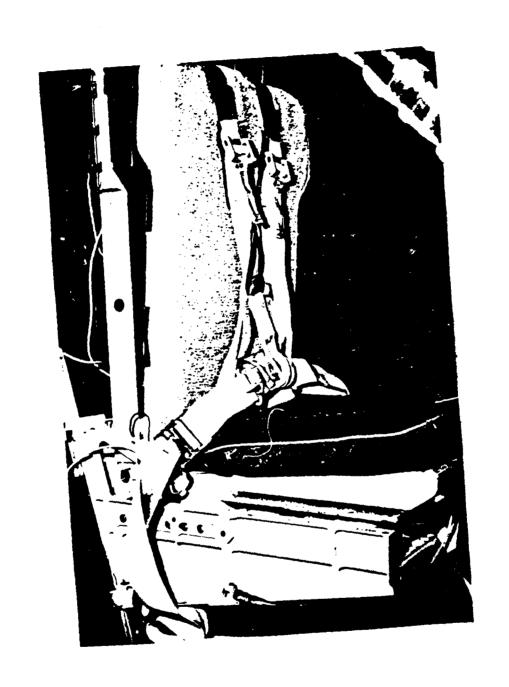
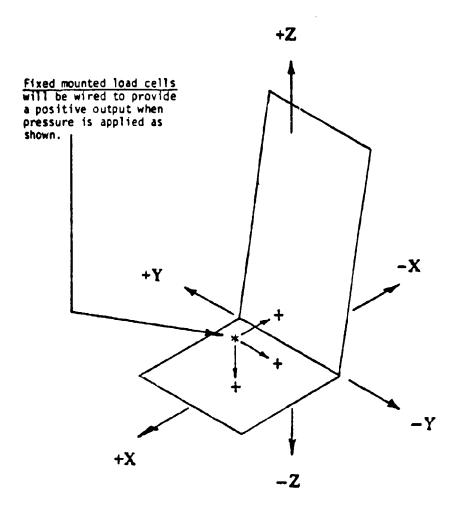


Figure A-8 - HARNESS ASSEMBLY (Conventional)

Swivel mount and Lebow belt load cells will be wired to provide a positive output when the belt is pulled.



AMRL BBP COORDINATE SYSTEM (Left Hand Rule)

Figure A-9

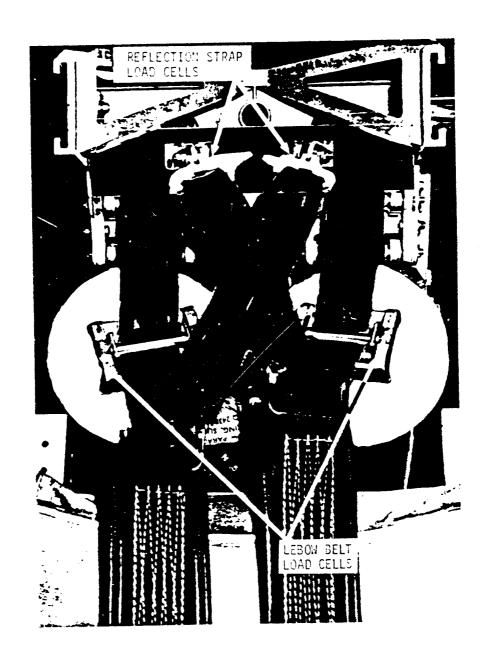


Figure A-10 - HARNESS INSTRUMENTATION

AUTOMOTIVE LOAD CELLS



Model 3419 Capacity Available 3500 lbs.

SPECIFICATIONS

Output at rated expacity: millivolts per volt, nominal	<u>+</u> 2
Nonlinearity: of rated output	<u>+</u> 2%
Hysterisis: of raced output	<u>+</u> 4%
Repeatability: of rated output	<u>+</u> 1.0%
Zero balance: of rated output	<u>+</u> 2%
Bridge resistance: ohms nominal	350
Temperature range, compeniated: ^O F	+ 30 to + 150
Temperature range, useable: ^O F	- 65 to + 200
Temperature effect on output: of reading per OF	± 0.003%
Temperature effect on zero: of rated output per OF	<u>+</u> 0.003%
Overload rating, sale: of rated capacity	150%
Excitation voltage, maximum: voits DC or AC rms	20
Insulation resistance, bridge/case: megohms at 50 VDC	1000
Belt thickness: (maximum) inches	0.10
Belt width: (maximum) inches	2.00
Weight: in ounces	8
Available capacities: pounds	3500

Figure A-11 - LOAD CELL SPECIFICATIONS

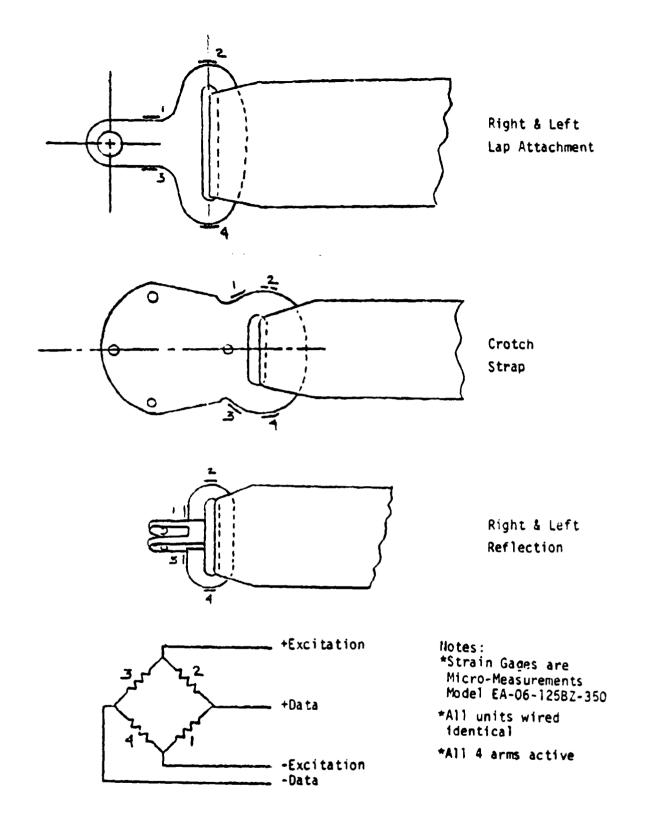


Figure A-12 - LOAD CELL SPECIFICATIONS (HARNESS HARDWARE)

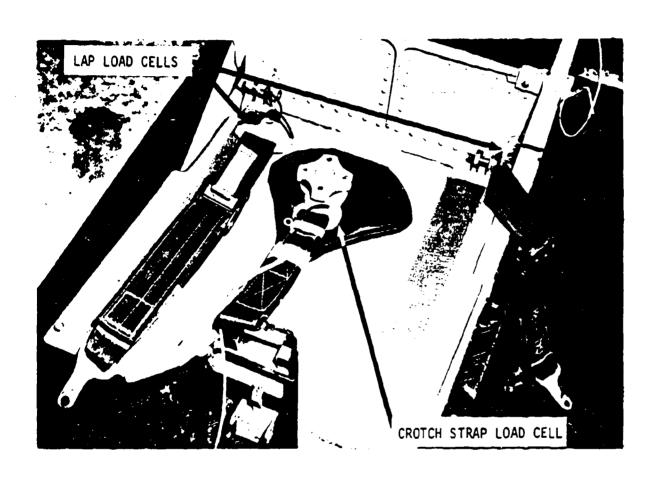


Figure A-13 - HARNESS INSTRUMENTATION (PROPOSED, MODIFIED F-111)

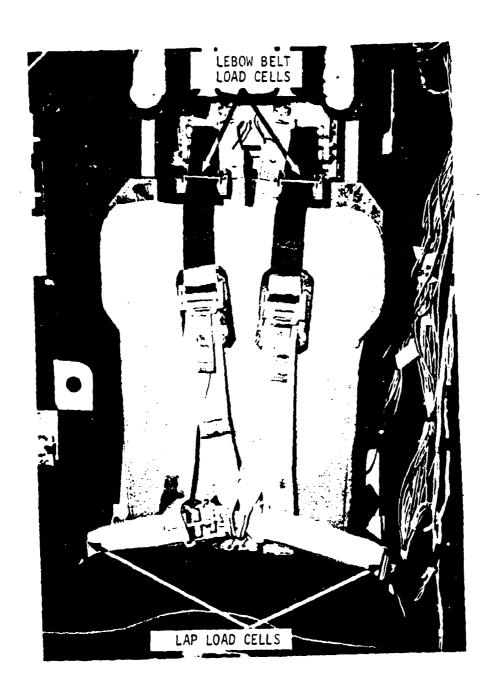


Figure A-14 - HARNESS INSTRUMENTATION (Conventional)

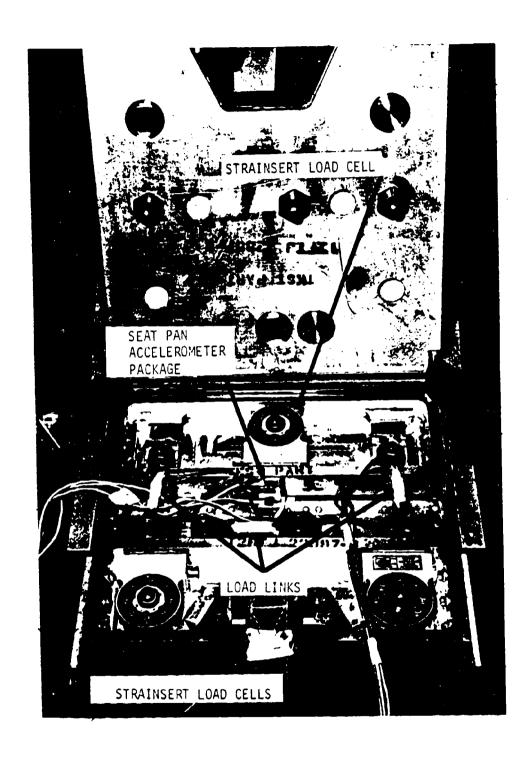


Figure A-15 - SEAT PAN INSTRUMENTATION

STRAINSERT CALIBRATION DATA

U.S. Air Force Wright-Patterson AFB Dayton, Ohio Q-3294 Strainsert Job No.

Strainsert Job No.

Customer P.O. No. F33-601-76-86950

Date: 10/16/76

Sign: CGH

Transducer: Universal Flat Load Cell, Model FL2.5U-2SPKT

2,500 lb. Capacity, 2 mv/v, 350 Chms

Gages: EA-06-104ZA-175 Service Temp.: 150°F Max. Calib. Temp.: 73°F Type: C (Bendix PT02H-10-6P)
Ins. Res.: Over 10,000 megohms-

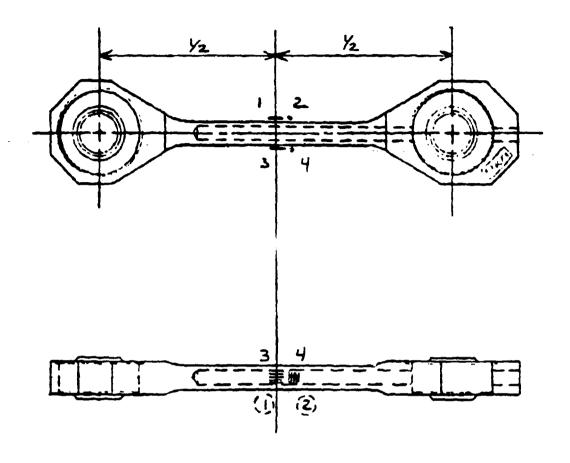
S/N: Q3294-6

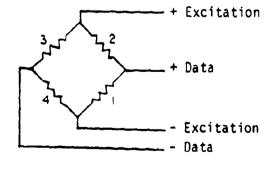
Load	Straight Line	Dev	iation,	μ ν/ν	Rep.
LBS.	Signal Mv/v	Run 1	Run 2	Run 3	μ ν/ν
0	, 0	0	0	0	0
500	0.400	- 15	0	0	1/2
1,000	0.800	+15	+15	+35	. 0
1.500	1.200	0	0	0	0
2,000	1.600	-1	-1	-1	0
2,500	2.000	- kg	- l _ž	-15	0
2,000	1.600	-1	-15	_ l _š	1.5
1,500	1.200	+1	+1	+1	0
1,000	0.800	+115	+ 15	+) ¼	0
500	0.400	+ 14	+1	+1	<u> </u>
	0	0	0	0	0
	Hysteresis	1 1	1 1	1	

Calibration Analysis:						
Non-Linearity:	1	parts	1 n	2,000		. 05%
Repetition						
Loading :	l _s	parts	1 n	2.000	-	. 03%
Unloading:	l _s	parts	in	2.000	•	. 03%
Zero Load:	ŏ	parts	1 n	2,000	•	
Max. Load:	0	parts	i n	2,000	•	
End Point :	. 15	parts	in	2,000	•	.03%
Hysteresis :	1	parts	in	2,000		.05%

Hold Down Bolts: 10-32NF; Torque = 6 ft. 1b. lubricated

Figure A-16 - LOAD CELL SPECIFICATIONS



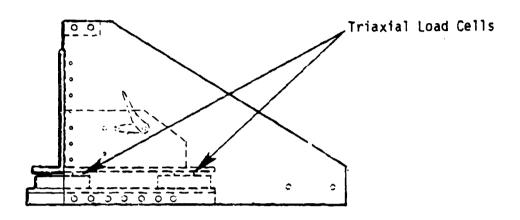


NOTES: *Strain Gages are Micro-Measurements Model EA-06-062TJ-350 *Z arms active

Figure A-17 - LOAD CELL SPECIFICATIONS (LOAD LINK)



Figure A-18 - FOOT REST ASSEMBLY



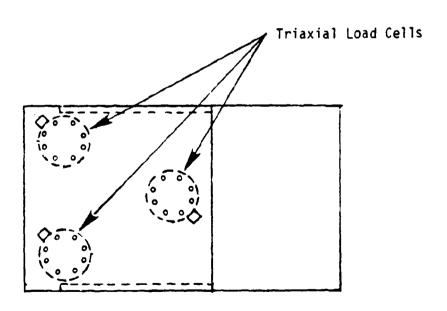


Figure A-19 - FOOT REST LOAD CELL LOCATIONS

2262A-200 2262CA-200

Damped, Overload Stops

PIEZORESISTIVE **ACCELEROMETERS**



SPECIFICATIONS FOR MODEL

2262A-200 and 2262CA-200 ACCELEROMETERS

DYNAMIC

RANGE

OVERRANGE LIMITING

SENSITIVITY

MOUNTED NATURAL FREQUENCY (AT 75°F)

FREQUENCY RESPONSE

DAMPING RATIO

TRANSVERSE SENSITIVITY

THERMAL SENSITIVITY SHIFT

LINEARITY AND HYSTERESIS

ELECTRICAL

EXCITATION

INPUT RESISTANCE (AT 75°F)

OUTPUT RESISTANCE (AT 75°F)

INSULATION RESISTANCE

ZERO MEASURAND OUTPUT

.200 g to 200 g

Models 2262A-200 (2252CA-200)*

1300 to 11 200 g

25 mV/g typical (1.2 mV/g typical)

2 mV/g minimum (1 miV/g minimum)

7 000 Hz typical

:5% maximum 0 to 3 000 Hz a: 75°F: -35%/10% typical at 0:200 °F and 3 000 Hz

0.7 typical

3% maximum

.2% of reading, maximum,

to 200 g

10 00 Vdc

1 600 1: typicat (1 000 1: typical)

1 200 :: typical (1 000 :: typical)

100 G:: minimum

t25 mV maximum

FHVIRONMENTAL

ACCELERATION LIMITS (In any direction)

Static 2 000 g Sinusoidal 1 000 g pk Shock 2 000 g half sine pulse

TEMPERATURE

Compensated 0°F to +200°F (-18°C to +93°C) Nonoperating -20°F to +220°F (-29°C to +104°C)

YTIOINIUH

Sealed by glass to metal fusion and welding.

0°F to -200°F

Figure A-20 - ACCELEROMETER SPECIFICATIONS

PROCRAM Head Rest Position Study

VOT FACTLITY RUN NO'S 308-449

DATE 1 July 80

		Π	d dive				-,,			,,,	due.	Pes				
	ONMENTS		Tests 308-424 only - removed due	to excessive zero shift.							Tests 308-340 only - removed due			Tests 425-449 Only	Tests 341-449 Only	
			٢					•			4	2 :	<u>}</u>	<u>-</u>	<u> </u>	
	A CHANGE	4.8	-	+.2	7.1	:	+	7	+.6	9. 1+	9.	+.5	4.	+,3		
כאר	SVAS	2.581	2.757	4.147	2.496	2.713	2.553	2.786	2.430	2.619	2.964	3.298	2.825	2.354	2.564	
POST CAL	DATE	30 Sep 80	*	•				29 Sep 80			03 Oct 80			30 Sep 80	03 Oct 80	
JY.	SENS	ì	2.767	4.138	2.462	2.709	2.550	2.702	2.416	2.577	2.990	3.280	2.814	2.346	5.569	
PRE CAL	DATE	17 Mar 80	2	15 Hay 80	25 Jun 80							*		08 Sep 80	25 Jun 80	
X /S		8 X 4 9	8756	FR42	BP10	BQ42	1508	BC26	8813	2A20	8795	BV41	BN63	1188	8V63	
IKANSDUCEK	MFG & MODEL	Endevco 2264-200	*	Endevco 2262A-200	Endevco 2264-200	evco 2264-200	*	avco 2264-150	ī	z	evco 2264-200	8	8	NCO 2264-150	8VCD 2264-200	
	+	End			Ende	Endevo		Endevco			Endevo			Endevco	Endevo	
DATA POINT		Carriage X	Carriage Y	Carriage 2	Head X	Head Y	Head 2	Chest X	Chest Y	Chest Z	Seat X	Seat Y	Seat 2	Carriage Y	Seat X	

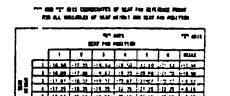
Figure A-21 - PROGRAM CALIBRATIONS (PRE AND POST)

PROGRAM Head Rest Position Study

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_	TRAISDUCER	2	PRE CAL	JS.	POST CAL	ะ	J. Grand	STATIONS
DATA PUINT NEG 5 NO	MODEL	E /d	DATE	357h	DATE	JVNs	A CIMINE	Civiliano
LF. Load Link X 1991 EA-26-0	062-13-	- - -	26 Jun 80	10.80	03 Oct 80	10.79	:	
Rt. Load Link X 350		200		10.05	•	10.11	9.+	
Centoad Link Y		8	•	10.27	•	10.23	4:	
Left Lap M EA-06-12582-350 13)\$E-28521) 13			02 Oct 80	15.10	1.1	
Right Lap		=	:	13.71		13.66	4.	
M-G Strap		143377	30 Jun 80	1.933	03 Oct 80	1.800	6.9-	
of Reflec.Strap		01-20	26 Jun 80	26.11	02 Oct 80	26.32	a: +	
Rt Reflec.Strap		01-3	•	34.29		34.04	7	
f inert R.		363	30 Jun 80	8.01	:	7.86	6.1-	
Strap Strap		364	27 Jun 80	7.401		7.54	41.9	
Left top		15	10 Jul 80	14.10	•	14.39	+2.1	
Right Lap	_	91	18 Aug 80	15.28	ı	15.35	+.5	

Figure A-22 - PROGRAM CALIBRATIONS (PRE AND POST)



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Figure A-23 - SEAT GEOMETRY

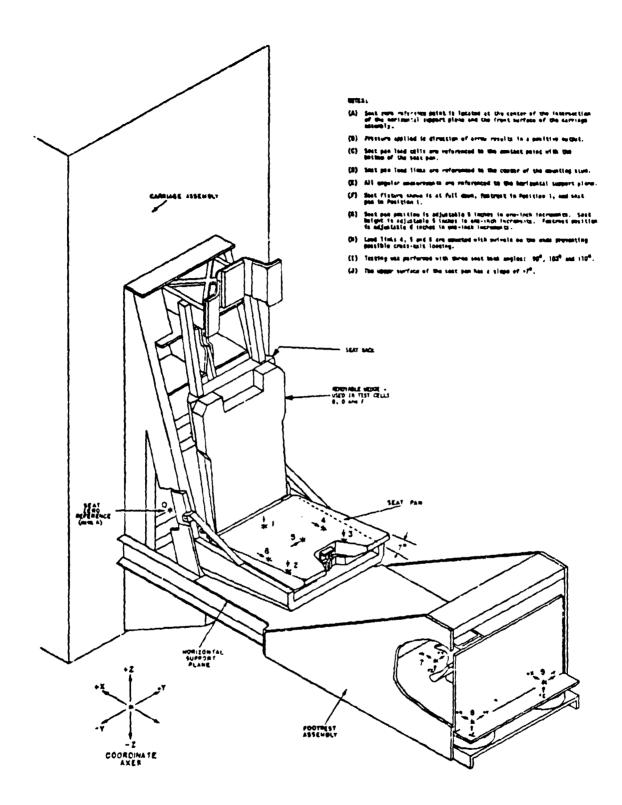


Figure A-24 - SEAT GEOMETRY

AUTOMATIC DATA ACQUISITION AND CONTROL SYSTEM

CARRIAGE DIGITAL DATA ACQUISITION SYSTEM EQUIPMENT

Figure A-25 is a photograph of the Carriage Digital Data Acquisition System. Figure A-26 shows the block diagram of the Carriage Digital Data Acquisition System. This system consists of four parts: the power conditioner, the signal conditioner and sensors, the encoder and the junction box. The power conditioner requires a 28 vdc, 4A power source and provides several regulated supplies. They are the +15 and -12 vdc (0.8A) supply for the signal conditioners, the 5 vdc and the 10 vdc bridge excitation voltages (1.2A total), and the 2.5 vdc signal output bias voltage (0.1A). The 28 vdc source also powers the pulse code modulator (PCM) encoder (0.24A).

The signal conditioner consists of 48 signal modules. Each module is capable of processing a sensor (transducer) signal which can be a voltage generating source or a bridge-type sensor. If a bridge-type sensor is used, the bridge excitation voltage is selectable from the 5V or the 10V source. By connecting the proper external resistors to the module input connector a half bridge is completed. A full or half bridge is balanced by connecting external resistors to its module input connector.

The signal conditioning module consists of a amplifier section and a filter section. The amplifier gain can be selected by inserting one of seven external gain plugs. These gains provide the capability of covering an input dynamic range from 50 mV up to 5 V. The filter section can be programmed by inserting one of four external filter plugs. These filter plugs are in accordance with the SAE recommended classes 60, 180, 600 and 1000.

The 48 channel data signals are time multiplexed and digitized via an encoder into 48 11-bit digital words. Two additional 11-bit synchronization (sync) words are added to the data frame. The 50-word frame is then sampled at a rate of 1000 samples/second. These serial digital data along with three additional synchronization pulse trains (bit sync, word sync, and frame sync) are connected to the computer room by four twisted pairs incorporated into a drag cable. They pass through a junction box to the digital computer interface to allow recording and processing.

PDP 11-34 DATA COLLECTION AND STORAGE

The PDP 11-34 minicomputer is the main control for all electronic data collection and storage functions. The block diagram of Figure A-27 shows the processor and its related equipment. All data transfer in the data collection system are under software control by the central processor unit. Serial data are constantly being received by the data formatter unit from the carriage data encoder. These data are converted by the data formatter from serial to parallel for input via a buffered data channel to computer memory for storage on disk. Finally, the data are transferred from disk to magnetic tape for permanement storage following the test event.

OUICK LOOK INERTIAL DATA

After each test, the data were sampled and checked. This check was made using the Single Channel ANalysis (SCAN) routine for the PDP 11-34 processor. This routine allows the operator to access and plot up to 2000 points of data for any of the 48 data channels. The operator selects the channel to be processed and enters its location description as well as the start and stop points to be processed. A maximum of 2000 milliseconds or 2000 data points may be accessed for each plot. The program converts the raw data into the appropriate units of measure and calculates the minimum and maximum values during the sample interval. If the sample is acceleration data, the velocity will also be calculated using an integration process.

An added optional feature is a digital smoothing routine which can smooth the data to remove any excess high frequency component that may be present.

FOOT REST AND SEAT PAN CORRECTION

Dynamic foot and seat pan loads were corrected by removing the effects of the foot support fixture and seat pan loading on supporting load cells.

A series of tests was conducted to determine the percentage of the total force resting on each cell. The weight assessed each load cell and multiplied by the carriage acceleration was subtracted from the acquired test data in the processing.

In practice, the load cell outputs are zeroed with the foot support fixture and seat pan weight resting on the load cells. During a drop, with no payload, the sum output of the load cells would reflect the weight of the fixture as a negative load (fixture weight removed from the load cell). The data were processed to remove this effect and thus reflect a zero output during a drop with no payload.

The final foot and seat pan loads were processed to provide corrected values which represent actual loads encountered by the human or dummy subjects.

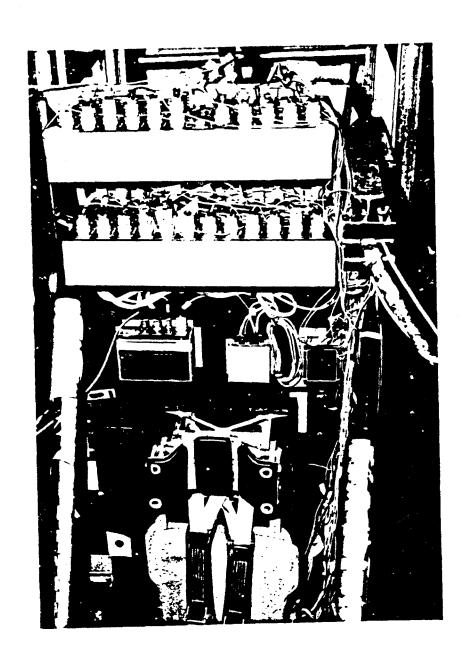


Figure A-25 - CAPRIAGE DIGITAL DATA ACQUISITION SYSTEM

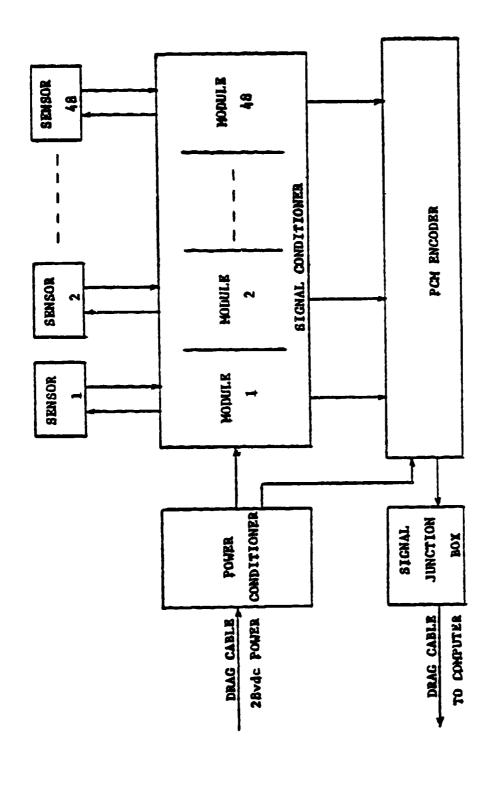


Figure A-26 - CARRIAGE DIGITAL DATA ACQUISITION SYSTEM BLOCK DIAGRAM

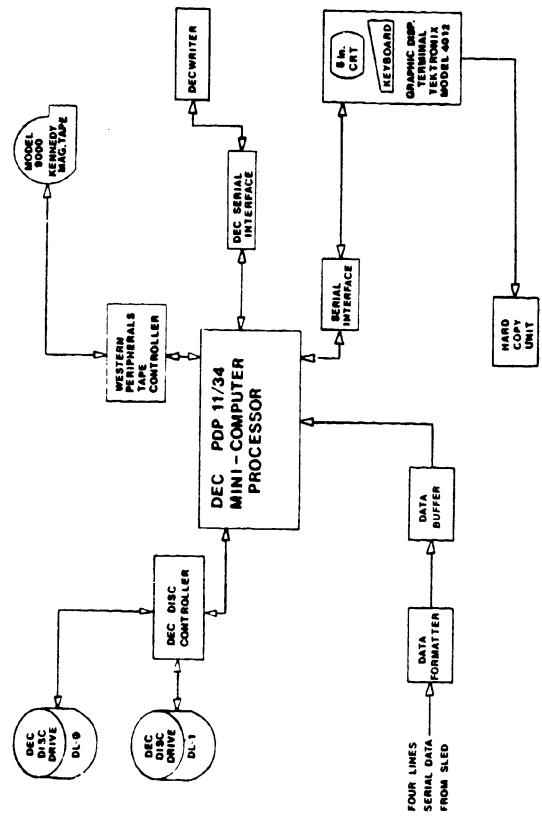


Figure A-27 - CENTRAL DATA ACQUISITION AND STORAGE SYSTEM

KINEMATIC DATA ACQUISITION SYSTEM

HIGH SPEED CAMERAS AND CONTROL

Kinematic data were acquired through the use of high speed 16mm cameras operating at a rate of 500 frames per second. The cameras were Teledyne Milliken Model DBM45 pin registered units which were capable of withstanding 25 G. Two cameras were mounted to the carriage, one to provide a frontal view and one to provide a right lateral view of the subject. During a test the cameras were started and stopped automatically by the Camera and Lighting Control Station which is part of the impact facility safety and control system. The cameras were started at a preset time in the test sequence and run for a period of 8 seconds.

AUTOMATIC FILM READER

The AFR subsystem was developed by Photo Digitizing Systems, Inc. It automatically extracts photo data, digitizes it and records it on magnetic tape. The subsystem consists of:

Film motion analyzer with 16mm projection head Electronic scanning camera
Control Unit
Alphanumeric Cathode Ray Tube (CRT)
Line printer
Magnetic tape transport

The film reader recognizes quadrant or circular fiducial targets. It automatically tracks targets and extracts data for up to twelve targets per film frame at a minimum rate of one-half frame per second. Film may be processed through the reader manually or automatically.

Figure A-28 is a block diagram of the Automatic Film Reader System (AFR). The X-Y coordinate position of each target on each film frame is input to the computer and recorded on magnetic tape.

A NOVA 3/12 computer controls the AFR which contains 16K, 16-bit, words of core memory, a CRT terminal, and a magnetic tape transport with suitable interface. In addition, a parallel data link is provided between the NOVA 3/12 and the PDP 11/34.

An alphanumeric CRT (DGC 6052) automatically displays the AFR control information. The CRT display and its keyboard function are used as separate devices. The keyboard is a transmit-only device and the display is a receive-only device but has the additional capability of transmitting cursor position information on program request.

A hard copy device, LA36 Decwriter II, provides hard copies of the information presented on the 6052 CRT. The LA36 is medium-sized interaction terminal with a low-speed impact printer and a standard ASCII keyboard consisting of alphanumeric characters and non-printing system control codes.

Either the Decwriter or the 6052 CRT output may be assigned to the PDP 11/34A. Programs can also be established which can "down load" from the disc on the PDP 11/34A to the NOVA, or digital film data can be loaded on the PDP 11/34A for processing or disc storage.

OUICK LOOK KINEMATIC DATA

The Instar (Instant Analytical Replay) System is a high-performance video recorder and display device designed for the analysis of high speed motion. It is a compact, portable, fully transistorized instrument that combines the long recording capacity and instant replay features of video tape. The system records 120 frames/second with an effective shutter speed of 10us or less and will playback all recordings in real time, stop action, reverse slow motion, and variable slow motion (2%-15% of real time). Each of the frames is sequential and non-interlaced.

Instar incorporates two cameras and a special effects generator for the added flexibility of split screen. The simultaneous display of two events offers the precise evaluation of three dimensional problems

or the referencing of one physical event to an instrument (i.e., dirital clock or oscilloscope). Other features include:

End of tape sensing
Foolproof logic control sequences
Dynamic braking
Interscene blanking
Video logic signal processing modules

The Instar System was utilized to record each impact event. This video tape was available for review by the test conductor and/or medical monitor immediately after the impact event.

TIMING REFERENCE

A 100 PPS timing signal was an intergral part of the Kinematic Data Acquisition System. The Camera and Lighting Control Station started the timing signal at T = 0. An event signal was generated less than one second after T = 0. This event signal performed two functions. It triggered a photo flash unit which marked the film frame at the beginning of the impact event. Second, it started the 100 PPS signal to the LED drivers, LM Dearing Model 2/3/3R. The LEDs, located in the high-speed cameras, were pulsed every 10 ms which produced a .75 ms timing bar on the edge of the film. The diagram of Figure A-29 shows the 100 PPS signal, the event signal and the LED driver signal. Figure A-30 illustrates the event and timing bar in relationship to the film.

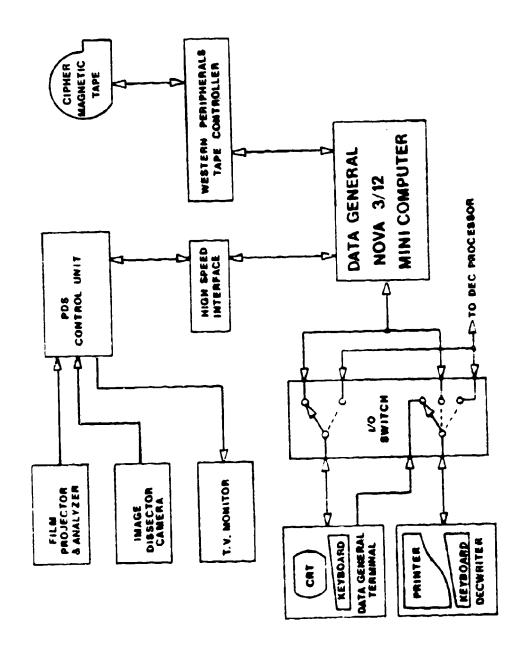


Figure A-28- AUTOMATIC FILM READER SYSTEM BLOCK DIAGRAM

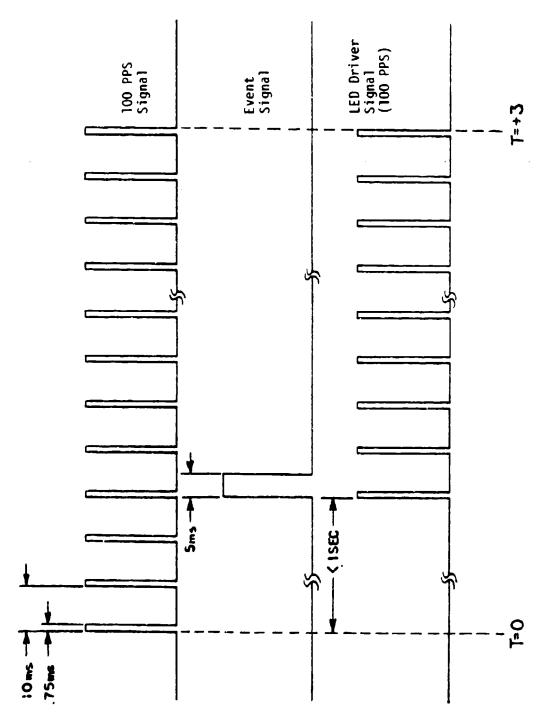


Figure A-29 - TIMING REFERENCE

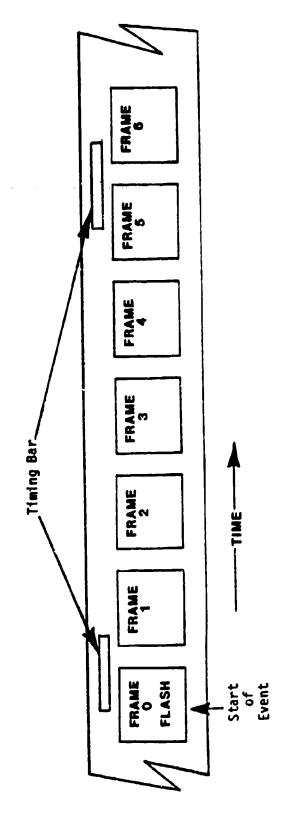


Figure A-30 - TIMING REFERENCE

APPENDIX B SUMMARY OF ELECTRONIC DATA

The means and estimated standard deviations of all peak measured and computed parameters from each cell of experimental matrix are shown in Table B-1. (The cell designations are explained in the experimental design matrix, Table 1, in the body of the report.) In addition, the maximum and minimum values of each parameter are tabulated for each test conducted at the experimental level. The times at which these values were achieved during the impact are also tabulated. These data are grouped according to test condition. Finally, a set of analog data from each test condition is presented. To permit comparability among these data, the test results of the same subject, S-3, are shown in each test condition. This subject was selected because his tabulated maxima and minima in each of the three tests were not beyond 2.5 standard deviations of the mean and because the subject's body weight, standing height, and sitting height were close to the means of those anthropometric measurements for the sample under investigation. (See Table 2.)

All electronic data derived from this test program will be maintained by the Biomechanical Protection Branch of AFAMRL until this work unit is retired. These experimental results will eventually be recorded in a permanent data bank within the Laboratory.

TABLE B-1

SUMMARY OF ELECTRONICALLY MEASURED AND COMPUTED DATA

(Peak values are tabulated for velocity, accelerations and loads.)

MATRIX CELL RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	A MODIFIE HANDS-O FORW	D F-111 N-KNEES ARD		B- MODIFIED F-111 HANDS-ON-KNEES AFT (n = 14)		
	(n =					
CARRIAGE ACCELERATION (G)	MEAN 10.6	ST DEV		MEAN 10.5	ST DEV	
CARRIAGE VELOCITY (ft/sec)	-25.7	0.13		-25.7	0.11	
SEAT ACCELERATION (G)	10.6	0.18		10.6	0.18	
CHEST ACCELERATION (G)	••••	0.10		10.0	0.10	
-X axis	-1.56	0.75		-1.45	0.80	
+X axis	4.29	1.66		4.21	and the same of th	
+Z axis	18.3	4.14		19.5	4.23	
Resultant	18.7	3.97		19.8	4.11	
CHEST SEVERITY INDEX	31.1	6.86		34.1	6.84	
HEAD ACCELERATION (G)					l i	
-X axis	-4.70	1.02		-2.04	1.29	
+X axis	1.04	0.95		1.97	1.16	
+Z axis	13.1	1.03		13.1	0.98	
Resultant	13.3	1.04		13.3	0.92	
HEAD SEVERITY INDEX	19.7	2.15		20.2	2.14	
STRAP LOADS (1b)	0.5	22		0.4		
Reflection Straps	95 95	23 29		94 81	21	
Inertia Reel Straps	181	29 54		165	24 48	
Total Shoulder Straps Total Lap Belt	106	23		99	24	
SEAT PAN LOADS (1b)	100	23	ł	23	24	
-X axis	-263	69		- 250	72	
+Z axis	1640	235	ł	1640	207	
Resultant	1660	238		1660	210	
FOOTREST LOADS (1b)	1					
-X axis	-536	149		- 525	163	
+Z axis	541	82		545	82	
Resultant	710	165		719	161	

TABLE B-1 (continued)

SUMMARY OF ELECTRONICALLY MEASURED AND COMPUTED DATA

(Peak values are tabulated for velocity, accelerations and loads.)

MATRIX CELL RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	MODIFIED HANDS-IN FORWA	N-LAP	MODIFIED HANDS-IN AF	N-LAP
HEADREST FOSTITOR	(n =		(n =	
	MEAN	ST DEV	MEAN	ŠT DEV
CARRIAGE ACCELERATION (G)	10.5	0.13	10.6	0.16
CARRIAGE VELOCITY (ft/sec)	-25.8		-25.7	
SEAT ACCELERATION (G) CHEST ACCELERATION (G)	10.6	0.14	10.6	0.19
-X axis	-2.08	0.97	-2.08	0.89
+X axis	4.47	1.30	3.79	1.21
+Z axis	20.0	3.02	18.5	3.43
Resultant	20.4	2.91	18.8	3.43
CHEST SEVERITY INDEX	35.2	5.94	32.7	6.83
HEAD ACCELERATION (G)				
-X axis	-4.83	0.95	-2.01	1.53
+X axis	1.25	0.98	2.69	1.35
+Z axis Resultant	13.2	0.92	12.7	0.85
HEAD SEVERITY INDEX	13.4 19.7	0.92 2.20	13.0 20.4	0.96 1.43
STRAP LOADS (1b)	19.7	2.20	20.4	1.43
Reflection Straps	104	25	109	20
Inertia Reel Straps	112	28	105	25
Total Shoulder Straps	206	54	210	44
Total Lap Belt	92	27	95	17
SEAT PAN LOADS (1b)	1			
-X axis	-285	70	-269	63
+Z axis	1730	220	1710	212
Resultant	1760	222	1730	214
FOOTREST LOADS (1b)				
-X axis	-387	121	- 398	90
+Z axis	465	74	484	75
Resultant	551	121	592	108

TABLE B-1 (continued)

SUMMARY OF ELECTRONICALLY MEASURED AND COMPUTED DATA

(Peak values are tabulated for velocity, accelerations and loads.)

			-	F		
MATRIX CELL	CONVENTION	VAL		CONVENTION HANDS-IN-	NAL LAP	
RESTRAINT HARNESS	HANDS-IN-	-AP	•	AFT	1	
BRACING POSITION	FORWAR	2	- [(n = 1)	2)	
HEADREST POSITION	(n = 1)	3)	1	MEAN	ST DEV	l
	MEAN	ST DEV	1	10.5	0.11	1
CONTRACTION (C)	10.5	0.16	- 1	-25.7	0.17	l
CARRIAGE ACCELERATION (G)	-25.8	0.14	1		0.10	l
CADDIAGE VELOCITY (TT/Sec)	10.6	0.17	1	10.7	0.10	ŧ
SEAT ACCELERATION (G)		Į.	1	1 06	0.97	į.
CHEST ACCELERATION (G)	-2.28	0.94	1	-1.86	1.62	1
-X axis	3.93	1.43	1	4.95	2.83	Ì
+X axis	20.2	3.31	. 1	19.5	2,71	1
+Z axis	20.5	3.23	1	19.9	5.47	}
Resultant	41.1	6.75		40.8	3.47	1
CHEST SEVERITY INDEX	12.0			0.63	1.66	1
HEAD ACCELERATION (G)	-4.44	1.13		-2.63	1.76	1
≈X axis	1.56	1.31	1	2.62	1.44	1
+X axis	14.7	1.32	Ì	14.8	1.55	1
+Z axis	15.0	1.37	ì	15.1	3.12	ł
Jacultant	24.3	2.75	1	26.7	3.12	1
HEAD SEVERITY INDEX			1	1	22	1
CTRAP LOADS (1D)	146	39	1	137	33 27	- 1
Total Shoulder Straps	108	23	1	116	21	1
Total Lap Belt	100		1			- 1
SEAT PAN LOADS (16)	-319	75	1	-308	63	- 1
-X axis	1820	247	1	1790	282	- 1
+Z axis	1850	253	1	1820	284	- 1
Resultant	1030		1	}	100	1
FOOTREST LOADS (1b)	-430	123	İ	-430	100	1
-X axis	476	81	1	473	59	ł
+Z axis	609	136	1	603	94	
Resultant	003					

HEAD REST POS STUDY	TEST: 399	SUBJ: D-1	MT: 212.0	G: 10	GP: 1 CELL:	A
DATA ID		HAX	MIN	T 1	15	CH
TOTAL LAP PAN Z Z Z SEAT Y SEAT PAN Z Z Z SEAT X TOTAL LAP PAN Z Z Z SEAT X SEAT SEAT COLLERT FORCE SEAT X TOTAL LAP PAN Z Z Z X SEAT X Z Z Z X SEAT Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X Z Z Z X SEAT X SEAT FORCE X X X Z Z Z X X X Z Z Z X X X X Z Z Z X X X X Z Z Z X X X X Z Z Z X X X X X Z Z X X X X X Z Z X X X X X X Z Z X	T	0.5008117979106580400759663447002887477150552173407721829761518008110010101010101010101010101010101	9.6841617774512899 5111 09909054866199677235250195812150790905486619967723525019581318089393119557100.23.0.318.35550697007188777188089393919557195812180893939195812818181818181818181818181818181818181	00000000000000000000000000000000000000	3858.000 38683.000 38685.000 38677.000 38777.000 38777.000 38777.000 38778.000 38778.000 36928.000 3	4831 9234 567 234 46 57 89 089 5123 035 147 258

		MT. 165 N	G: 10 GP	: 1 CELL:	A
HERD REST POS STUDY TEST: 363	SUBJ: 1-3	MIN NIN		57	CH
DATA 10		• •	1517.00	1923.00	48
104 EXT PHR	10.05 1.78	9.96 -1.54 -1.18	3830.00	3843.00 3614.00	3 j
CARAIAGE X CARAIAGE T CARAIAGE Z	0.45 12.19 10.42	-0.25 -0.09	3862.00 3862.00	3750.00 3749.00))
CARRIAGE Z (SM) CARRIAGE VEL	-0.89 2.41	-25.72 -1.48	4193.00 3828.00	3826.00 3841.00 3837.00	29 32 33
SEAT X SEAT Y	0.87 11.14	-1.07 -0.28	3867.00 3867.00 3868.00	3654.00 3763.00	94
SEAT Z (SM)	10.28 2.36	-0.17 -2.35 -1.69	3841.00 3935.00	3911.00 3865.00	5 6 7
CHEST X CHEST Y CHEST Z	0.19 17.36 17.48	-0.95 0.95	38 90.00 3 8 90.00	9766.00 4181.00	- "
CHEST RES CHEST SI	91.60	-3.29	3827.00 3871.00	3965.00 3922.00 3895.00	3
HEAD X HEAD Y	2.36 11.97	-0.41 -1.40 0.78	4087.00 3880.00 3881.00	9694.00 4116.00	ų
HEAD Z HEAD RES	12.01	0.76	3839.00 3856.00	3948.00 3929.00	14
HEAD SI HEAD HIC SHD REFL LF	13.63 60.29 58.01	17.25	3917.00 3913.00	4092.00 3884.00 3882.00	16
SHO REEL LY LE SHOULDER	114.88 71.57 87.15	36.44 31.30	3914.00 3901.00 3905.00	3963.00 3874.00	15 17
SHD REFL RT SHD REEL RT	156.15	15.34 60.87 61.58	3904.00 3903.00	3873.00 4100.00	
RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL	126.45 130.98 251.87	22.62	3911.00 3909.00	3874.00 3874.00 3874.00	
TOTAL SHOULDER	53.33	0.61	3909.00 3974.00 3971.00	3871.00	8 9
LF LAP BELT	47.53 100.12	15.74 30.40 0.18	3973.00 3973.00	3872.00 3872.00	
TOTAL LAP TOTAL LAP / NT CROTCH STRAP	0.61 90.45 38.42	-27.49 -181.46	3977.00 3975.00	3876.00 3883.00	10 18 19
LF SEAT LNK X	29.44 42.19	-87.48	3635.00 3768.00	3876.00 3876.00 3884.00	35
TOTAL SEN! A	นูย.68 นู1น.99	18.00	3936.00 3884.00 3878.00	3631.00 3604.00	15
SEHIT PAN Z RT SEAT PAN Z CT SEAT PAN Z	309.34 820.43	50.34	3884.00	9890.00 9604.00	1 3
TOTAL SERT Z HT	1534.20 9.30 1556.65	0.54	3884.00 3884.00	3604.00 3604.00	
RES SEAT FORCE / NT	9.43	0.59 189.61	3831.00	3604.00 3639.00 3886.00	53 50
LF FOOT X AT FOOT X	28.36 21.99	-163.// -197.18	30300		26
ČÍ FOOT X TOTAL FOOT X	50.57 156.7	9 -25.77	3872.00 3700.00	4111.00 3863.00	21 24 27
LF F00T T AT F00T T CT F00T T	25.9° 24.0 30.3	-38.29 -63.63	3831.00 3849.00	3838.00	
TOTAL FOOT T	195.2	7 ~32.45 7 15.69	3881.00	3840.00	22 25 28
AT FOOT Z	188.7 527.2	u -155.00 2 -120.5	3881.00	3821.00	
TOTAL FOOT Z RES FOOT FORCE	728.4	4 100.0			

HEAD REST POS STUDT	1EST: 398	SU8J: F-2	HT: 160.0	G: 10	GP: 1 CELL:	R
DATA LO		MRX	MIN	T1	12	CH
10V EXT PWR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z (SM)		10.05 1.49 1.00 12.47	9.97 -0.76 -1.06 -0.14	2573.00 3834.00 3835.00 3828.00	760.00 3840.00 3810.00 3676.00	48 36 31
CARRIAGE VEL SEAT X SEAT Y SEAT Z SEAT Z (SM)		10.67 -1.09 0.92 0.92 11.85	-0.05 -25.77 -1.12 -1.26 -0.28 -0.20	3828.00 4185.00 3793.00 5795.00 3834.00	3679.00 3789.00 3840.00 3802.00 3657.00	29 32 33 34 56 7
CHEST X CHEST Y CHEST Y CHEST RES CHEST S!		10.69 3.15 0.39 24.11 24.11 40.47	-0.20 -1.13 -3.46 -1.42 0.77	3834.00 3851.00 3839.00 3655.00 3855.00	3658.00 3885.00 3854.00 3755.00 3789.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD RES HEAD SI		10.47 .11 1.29 13.72 13.94 21.04	~4.69 -2.14 -0.82 0.59	3799.00 3755.00 3966.00 3846.00 3846.00 3799.00	3916.00 3877.00 3846.00 3654.00 4146.00 3945.00	2 3 4
HEAD HIC SHD REFL LF SHD REFL LF LF SHOULDER SHD REFL BI		16.49 25.05 28.90 44.33 44.49	7.48 4.19 13.98 16.75	3822.00 3844.00 3902.00 3901.00 3670.00	3894.00 4100.00 3987.00 3966.00 4069.00	14 16
SMD REEL RT RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER		50.57 83.49 68.17 73.93	16.75 8.76 33.46 25.33 16.17 49.80	3926.00 3873.00 3871.00 3929.00 3928.00	3841.00 4099.00 4077.00 3986.00 3986.00	15 17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / WT CAOTCH STRAP		0.73 47.58 60.52 106.65 0.67 82.24	0.31 19.58 34.69 54.33 0.34 -82.50	3928.00 3939.00 3948.00 3939.00 3939.00 3933.00	3986.00 3839.00 3838.00 3838.00 3838.00 3847.00	8 9
LF SEAT LNK X MT SEAT LNK X TOTAL SEAT X SEAT LNK Y		28.39 7.30 19.97 59.92	-213.36 -128.16 -339.18 -69.61	3926.00 3602.00 3619.00 3909.00	3846.00 3650.00 3847.00 3844.00	10 18 19
LF SERT PAN Z RY SERT PAN Z CT SERT PAN Z TOTAL SERT Z TOTAL SERT Z / HT RES SERT FORCE		458.96 403.93 739.41 1593.65 1630.68	24.71 27.24 43.98 107.80 0.67 111.23	3847.00 3848.00 3851.00 3847.00 3847.00 3847.00	3601.00 3608.00 3619.00 3601.00 3601.00	11213
RES SEAT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		10.19 -4.39 -9.55 -24.01 -40.64	0.70 -113.79 -154.95 -214.52 -481.47	3847.00 3793.00 3793.00 3794.00 3793.00	3601.00 3845.00 3847.00 3846.00 3846.00	26 23 20
LF FOOT Y AT FOOT T CT FOOT Y TOTAL FOOT Y LF FOOT Z		152.75 20.50 48.70 57.00 228.49	-25.44 -202.24 -12.71 -67.54 25.82	3830.00 4099.00 3830.00 3608.00 3830.00	3800.00 3838.00 3907.00 3837.00 3786.00	21 24 27
RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		225.81 209.54 597.93 710.80	10.61 -47.05 32.46 110.31	3838.00 3834.00 3831.00 3839.00	3916.00 3600.00 3785.00 4186.00	25 28

HEAD REST POS STUDY	TEST: 391	SUBJ: G-	MT: 159.0	G: 10	GP: 2 CELL:	A
DATA 10		MAX	HIN	T1	15	CH
10V EXT PHR CRABIAGE X CRABIAGE T CRABIAGE Z CARBIAGE Z (SH)		10.04 1.67 0.63 11.94 10.72	9.96 -1.02 -0.75 -0.21 -0.10 -25.73	1238.00 3846.00 3847.00 3838.00 3839.00 4129.00	1939.00 3790.00 3794.00 3743.00 3641.00 3791.00	48 36 31 1
CARRIAGE VEL SEAT X SEAT Y SEAT Z		-1.05 1.91 0.93 11.19	-1.62 -1.09 -0.23	3846.00 3815.00 3843.00	3851.00 3810.00 3652.00	32 33 34
SERT Z (SM) CHEST X CHEST Z CHEST Z CHEST RES		10.51 5.78 1.60 20.86 20.91	-0.17 -1.86 -1.83 -1.02 0.42	3646.00 3863.00 3851.00 3877.00 3877.00	3653.00 3893.00 3881.00 3602.00 3940.00	5 6 7
CHEST SI HEAD X HEAD Y HEAD RES HEAD SI		92.47 0.48 1.48 12.89 12.32	-5.71 -0.05 -1.06 0.71	3802.00 3947.00 3859.00 3859.00 3811.00	3900.00 3868.00 3665.00 4105.00 3965.00	2 3 4
HEAD HIC SHD REFL LF SHD REEL LF		16.77 64.44 50.30 111.19	19.62 4.47 33.30	3834.00 3883.00 3889.00 3887.00	3917.00 3954.00 3846.00 3977.00	14 16
LF SHOULDER SHD REFL RT SHD REEL RT RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHDULDER		16.94 55.96 97.60 110.22 103.98 206.34	20.46 1.72 30.46 41.17 9.11 67.57 0.42	3886.00 3894.00 3892.00 3892.00 3892.00	3977.00 3949.00 3851.00 3859.00 3849.00 3839.00	15 17
TOTAL SHO / HT LF LAP BELT AT LAP BELT TOTAL LAP		88.13 82.45 169.33 1.06	24.08 24.12 48.20 0.30	3690.00 4075.00 4086.00 4086.00 4086.00	3839.00 3849.00 3849.00 3849.00 3849.00	8 9
TOTAL LAP / HT CROTCH STRAP LF SERT LNK X BT SERT LNK X		45.20 41.42 7.14	-66.29 -173.28 -114.10 -287.37	4098.00 3704.00 3680.00 3680.00	3861.00 3852.00 3653.00 3853.00	10 18 19
TOTAL SERT X SEAT LANK T LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE		40.50 60.76 640.86 613.97 571.10 1616.36 10.17	-72.41 67.91 41.64 29.71 156.24 0.98 162.14	3952.00 3861.00 3860.00 3863.00 3860.00 3860.00	3866.00 3635.00 3652.00 3616.00 3654.00 3654.00 3654.00	35 11 12 13
RES SERT FORCE / WT LF FOOT X RT FOOT X CT FOOT X		1641.74 10.33 -12.40 2.38 -15.37	1.02 -160.75 -132.44 -174.57	3860.00 3805.00 3803.00 3804.00	3856.00 3856.00 3866.00	56 53 50
TOTAL FOOT X LF FOOT T RT FOOT T CT FOOT Y		-96.04 199.07 18.32 19.05	-462.40 -25.14 -128.11 -33.07 -53.19	3805.00 3850.00 3631.00 3807.00 3867.00	4116.00 3840.00 3858.00	21 24 27
TOTAL FOOT Y LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		28.06 184.68 194.48 124.48 442.55 603.53	-28.12 10.66 -109.94 -127.41 99.52	3865.00 3865.00 3805.00 3863.00 3865.00	3796.00 3796.00 3796.00 3796.00	22 25 26

HERD REST POS STUDY	TEST: 420	508J: 6-2	NT: 119.0	G: iO	GP: 2 CELL:	A
CI ATAD		MAX	HIN	Ť 1	12	CH
10V EXT PWR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE VEL SEAT X SEAT X SEAT Z SEAT Z SEAT Z SEAT Z		10.04 1.51 0.46 13.00 -1.02 1.294 18.15	9.96 -1.16 -0.15 -0.45 -1.50 -1.58	6.00 3839.00 3932.00 3833.00 4163.00 3796.00 3796.00	933.00 3832.00 3786.00 3610.00 3682.00 3832.00 3837.00	48 36 31 29 32 33 34 56
CHEST X CHEST Z CHEST Z CHEST RES CHEST SI		12.15 10.87 3.42 -0.08 14.36 14.35 26.19	-0.18 -1.16 -1.46 -0.96 0.71	3840.00 3858.00 3829.00 3864.00 3864.00 3797.00	3647.00 3892.00 3889.00 3651.00 3794.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD RES HEAD SIC		26.19 0.597 12.687 12.687 16.06	-4.60 -0.73 -1.07 0.51	3662.00 3926.00 3855.00 3856.00 3803.00 3830.00	3891.00 3855.00 3768.00 4121.00 3935.00 3901.00	2 3 4
SHD REFL LF SHD REEL LF LF SHOULDER		44.24 38.35 79.89	12.61 4.02 29.75	3885.00 3891.00 3889.00	4095.00 3858.00 4080.00	14 16
SHD REFL AT SHD REEL AT AT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHUD REEL TOTAL SHOULDER TOTAL SHOULDER		98.25 55.89 93.70 82.49 93.86 173.59	19.88 3.44 28.28 32.93	3886.00 3889.00 3889.00 3886.00 3890.00 3889.00	4098.00 3844.00 3844.00 4096.00 3858.00 3846.00	15 17
TOTAL SHO Z WT LF LAP BELT MT LAP BELT TOTAL LAP TOTAL LAP Z WT CROTCH STRAP		1.46 43.77 46.60 90.28 0.76	63.19 0.53 2.03 9.36 11.39 0.10	3932.00 3935.00 3935.00 3935.00	3842.00 3842.00 3842.00 3842.00	8
LF SEAT LNK X AT SEAT LNK X TOTAL SEAT X		102.85 56.21 55.41 69.98	-123.37 -20.67 -141.66	3932.00 3950.00 3805.00 3796.00	3849.00 3849.00 3862.00 3856.00	10 18 19
SERT LNK Y LF SERT PAN Z RT SERT PAN Z CT SERT PAN Z TOTAL SERT Z TOTAL SERT Z HT RES SERT FORCE / HT		49.61 305.58 337.45 415.47 1047.95 8.81 1058.21 8.89	-52.64 16.02 15.03 95.61 86.63 0.73 114.96	3927.00 3650.00 3656.00 3658.00 3858.00 3858.00 3858.00	3845.00 3634.00 3660.00 3608.00 3607.00 3607.00 3607.00	35 11 12 13
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		-18.40 -17.15 -31.57 -65.12 120.56	-230.13 -558 ug	4194.00 4174.00 4168.00 4197.00 3835.00	3848.00 3848.00 3848.00 3848.00 3807.00	20 23 26
AT FOOT T CT FOOT T TOTAL FOOT T		K1 /4	-32.30 -150.26 -3.24 -42.00	3697.00 3873.00 3813.00	3844.00 3923.00 3807.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		219.78 193.24 155.96 502.68 646.32	15.77 16.14 -97.88 7.70 77.97	3836.00 3837.00 3840.00 3842.00 3837.00	4060.00 4170.00 3791.00 3791.00 4170.00	25 25 28

HERD REST POS STUDT	1651: 382	SUBJ: K-1	NT: 176.0	G: 19 (Pr 2 CELLI	A
DATA ID		MAX	MIN	TI	12	CH
10V EXT PWR CARRIAGE X CARRIAGE T CARRIAGE Z		10.05 1.33 0.99 12.14	9.97 -1.11 -0.63 -0.18	3054.00 3626.00 3626.00 3622.00	2.00 3803.00 3947.00 3666.00	48 36 31
CAMMIAGE Z (SM) CAMMIAGE VEL SENT X SENT T SENT Z		10.38 -1.08 1.28 0.99 11.22	-0.06 -25.54 -1.09 -1.36 -0.26	3836.00 4208.00 3794.00 3740.00 3629.00	3681.00 3790.00 3802.00 3846.00 3659.00	39 33 34
ŠĒRT Ž (SM) CHEST X CHEST T CHEST Z		10.42 6.18 0.85 18.39 19.00	-0.17 -1.09 -1.22 -0.69 0.62	3630.00 3647.30 3633.00 3656.00 3656.00	3663.00 3895.00 3789.00 3734.00 4077.00	5 6 7
CHEST RES CHEST SI MEAD X MEAD Y MEAD Z		32.67 0.32 1.35 12.93 13.51	-6.52 -1.39 -1.16 0.75	3767.00 3719.00 3770.00 3641.00 3644.00	3930.00 3867.00 3844.00 3652.00 4190.00	2 3 4
HERD RES HERD SI MERD HIC SHO REFL LF SHO REFL LF		20.24 16.08 37.97 25.14 49.26	6.24 6.47 20.13	3797.00 3623.00 3854.00 3928.00 3656.00	3928.00 3864.00 4038.00 4005.00 4015.00	14
LF SHOULDER SHD REFL RT SHD REEL RT RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL		35.23 32.15 53.21 71.09 54.44	14.24 0.58 23.18 23.84 7.98	3840.00 3910.00 3910.00 3845.00 3915.00	4047.00 3823.00 3960.00 4088.00 3824.00	15 17
TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT RT LAP BELT TOTAL LAP		95.83 0.54 52.38 60.04 117.75	45.29 0.25 30.46 36.84 71.44	3865.00 3865.00 3902.00 3923.00 3922.00	3960.00 3960.00 3829.00 4317.00 4006.00	6
TOTAL LAP / HT CROTCH STRAP LF SEAT NK X RT SEAT LNK X TOTAL SEAT X		0.66 65.42 39.34 4.50 33.58	0.40 -79.26 -160.40 -129.72 -286.88	3922.00 3921.00 3775.00 3649.00 3666.00	#006.00 3850.00 3843.00 3844.00	10 18 19
SERT LNK Y LF SERT PAN Z RT SERT PAN Z CT SERT PAN Z TOTAL SERT Z TOTAL SERT Z TOTAL SERT Z HT RES SERT FORCE		46.38 633.19 649.82 677.69 1960.70 11.02	-84.37 50.23 50.10 42.45 151.40 0.85 154.31	3908.00 3846.00 3646.00 3646.00 3846.00 3846.00	3848.00 3607.00 3623.00 3607.00 3607.00 3607.00	11 12 13
RES SEAT FORCE / WT LF FOOT X AT FOOT X CT FOOT X TOTAL FOOT X		11.14 -9.53 8.34 0.77 -17.18	0.87 -166.85 -133.53 -208.52 -508.90	3846.00 3704.00 3791.00 3940.00 3941.00	3607.00 3641.00 3841.00 3841.00 3841.00	26 23
LF FOOT Y BT FOOT Y CT FOOT Y TOTAL FOOT Y		154.10 16.92 35.26 67.33	-22.34 -178.98 -47.51 -97.17 -18.88	3833.00 3962.00 3792.00 3817.00 3625.00	3800.00 3524.00 3828.00 3843.00 3801.00	21 24 27 22
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		196.81 244.58 161.57 546.82 707.32	-19.12 -96.29 -77.24 60.05	3824.00 3617.00 3625.00 3834.00	3952.01 3802.00 3801.00 4074.00	22 25 28

HEAD REST POS STUDT	TEST: 396	SUBJ: M-2	MT: 163.0	G: 10	GP: 1 CELL:	A
DATA ID		MAX 	MIN	Ť1	15	CH
IOV EXT PHR CRRRINGE X CRRRINGE T CRRRINGE Z		10.06 1.14 0.08 12.43	9.97 ~0.73 ~0.90 ~0.27	2293.00 3913.00 3895.00 3887.00	537.00 3886.00 3612.00 3698.00	48 36 31 1
CARRIAGE Z (SM) CRHRIAGE VEL SEAT T SEAT Z		10.54 -1.17 1.42 0.62 11.45	-0.07 -25.50 -1.05 -1.26 -0.31	3888.00 4160.00 3851.00 3850.00 3894.00	3698.00 3838.00 3866.00 3663.00 3716.00	29 32 33 34
SEAT Z (SM) CHEST X CHEST Z CHEST RES		10.60 2.57 2.01 21.73 21.74	-0.17 -2.55 -1.97 -0.81 0.49	3894.00 3910.00 3920.00 3920.00	3715.00 3946.00 3911.00 3777.00 3844.00	5 6 7
CHEST SI HEAD X HEAD T HEAD RES HEAD SI		38.23 2.59 0.99 11.98 12.35 16.43	-3.90 -1.91 -1.23 0.39	3851.00 3904.00 3770.00 3909.00 3909.00 3867.00	4113.00 3956.00 3911.00 3650.00 4183.00 4045.00	2 3 4
HEAD HIC SHO REFL LF SHO REEL LF LF SHOULDER SHO REFL RT		12.23 50.91 40.75 89.14 42.33	13.73 3.20 29.34 25.46	3885.00 3957.00 3951.00 3950.00 3974.00	3941.00 4098.00 3910.00 4098.00 4041.00	14 16 15
SHO REEL RT RT SHOULDER TOTAL SHLO REFL TOTAL SHOULDER TOTAL SHOULDER		64.22 106.34 58.72 99.70 187.25	4.87 38.46 41.29 8.21 72.98	3982.00 3974.00 3957.00 3952.00 3956.00	3909.00 4048.00 4097.00 3909.00 4098.00	iŦ
TOTAL SHD / WT LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / WT		1.15 25.92 51.02 76.25 0.47	0.45 1.83 8.67 11.41 0.07	3956.00 3999.00 4003.00 4002.00 4002.00	4098.00 3894.00 3890.00 3894.00 3894.00	8 9
CROTCH STRAP LF SEAT LNK X BT SEAT LNK X TOTAL SEAT X SEAT LNK Y		122.14 67.51 35.17 71.83 70.44	-47.31 -126.47 -57.61 -184.08 -43.35	3984.00 3986.00 3862.00 3988.00 3966.00	3909.00 3909.00 3909.00 3909.00 3908.00	10 18 19
LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z RES SEAT FORCE		375.46 357.94 893.64 1621.90 9.95 1632.87	28.28 25.17 65.97 135.18 0.83 145.88	3909.00 3910.00 3909.00 3909.00 3909.00 3909.00	3819.00 3607.00 3616.00 3625.00 3625.00 3625.00	11 12 13
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		-26.18 -31.67 -82.29 -153.70 157.85	-148.24 -222.88 -274.59 -635.96 -28.20	4005.00 4195.00 4195.00 4195.00 3890.00 3699.00	3905.00 3907.00 3907.00 3906.00 3976.00 3898.00	20 23 26 21 24
NT FOOT Y CT FOOT Y TOTAL FOOT Y LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		18.25 35.33 45.66 274.17 279.44 148.29 560.97 823.69	-199.17 -42.10 -100.57 30.84 53.71 -130.15 28.35 180.68	3927.00 3867.00 3890.00 3907.00 3890.00 3890.00	3902.00 3898.00 3845.00 4196.00 3845.00 4196.00	27 22 25 28

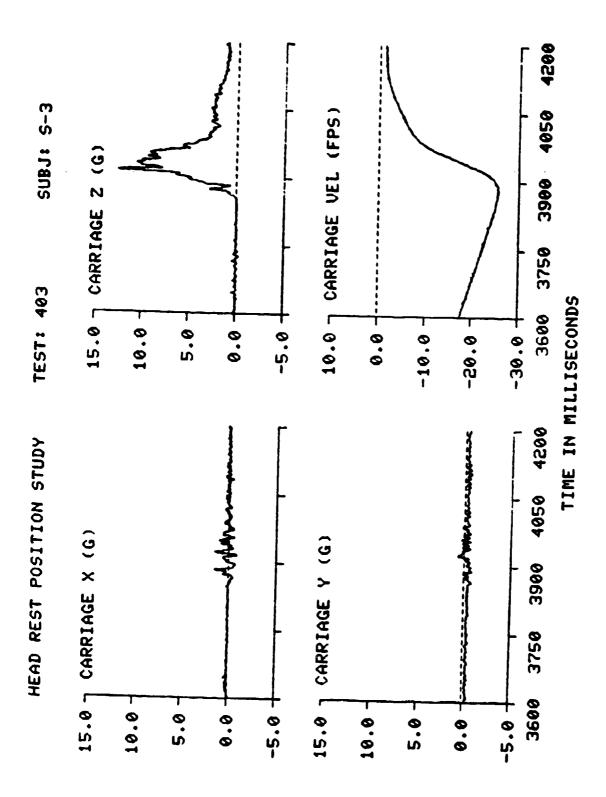
HEAD REST POS STUDY	TEST: 364	SUBJ: M11	HT: 155.0	G: 10 G	Pr 1 CELL:	A
DATA ID		MAX	HIN	T1	T2	CH
10V EXT PHA CARRIAGE X CARRIAGE Y CARRIAGE Z		10.05 1.33 0.89 12.46	9.96 -1.01 -0.75 -0.36 -0.15	2240.00 3910.00 3907.00 3901.00 3902.00	1342.00 3879.00 3853.00 3683.00 3684.00	48 36 31 1
CARRIAGE Z (SM) CARRIAGE VEL SEAT X SEAT Z		10.72 -0.99 1.34 0.56 11.27	-25.67 -1.21 -0.97 -0.26 -0.20	4155.00 3868.00 3866.00 3908.00 3909.00	3875.00 3916.00 3928.00 3689.00 3710.00	29 32 33 34
SEAT Z (SM) CHEST X CHEST Z CHEST RES		10.61 3.51 0.37 18.12 18.18 30.97	-2.17 -1.53 -0.85 0.49	3925.00 3898.00 3935.00 3935.00 3863.00	3957.00 3916.00 3714.00 3860.00 4012.00	5 6 7
CHEST SI HERD X HERD Y HERD Z HERD RES		1.90 0.96 13.09 13.27 18.08	-4.66 -1.86 -1.02 0.49	3909.00 3790.00 3919.00 3919.00 3873.00	3956.00 3925.00 3725.00 4137.00 4027.00	# 3 5
HEAD SI HEAD HIC SHD REFL LF SHO REEL LF LF SHOULDER		13.62 61.75 63.51 122.35 55.10	17.63 6.37 30.27 23.87	3899.00 3950.00 3955.00 3954.00 3950.00	3943.00 4008.00 3910.00 3911.00 3995.00	14 16 15
SHO REFL AT SHO REEL AT RT SHOULDER TOTAL SHLO REFL TOTAL SHLO REEL TOTAL SHOULDER		48.12 99.81 116.85 110.66 221.82	3.44 35.44 43.15 11.99 67.07	3958.00 3957.00 3950.00 3957.00 3955.00	3925.00 3503.00 4007.00 3912.00 3903.00	17
TOTAL SHO / NT LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / NT		1.43 59.20 60.40 119.54 0.77	0.43 20.86 18.46 39.43 0.25	3955.00 4021.00 4022.00 4022.00 4022.00	3903.00 3911.00 3905.00 3911.00	8 9
CROTCH STRAP LF SEAT LNK X RT SEAT LNK X TOTAL SEAT X		38.89 48.97 26.36 39.19 69.13	-47.97 -176.66 -117.76 -293.85 -54.96	4004.00 4123.00 3869.00 3732.00 3978.00	3912.00 3919.00 3917.00 3917.00 3924.00	10 18 19
SERT LNK Y LF SERT PAN Z RT SERT PAN Z CT SERT PAN Z TOTAL SERT Z TOTAL SERT Z HT RES SERT FORCE		508.45 451.71 673.95 1606.59 10.37 1629.64	31.78 22.98 48.03 111.87 0.72 116.10 0.75	3919.00 3923.00 3926.00 3927.00 3927.00 3927.00 3927.00	3619.00 3620.00 3618.00 3619.00 3619.00 3619.00	11 12 13
RES SERT FORCE / WT LF FOOT X RT FOOT X CT FOOT X TOTAL FOO! X		10.51 2.60 8.51 9.27 10.64	-156.52 -155.39 -157.99 -461 90	3999.00 3868.00 3875.00 3999.00	3919.00 3930.00 3930.00 3919.00	20 23 26
LF FOOT Y RT FOOT Y CT FOOT Y TOTAL FOOT Y		131.81 13.60 25.90 47.09	-28.91 -149.69 -19.49 -66.02	3913.00 3731.00 3869.00 3870.00 3930.00	3877.00 3921.00 3981.00 3922.00 3876.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		192.53 221.07 133.43 475.90 639.24	-18.10 -12.40 -96.15 -81.72 11.35	3926.00 3926.00 3926.00 3930.00	3872.00 3879.00 3858.00 4011.00	22 25 28

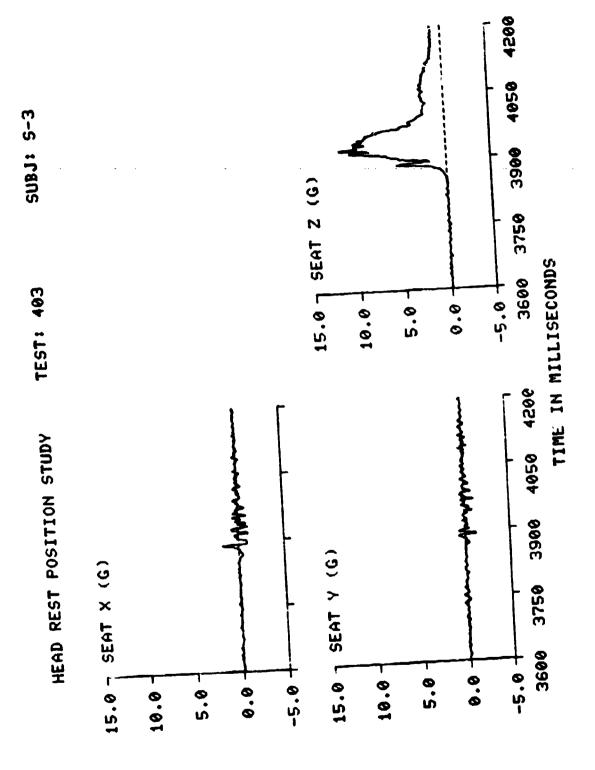
HEAD REST POS STUDY TEST: 366	SUBJ: M13	MT: 170.0	G: 10	GP: 1 CELL:	R
DATA LD	MAX	MIN	T 1	T2	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z (SM)	10.05 1.11 0.63 12.10	9.96 -0.98 -0.60 -0.24	4068.00 3857.00 3859.00 3850.00 3866.00	2490.00 3832.00 3800.00 3664.00	48 36 31 1
CARRIAGE VEL SEAT X SEAT T SEAT Z	10.45 -0.89 2.41 0.75 11.14	-0.10 -25.82 -1.13 -1.16 -0.31	4149.00 3821.00 3819.00 3857.00	3664.00 3820.00 3830.00 3878.00 3771.00	29 32 93 34
SEAT Z (SM) - CHEST X CHEST Y - CHEST Z - CHEST RES - CHEST SI	11.14 10.45 2.93 1.02 19.43	-0.21 -1.49 -3.29 -1.48 0.77	3858.00 3868.00 3862.00 3883.00 3883.00	3681.00 3904.00	23233
HEAD X HEAD Y HEAD Z HEAD RES HEAD SI	29.84 0.08 1.81 14.33 20.92	-4.67 -0.81 -0.90 0.83	3823.00 3671.00 3956.00 3868.00 3868.00 3825.00	3852.00 3894.00 3865.00 9692.00 4189.00	3
HEAD HIC SHD REFL LF SHD REEL LF LF SHOULDER SHD REFL RT	14.76 36.01 20.49 47.93 41.54	10.15 1.24 14.20 14.92	3846.00 3910.00 4095.00 3917.00 3897.00	3918.00 3853.00 3866.00 3859.00	14 16 15
SHO REEL AT AT SHOULDER TOTAL SHLO REEL TOTAL SHLO REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER	78.55 78.13 53.54 122.97 0.72	22.23 25.23 8.12 37.43 7.45	3911.00 3907.00 3897.00 3916.00 3909.00	3878.00 3854.00 3857.00 3877.00 3858.00	
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / NT	54.58 53.98 106.80 0.63	11.94 19.46 0.11	3955.00 3950.00 3954.00 3954.00	3861.00 3860.00 3861.00 3851.00	8 9
CROTCH SIRAP LF SEAT LNK X BT SEAT LNK X TOTAL SEAT X	69.50 27.19 13.30 16.65	-4.36 -201.90 -144.43 -345.75	4090.00 4152.00 3822.00 3758.00	3867.00 3867.00 3865.00 3866.00	10 18 19
SERT LNK Y LF SERT PRN Z RT SERT PRN Z CT SERT PRN Z TOT - SERT Z TO - SERT Z REC SERT Z / HT REC SERT FORCE	\$7.31 352.98 408.61 689.42 1630.50 9.59 1666.61	23.49 22.21 25.01 52.91 111.27	3933.00 3867.00 3873.00 3868.00 3867.00 3867.00	3864.00 3601.00 3614.00 3604.00 3604.00 3604.00	35 11 12 13
RES SCAT FORCE / NT LE COT X RT FOOT X CT FOOT X TOTAL FOOT X	9.80 -35.53 -4.04 -9.86 -58.37 168.72	111.33 0.65 -187.43 -197.01 -199.47 -578.49	3867.00 3821.00 3821.00 3822.00 3821.00 3853.00	3604.00 3889.00 3880.00 3880,00 3880.00	20 23 26
LF FOOT Y NI FCOT Y CI FOOT Y TOTAL FOOT Y LF FOOT Z	15.00 35.85 58.68 279.62	-25.19 -190.00 -30.90 -87.65 -44.81	3853.00 3924.00 3677.00 3840.00 3854.00	3727.00 3881.00 3875.00 3882.00 3829.00	21 24 27 22
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE	277.58 117.55 597.23 800.50	28.33 -140.93 -22.27 131.99	3671.00 3874.00 3871.00 3871.00	3823.00 3834.00 3811.00 3822.00	22 25 26

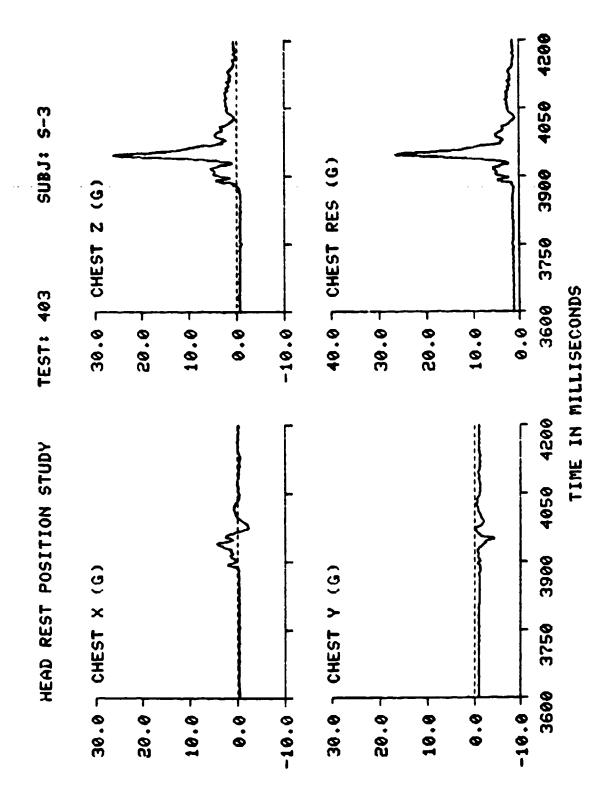
	AUR I. Rai	NT: 197.0	G: 10 GP	, 2 CELLI	A
HEAD REST POS STUDY TEST: 404	HUX	MIN	71	15	CH
DATA 1D		9,96	3421.00	2565.00	48
109 EXT PHR	10.05	-1.03 -1.10	3887.00 3938.00	3901.00 3872.00	36 31
CARRIAGE X CARRIAGE Y CARRIAGE Z	0.40 11.84 10.50	-0.29 -0.10	3919.00	3824.00 3823.00	59 1
CARRIAGE Z (SM) CARRIAGE VEL	-1.12	-25.83 -1.34	4178.00 3884.00	3879.00 3933.00 3895.00	32 33
SEAT X SEAT T	1.54 1.24 11.44	-1.43	3888.00 3926.00 3926.00	3728.00 3728.00	34
SERT Z SERT Z (SM) CHEST X	10.38 7.25	-0.14 -0.45 -2.58	3949.00	3643.00 3951.00	5 6 7
CHEST X CHEST T CHEST Z	-0.44 15.30 16.94	-0.99 0.84	3953.00 3951.00	3826.00 3880.00	•
CHEST RES CHEST SI	29.17 1.75	-5.36	3885.00 3928.00	4012.00 3980.00 3939.00	2
HEAD X HEAD Y	1.18	-1.44 -0.95 0.21	00.000 00.14ec 00.14ec	3847.00 4152.00	4
MEAD Z HEAD RES HEAD SI	12.45 19.35	0,21	3893.00 3914.00	4116.00 4004.00	14
HEAD HIC	14.98 69.17 75.63	28.92 12.13	3975.00 4010.00	3925.00 3931.00 3925.00	18
SHO REEL LY LE SHOULDER	138.91 76.89	42.51 33.95	3975.00 4098.00 4000.00	3922.00 3933.00	15 17
SHO REFL AT SHO REEL AT	89.70 137.56	2.62 30.07 63.70	4000.00	3930.00	
AT SHOULDER TOTAL SHLO REFL TOTAL SHLO REEL	128,82 153,36 269,52	15.00 82.46	4004.00 3973.00	3932.00 3932.00	
TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT	1.37 53.48	0.42 33.52	3973.00 4078.00 4078.00	3932.00 3926.00	8 9
MI LAP BELI	84.79 118.27	\$9.56 74.50 0.38 -72.56	4078.00 4078.00	3920.00 3919. 50 3919.00	
TOTAL LAP TOTAL LAP / HT CAOTCH_STRAP_	0.60 260.97 30.84	-72.56 -191.91	4029.00	3942.00 3835.00	10 18 19
LF SEAT LNK X	-4.54 8.71	-165.98 -354.98	3770.00 4191.00	3940.00 3941,00 3840.00	35
TOTAL SERT X SERT LNK Y	57.04 464.47	-67.04 44.61	4020.00 3941.00 3941.00	3629.00 3602.00	11
LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z	665.77 794.73	50.05 57.89 164.42	3943.00	3602.00 3602.00	1 3
TOTAL SEAT Z / HT	1918.39 9.74 1951.14	0.83	3942.00	3602.00 3602.00	
RES SEAT FORCE / HT	9,90 -23,60	0.84 225.42	3942.00	3602.00 3936.00 3937.00	20 23
LF FOOT X	-17.73 -43.16	-189.56 -269.45	3889.00 3889.00 3889.00	3935.00 3936.00	23
CT FOOT X TOTAL FOOT X LF FOOT T	-89,21 197.32	- 54.54	3921.00	4128.00 3938.00	21 24 27
AT FOOT T CT FOOT Y	90.86 26.86 60.29	-55.91 -65.62	3962.00	3932.00 3950.00	
TOTAL FOOT T LF FOOT Z	296.60 275.30	28.63 36.83	3922.00 3937.00	3880.00 3618.00 3901.00	22 25 28
ŘT FDOT Z CT FOOT Z	122.19 633.3	-151.03	3922.00		
TOTAL FOOT Z RES FOOT FORCE	668.3	, 100.3			

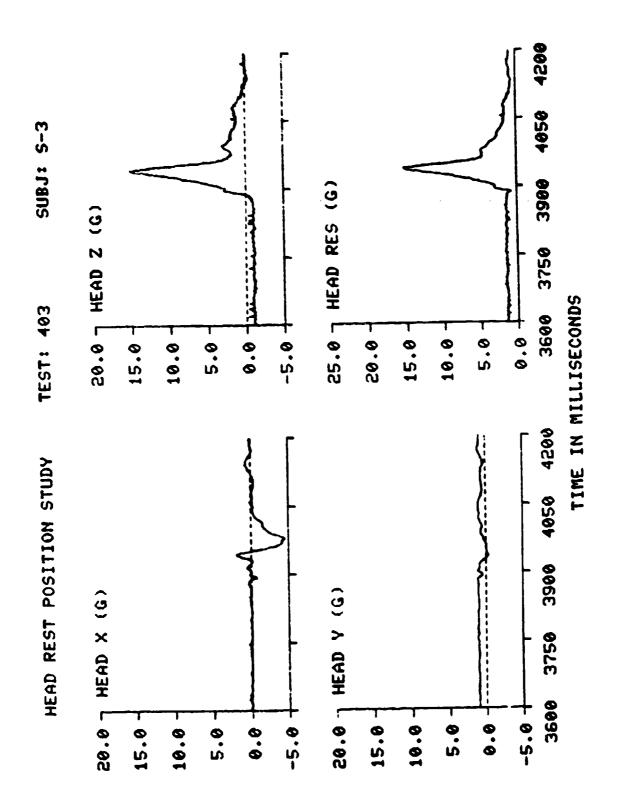
HEAD REST POS STUDY	TEST: 385	SUBJ: R-3	HT: 146.0	G: 10	GP: 2 CELL:	A
DATA ID		MAX	MIN	<u>T1</u>	72	CH
10V EXT PWR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z (SM) CARRIAGE Z (SM)		10.04 1.57 1.00 12.88 10.69	9.96 -1.18 -0.65 -0.26 -0.14 -25.47	12.00 3925.00 3924.00 3919.00 3935.00 4189.00	788.00 3935.00 4080.00 3751.00 3751.00 3889.00	48 36 31 1
SERT X SERT T SEAT 7		1.36 0.47 12.27 10.78 3.11	-1.61 -0.99 -0.16	3886.00	3934.00 3890.00 3734.00	29 32 33 34
SERT Z (SM) CHEST X CHEST X CHEST Z CHEST RES CHEST SI	·	14.76 15.12 22.32	-0.10 -0.80 -2.00 -0.99 0.99	3925.00 3926.00 3952.00 3950.00 3950.00 3952.00 3887.00	3612.00 3974.00 3938.00 3763.00 4185.00 4009.00	5 6 7
HERD X HERD Y HERD Z HERD RES HERD SI		3.91 11.78	-5.46 -0.96 -1.51 0.62	3724.00 4042.00 3936.00 3936.00 3891.00	3965.00 3954.00 4042.00 4160.00 4034.00	9
MEAD HIC SHO REFL LF SHO REEL LF LF SHOULDER		18.99 19.99 55.89 85.27 61.30	26.78 9.18 48.85	3910.00 3968.00 4080.00 3968.00	3992.00 4087.00 3933.00 3922.00	14 16
SHD REFL AT SHD REEL AT AT SHOULDER TOTAL SHLO REFL TOTAL SHLO REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHO / NT		57.27 61.34 111.90 108.18 69.03 193.88 1.33	38.85 30.852 13.225 59.75 64.93 23.19 109.17	3953.00 3991.00 3961.00 3963.00 3961.00	4038.00 3930.00 3921.00 4036.00 3931.00 3922.00 3922.00	15 17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / HT		50.95 53.76 104.28 0.71	11.74 18.54 30.48 0.21	3961.00 4011.00 4007.00 4010.00 4010.00	3944.00 3945.00 3944.00 3944.00	8 9
CROTCH STRAP LF SEAT LNK X AT SEAT LNK X TOTAL SEAT X		60.74 60.87 43.26	-43.70 -144.61 -46.43 -191.04	4020.00 4014.00 3983.00 4012.00	3932.00 3934.00 3934.00 3934.00	10 18 19
SEAT LNK T LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE / HT		81.19 75.57 417.16 334.67 787.64 1553.97 10.64 1565.65	-58.21 53.05 44.17 91.92 198.71 202.42	4001.00 3936.00 3935.00 3936.00 3936.00 3936.00	3933.00 3617.00 3623.00 3623.00 3617.00 3617.00 3617.00	35 11 12 13
PT F001 X CT F001 X T01AL F001 X LF F001 T AT F001 T		10.56 13.40 15.54 148.18 27.28 18.95	-138.13 -90.78 -139.55 -361.98 -21.28	3884.00 3926.00 3883.00 3685.00 3921.00 4075.00	3934.00 3934.00 3935.00 3934.00 4072.00 3929.00	20 23 26 21
CT FOOT Y TOTAL FOOT Y LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z MES FOOT FORCE		19.95 41.11 167.97 194.09 151.82 458.59 516.44	-50.35 -61.08 -16.48 -7.03 -63.08 -59.63 16.66	3897.00 3897.00 3921.00 3922.00 3928.00 3922.00 9945.00	3931.00 3940.00 3875.00 3895.00 3895.00 3895.00	27 22 25 28

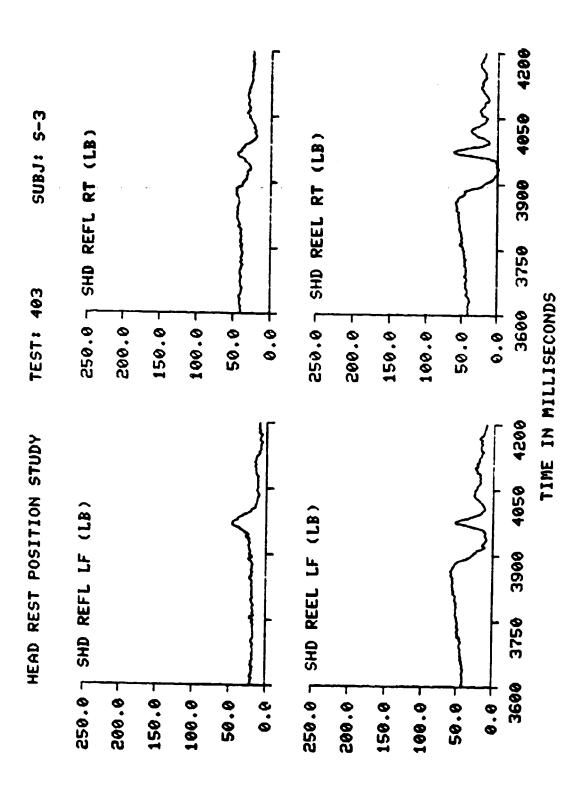
10V EXT PHR 10.05	HEAD REST POS STUDY	TEST: 403	SUBJ: 5-3	HT: 165.0	G: 10	GP: 2 CELL:	A
CARRIAGE X CARRIAGE Y CARRIAGE Y CARRIAGE Z	DATA 10		MAX	HIN	T1	†2 	CH
RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL S TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL S TOTAL SEAT Z TOTAL S TOTAL S TOTAL S TOTAL S TOTAL S TOTAL S TOTA	DATA 10 IONTA 1		X- 0466528931927026323355670460174183872030829050085000850008502001741836985720985008500850085008500850085008500850085	N- 98826807849310 7107 935749455653586283972179913922 N- 9000.1712212318 4435 07921819738951654263977859243 N- 900005110002410 4010 005925368021590.151760.90113760900000000000000000000000000000000000	256239917.000 399247.000 399247.000 399247.000 399249.000 399249.000 399249.000 399249.000 399249.000 399249.000 399249.000 399249.000 399249.000 399249.000 399249.000 3992	00000000000000000000000000000000000000	

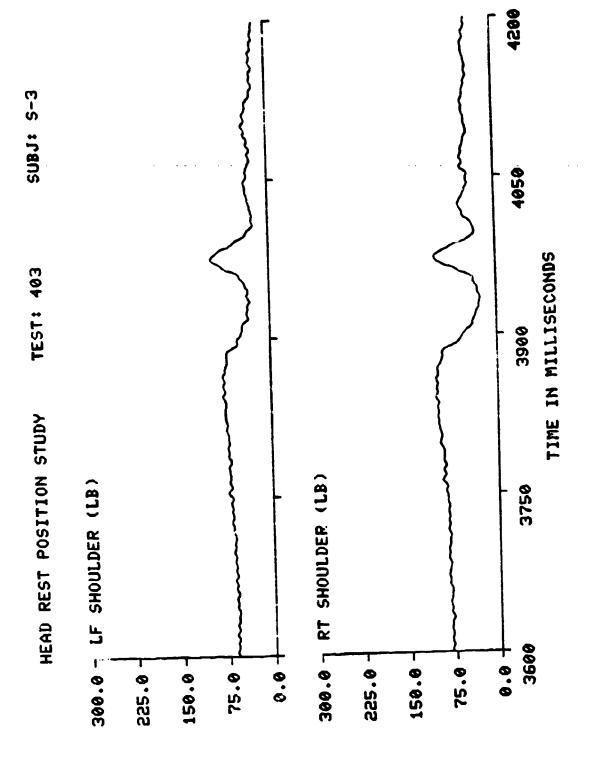


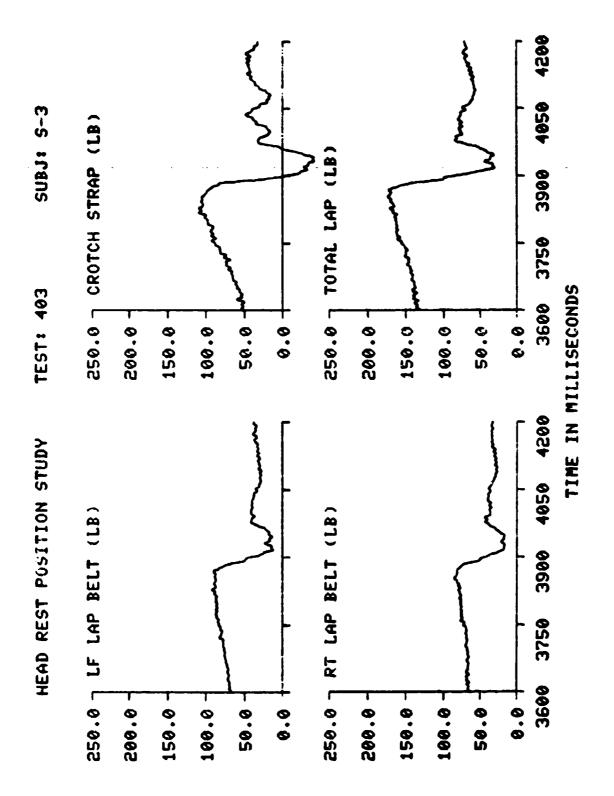


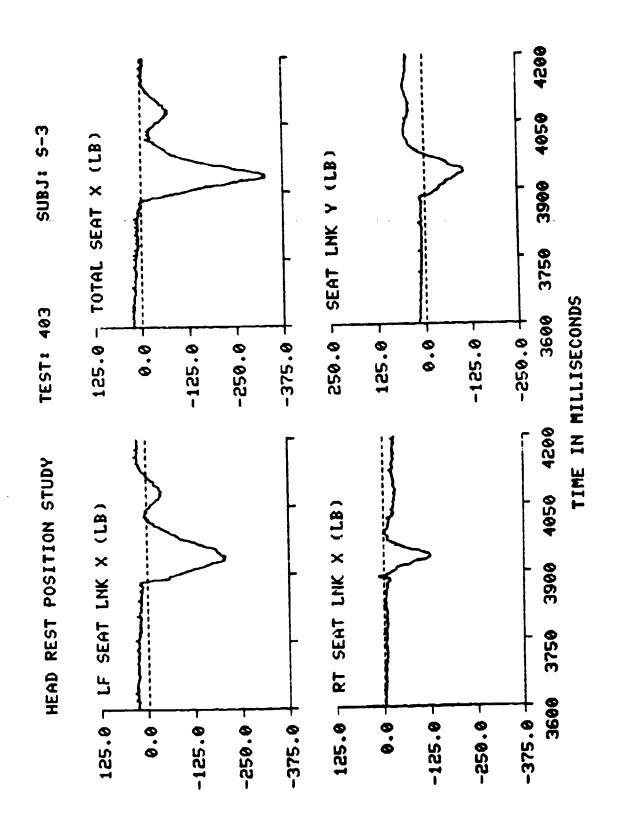


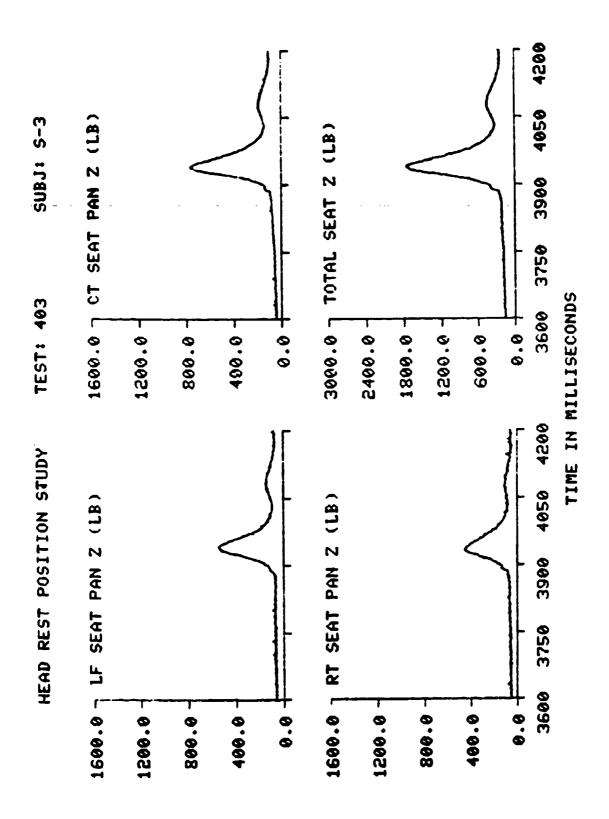


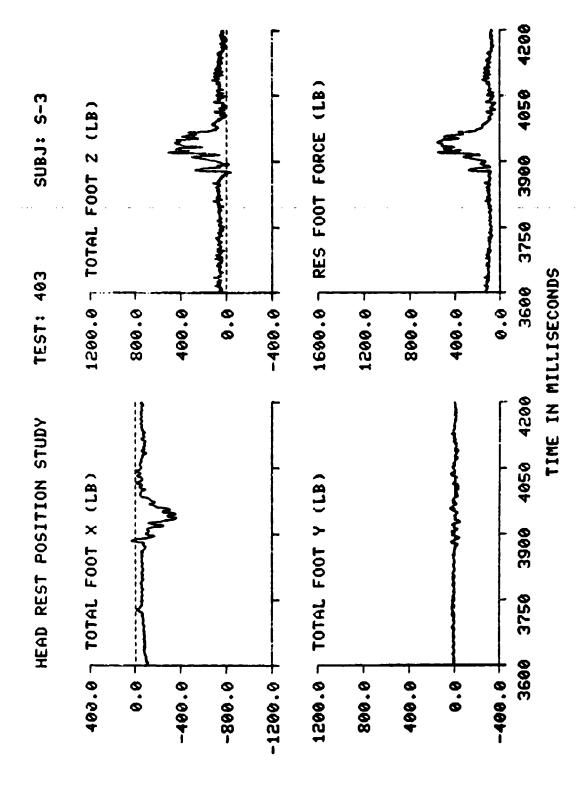












MEAD REST POS STUDY	TEST: 345	\$UBJ: D-1	NT: 205.0	G: 10	GP: 1 CFLL:	В
DATR ID		MAX	MIN	Ť 1	T 2	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z		10.05 1.48 0.54 12.45 10.61	9.96 -0.99 -0.87 -0.21 -0.10 -25.73	3367.00 3840.00 3841.00 3833.00 3834.00 4161.00	377.00 3833.00 3981.00 3613.00 3612.00 3795.00	48 36 31 1
SERT X SERT Y		1.24 0.89 11.48	-1.07 -1.52 -0.21 -0.14	3841.00 3812.00 3840.00	3833.00 3806.00 3660.00	29 32 33 34 56 7
SERT Z (SM) SERT Z (SM) CHEST X CHEST T CHEST Z CHEST RES CHEST SI		10.62 5.45 -0.24 15.06 15.19 27.94	-0.14 -0.96 -3.93 -0.79 0.67	3841.00 3852.00 3929.00 3871.00 3871.00 3797.00	3660.00 3882.00 3864.00 3672.00 3694.00 3931.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD RES HEAD SI		0.82 19.05	-1.29 -1.31 -0.83 0.44	3841.00 3902.00 3853.00 3853.00	3879.00 3849.00 3673.00 3798.00	2 3 4
HEAD HIC SHO REFL LF SHO REEL LF LF SHOULDER SHO REFL RT		19.122 16.222 50.331 59.55	10.41 2.33 21.45 18.66	3805.00 3827.00 3863.00 3942.00 3884.00 3875.00	3891.00 4093.00 3838.00 4094.00	14 16
SHO REEL AT AT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER		13.93 96.92 108.23 69.16 161.97	32.58 32.58 29.57 8.39 60.92 0.30	3929.00 3879.00 3871.00 3939.00 3881.00	3847.00 3838.00 4093.00 3839.00 3837.00 3837.00	15 17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP TOTAL LAP TOTAL LAP		\$9.40 45.87 104.85 0.51	29.41 20.85 51.63 0.25	3939.00 3943.00 3943.00 3943.00	3836.00 3843.00 3843.00 3843.00	8 9
CROTCH STRAP LF SEAT LNK X AT SEAT LNK X		249.79 69.11 49.26 105.76	-22.05 -109.33 -49.71 -157.80	3946.00 3920.00 3906.00	3849.00 3847.00 3846.00 3847.00	10 18 19
TOTAL SEAT X SEAT LAM Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z / HT		\$2.20 479.12 402.81 1131.66 2006.65 979 2012.48	-39.20 34.85 38.43 106.95 202.21 0.99 207.09	3914.00 3904.00 3849.00 3855.00 3852.00 3852.00	3856.00 3603.00 3688.00 3678.00 3671.00 3671.00	35 11 12 13
RES SEAT FORCE RES SEAT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		9.82 -95.44 -29.56 -90.37 -105.39	1.01 -244.29 -270.22 -276.34 -782.82	3852.00 3852.00 4093.00 4086.00 4068.00 4086.00	3671.00 3850.00 3850.00 3852.00 3851.00	26 53 50
LF FOOT Y AT FOOT Y CT FOOT Y TOTAL FOOT Y		10.67 25.29 38.22	-26.57 -204.07 -29.88 -51.57	3835.00 4059.00 3822.00 3884.00	3946.00 3852.00 3847.00 3850.00 3789.00	21 24 27
LF FOOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z AES FOOT FORCE		202.25 314.19 150.25 878.79 986.66	22.61 40.41 -108.06 -18.99 125.09	3860.00 3860.00 3844.00 3844.00 3852.00	3789.00 4059.00 3790.00 3789.00 4086.00	22 25 28

HEAD REST POS STUDY	TEST: 339	SU8J: F-2	MT: 159.0	G: 10	GP: 1 CELt. 1	8
DATA 10		HAX	HIN	T1	72	CH
10V EXT PHR CARAIAGE X CARAIAGE T CARRIAGE Z		10.05 1.35 0.64 12.54	9.96 -0.77 -0.70 -0.19	2414.00 3900.00 3898.00 3893.00	350.00 3892.00 9941.00 3697.00	48 36 31
CARRIAGE Z (SM) CARRIAGE VEL SEAT X SEAT T SEAT Z	<u>.</u> .	10.64 -1.17 8.35 0.73 11.59	-0.10 -25.51 -10.54 -0.87 -0.35	3894.00 4164.00 9862.00 3862.00	3698.00 3847.00 3622.00 3867.00 3717.00	- 34 35 35 59
SERT Z SERT Z (SM) CHEST X CHEST Z CHEST Z CHEST RES		10.65 9.31 -0.48 19.68 20.34	-0.19 -0.97 -4.65 -1.07 0.85	3900.00 3915.00 3896.00 3919.00 3919.00	3688.00 3948.00 3916.00 3601.00 3717.00	5 6 7
CHEST SI HEAD X HEAD T HEAD Z HEAD RES		88.01 1.67 0.59 13.89 14.01	-1.95 -0.96 -0.46 0.47	3857.00 3918.00 4180.00 3913.00 3913.00	3988.00 3949.00 3906.00 3826.00 4126.00	2 3 ¥
HERD SI HERD HIC SHD REFL LF SHD REEL LF LF SHOULDER		18.99 40.29 42.42 64.53	13.21 10.01 38.00	3863.00 3887.00 3893.00 999.00 4000.00	4112.00 9952.00 3980.00 3913.00 3979.00	1 4 1 6
SHO REFL RT SHD REEL RT AT SHOULDER TOTAL SHLO REFL TOTAL SHLO REEL TOTAL SHOULDER		47.90 39.65 86.30 80.71 77.97 136.69	21.59 6.97 34.60 35.26 17.96 77.50	3936.00 3939.00 3936.00 3935.00 3999.00 3937.00	3984.00 3902.00 3971.00 3982.00 3904.00 3970.00	15 17
TOTAL SHO / NT LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / NT		0.86 34.22 29.08 62.37 0.39	0.49 8.90 10.43 19.67 0.12 8.37	3937.00 4002.00 3999.00 4000.00	3970.00 3970.00 3898.00 3900.00 3899.00	8
CROTCH STRAP LF SEAT LNK X RT SEAT LNK X TOTAL SEAT X		230.14 -0.61 -1.50 -1.50	8.37 -126.67 -201.60 -328.26	4003.00 3679.00 3620.00	3911.00 3909.00 3909.00 3909.00	10 18 19
SERT LNK T LF SERT PRN Z RT SERT PRN Z CT SERT PRN Z TOTAL SERT Z HT		398.52 564.95 657.68 1613.10 10.15	-8,96 22,15 33,77 31,49 92,19 0,56	3647.00 3932.00 3910.00 3913.00 3913.00 3913.00	4025.00 3688.00 3659.00 3729.00 3659.00 3659.00	35 11 12 13
RES SEAT FORCE / WT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		1645.51 10.35 5.57 6.52 18.88 29.34	92.88 0.58 -98.40 -150.33 -166.15 -409.45	3913.00 3913.00 3651.00 3860.00 3861.00	3659.00 3659.00 3910.00 3911.00 3911.00	20 23 26
LF FOOT Y MT FOOT T CT FOOT Y TOTAL FOOT Y		129.87 14.11 51.28 69.97	-23,86 -166.04 -8.35 -67,83	3904.00 3860.00 3884.00 3884.00	3851.00 3894.00 3849.00 3867.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		201.82 215.00 215.23 541.41 648.94	-21.98 -21.98 -51.53 -34.08 80.61	3896.00 3912.00 3900.00 3904.00 3913.00	3853.00 3856.00 3853.00 3852.00 4134.00	22 25 28

					G: 10 G	P: 2 CELL:	В
HERD REST POS STUDY	TEST: 351	20B7:	G-3 Max	MIN 158.U	T1	15	CH
OI RYAD			MMX	***			
LOV EXT PHR CARRIAGE X			10.06 1.54 0.89	9.96 -0.83 -0.89 -0.30	323.00 3879.00 3880.00 3871.00	1134.00 3847.00 3983.00 3698.00	48 36 31 1
CARRIAGE Y CARRIAGE Z CARRIAGE Z (SH) CARRIAGE YEL SERT X			12.06 10.64 -0.81	-0.11 -25.62 -1.26	9872.00 4150.00 3841.00 3837.00	3698.00 3843.00 3848.00 3843.00	39 32 33
SEAT T SEAT Z			1.10 11.35 10.56	-1.20 -0.27 -0.14	3878.00 3879.00	3710.00 3711.00	ν̃ε
ŠĒĢT Ž (SM) CHEST X CHEST T			2.89 0.29 21.60	-2.74 -2.29 -1.25 0.75	3887.00 3883.00 3916.00 3916.00	3933.00 3912.00 3794.00 4112.00	5 6 7
CHEST RES			21.70 34.22		3835.00	3995.00 3926.00	2
CHEST SI HEAD X HEAD Y HEAD Z			1.22 1.46 12.12 12.19	-3.12 0.15 -1.80 0.66	3943.00 3986.00 3896.00 3896.00	3952.00 3657.00 3964.00	3
HEAD RES HEAD SI			19.24 15.58		3847.00 3869.00	3948.00	14
HEAD HIC SHO REFL LE			71.40	18.72 3.79	3923.00 3922.00	4000.00 3875.00	iš
SHO REEL LF LF SHOULDER SHO REFL BI			121.01	40.00 22.52	3922.00 3921.00 3925.00	4000.00 4008.00 3893.00	15 17
SHD REEL RT			49.85 104.21 126.99	1.83 35.78 43.18	3922.00 3921.00	3891.00	
TOTAL SHLO MERL			98.73 225.22	43.18 7.34 82.31	3923,00	3892.00 3875.00	
TOTAL SHOULDER			56.01	0.52 10.06	3922.00 3922.00 3984.00 3984.00	3875.00 3893.00 3884.00	8 9
LE LAP BELT			120.15	13.03 23.89	3984.00	3894.00 3894.00	
TOTAL LAP TOTAL LAP / HT CAOTCH STAAP			0.76 73.77 90.21	0.15 -33.81 -154.56	3989.00 3693.00	3898.00 3886.00	10 18
LF SERT LNK X			11.85 35.25	-152.89 -286.83	3762.00 3815.00	3886.00	19 35
TOTAL SEHI X			ua.92	-59.43 74.44	3970.00 3896.00 3894.00	3898.00 3621.00	11
LF SERT PRN Z			666.35 661.24 338.78	70.31	3694.00 3696.00 3896.00	3617.00 3606.00 3601.00	12
CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT			1683.42 10.53	182.31	3896.00 3896.00	3601.00 3601.00	
TOTAL SEAT Z / HT RES SEAT FORCE RES SEAT FORCE / H	T		1686.50 10.87	184.40	3896.00	3601.00 3888.00	20
LE FOOT X RT FOOT X	•		2.84 7.75	-119.42 -130.59 -135.75 -377.77	3838.00 3840.00	3890.00 3886.00	23 26
CT FOOT X TOTAL FOOT X			18.98 23.17 141.82	-377.77 -21.52	3839.00 3874.00	3889.00 3821.00	21
LF FOOT Y			24.94	-139,24 -45,55	4074.00 4178.00	3890.00	21 24 27
CT FOOT Y TOTAL FOOT Y			54.96 181.56	-80.09 -5.55	3851.00 3898.00 3897.00	3831.00	22 25 28
F FOOT Z AT FOOT Z CT FOOT Z			210.07 153.08	-73.00	3877.00	3850.00	28
TOTAL FOOT Z			456.19 570.21				

HEAD REST POS STUDY	TEST: 426	SUBJ: G-2	HT: 120.0	G: 10	GP: 2 CELL:	8
DATA 10		MAX	HIN	T1	T2	CH
IOV EXT PHR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z (SM)		10.05 1.20 0.78 12.48 10.67	9.96 -0.92 -0.95 -0.32 -0.11	2317.00 3831.00 3879.00 3869.00	1193.00 3868.00 3325.00 3664.00 3665.00	48 36 31 1
CARRIAGE VEL		-0.88 1.29	-25.68 -1.20 -1.40 -0.21	4186.00 3832.00 3851.00 3875.00	3828.00 3868.00 3843.00 3671.00	29 32 33 34
CHEST T CHEST Z CHEST RES		~0.14 15.77	-0.13 -1.07 -1.88 -1.11 1.10	3876.00 3892.00 3887.00 3903.00	3674.00 3922.00 3973.00 3631.00 3720.00	5 6 7
CHEST SI HEAD X HEAD Y HEAD Z HEAD Z HEAD RES HEAD SI		15.80 27.48 1.21 1.09 14.26 14.30 22.30	-1.15 -0.94 -0.80 0.36	3833.00 3884.00 3972.00 3888.00 3888.00	3979.00 3904.00 3895.00 3670.00 4129.00 3961.00	2 3 4
MERO HIC SHD REFL LF SHD REEL LF LF SHOULDER SHO REFL RT		16.48 47.38 30.01 71.27 94.88	10.93 7.69 29.35 13.43	3866.00 3908.00 3916.00 3915.00 3913.00	3928.00 3972.00 3871.00 3954.00 3999.00	14 16 15 17
SHD REEL AT AT SHOULDER TOTAL SHLO REEL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHO / MT LF LAP BELT		36.08 60.97 78.30 60.91 132.10 1.10 28.84	2.42 25.62 27.76 11.45 56.47 0.32	3974.00 3916.00 3910.00 3975.00 3916.00 3973.00	3883.00 4009.00 3981.00 3989.00 3999.00 3879.00	17 8 9
AT LAP BELT TOTAL LAP TOTAL LAP / HT CAOTCH STRAP LF SEAT LNK X AT SEAT LNK X		28.78 57.31 0.48 62.08 40.68 39.78 60.49	3.81 4.28 0.04 -23.90 -89.08 -118.43	3977.00 3975.00 3975.00 3975.00 3983.00 3839.00 3801.00	3878.00 3879.00 3879.00 3888.00 3882.00 3906.00 3891.00	10 18 19
TOTAL SERT X SERT LNK Y LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z HT RES SEAT FORCE		45.72 323.65 374.97 485.63 1143.51 9.53	-20.86 19.43 15.82 26.58 74.92 90.05	3941.00 3885.00 3885.00 3885.00 3885.00 3885.00	3848.00 3633.00 3692.00 3675.00 3667.00 3667.00	35 11 12 13
RES SEAT FORCE / NT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		1148.93 9.57 -0.91 -10.12 -8.75 -45.62 113.60	0.75 -94.34 -145.82 -166.16 -400.06 -27.62	3885.00 3836.00 4090.00 4174.00 3836.00 3870.00	3605.00 3886.00 3886.00 3882.00 3886.00 3952.00	20 23 26 21
RT FOOT Y CT FOOT Y TOTAL FOOT ? LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		21.21 51.51 66.19 166.19 183.59 182.19 430.54 527.28	-150.06 -20.58 -52.14 -17.63 -7.76 -95.76 -47.95 54.42	3849.00 3834.00 3853.00 3872.00 3879.00 3879.00 3879.00	3844.00 4140.00 3828.00 3828.00	27 22 25 28

HEAD REST POS STUDY	TEST: 390	SUBJ: K-1	HT: 175.0	G: 10	SP: 2 CELL:	В
DATA 10		HAX	MIN	T 1	72	CH
TOTAL LAP HEADO SHEELT TOTAL LAP PAN X Z Z CCHEST XY Z REBULL LOER TREEDLY TOTAL LAP PAN X Z Z CCHEST XY Z REBULL LAP BELT TOTAL LAP PAN X Z Z CCHEST XY Z REBULL LAP BELT TOTAL LAP PAN X Z Z CCHEST XY Z REBULL LAP BELT TOTAL LAP PAN X Z Z CCHEST XY Z CCHEST	•	0.5.2.5.8.2.5.4.4.7.66.3.5.8.1.1.6.6.2.2.7.3.6.2.2.5.8.2.1.1.5.0.3.5.6.3.8.1.1.1.5.0.3.7.3.6.2.2.3.3.5.6.3.8.1.1.5.0.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.5.6.3.8.1.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3	75471983455016 7961 65376201150437847395797527617804517802511000100 4110 267462782299323563142779957997804517804787847878478905382780552761780451780451780478784787847899058247805824780582478058247805824780582478058247805824780582478058247805824780582478049780665896431445169068484487894068784888888888888888888888888888888888	00000000000000000000000000000000000000	3603.00 3603.00 3603.00 3603.00 3849.00 3849.00 3849.00 3849.00 3851.00 3851.00 3851.00 3784.00 3784.00	96611 9234 567 234 46 57 89 089 5123 036 147 258

10	ORTH ID MAX	MIN	TI		6
CRRNINGE X CRARINGE T CRARINGE T CRARINGE T CRARINGE T CRARINGE Z CRACING Z CRARINGE Z CRARINGE Z CRACING Z	10V EXT PHR			12	CH
TOTAL FOOT Y LF FOOT Z AT FOOT Z TOTAL FOOT Z AT FOOT Z AT FOOT Z TOTAL FOOT Z AT FOOT Z AT FOOT Z BEST FOOT FOOCE BEST FOOCE BEST FOOT FOOCE BEST FOOCE BEST FOOT FOOCE BEST	CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Y CARRIAGE Y CARRIAGE Y CARRIAGE Y CARRIAGE CARRIAGE VEL 1.349 11.633 12.487 SERT Z SERT Z SERT Z CHEST Y CHEST Y CHEST X	235043333972 68808 1306598198342747479787315057742833333333333333333333333333333333333	00000000000000000000000000000000000000	00000000000000000000000000000000000000	9611 9234 567 234 46 57 89 089 5123 036 147

THE STATE OF CTURY	TEST: 423	SUBJ: MII	NT: 155.0	G: 10 G	P: 1 CELL:	8
MEND REST POS STUDY	1631, 465	MAX	MIN	T 1	15	CH.
THE CHEST Y CH		57 47 4 6 6 7 9 1 1 4 7 7 5 7 7 5 7 7 9 7 4 6 6 7 9 3 1 4 4 7 6 6 7 9 3 1 4 4 7 6 6 7 9 3 1 4 4 7 6 6 7 9 3 1 1 4 4 6 7 9 3 1 1 1 1 1 1 1 1 1 2 1 1 1 1 2 1 1 1 1	77861 7761 7761 7761 7761 7761 7761 7761	3906.00 3688.00 3907.00	3902.00 3900.00 4011.00 3994.00 3835.00 3994.00	9611 9294 567 234 46 57 89 089 5129 036 147 258

HERD REST POS STUDY	TEST: 381	SUBJ: M10	MT: 142.0	G: 10	GP: 2 CELL:	В
DATA ID		MAX	M1N	T 1	12	CH
IOV EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE VEL SERT X SERT X		10.05 1.34 0.62 12.32 10.52 -1.22 1.70 0.68	9.96 -0.97 -0.95 -0.17 -25.69 -1.24 -0.25	3344.00 3902.00 3901.00 3895.00 3896.00 4178.00 3861.00 3965.00	3221.00 3875.00 4008.00 3658.00 3759.00 3853.00 3876.00 3919.00	98611 992334
SEAT Z SEAT Z (SM) CHEST X CHEST Y CHEST Z CHEST RES CHEST S1 HEAD X		11.56 10.55 5.75 0.75 14.44 14.80 27.98 3.92	-0.15 -1.26 -2.89 -1.12 0.83	3903.00 3919.00 3899.00 3927.00 3927.00 3861.00 3915.00	3710.00 3954.00 3914.00 3840.00 3646.00 3995.00	5 6 7
MEAD Y MEAD Z MEAD RES MEAD SI		0.78 13.43 14.09 23.48	-1.86 -0.60 0.49	4011.00 3912.00 3914.00 3867.00 3868.00	3913.00 3735.00 3680.00 4094.00 3945.00	334
HEAD HIC SHD REFL LF SHD REEL LF LF SHOULDER		18.63 25.56 20.78 36.90	8.28 3.10 14.34	3931.00 4019.00 3951.00	3989.00 3917.00 3989.00	1 4 1 6
SHD REFL RT SHD REEL RT RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER		38.10 46.12 80.10 82.67 60.59 114.26 0.80 39.83 55.76 84.81	163.76 133.76 135.89 144.99 154.00 154.00	3940.00 3948.00 3941.00 3949.00 3943.00 4007.00 4011.00	3981.00 3908.00 4036.00 3989.00 3908.00 4043.00 3906.00 3907.00 3906.00	15 17 8 9
TOTAL LAP / HT CROTCH STRAP LF SEAT LNK X RT SEAT LNK X		8.15 48.80 28.69	-91.20 -136.54 -83.89	4011.00 4009.00 4186.00 3959.00	3914.00 3909.00 3908.00	10 18 19
TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z HT RES SEAT FORCE		60.02 55.08 371.97 387.43 780.82 1527.30 10.76	-218.57 -65.37 10.27 11.42 37.23 75.06 0.53 80.85 0.57	4139.00 3970.00 3906.00 3910.00 3912.00 3912.00 3912.00	3909.00 3909.00 3696.00 3696.00 3606.00 3606.00	35 11 12 13
RES SERT FORCE / NT LF FOOT X RT FOOT X CT FOOT X		10.87 -3.02 11.72 -1.36	-160.34 -101.95 -178.45 -436.27	3912.00 3608.00 3859.00 3859.00	3686.00 3913.00 3913.00 3914.00	20 23 26
TOTAL FOOT X LF FOOT T AT FOOT T CT FOOT Y		-9.84 156.42 24.26 18.14	-436.27 -17.40 -139.02 -52.17 -70.02	3859.00 3906.00 3729.00 3715.00	3913.00 3850.00 3897.00 3918.00	21 24 27
TOTAL FOOT Y LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		40.73 179.41 177.80 154.44 495.17 592.31	-70.02 -11.27 -0.51 -89.84 -59.65 38.11	3883.00 3906.00 3898.00 3917.00 3906.00	3918.00 3917.00 3852.00 4002.00 3875.00 3853.00 3650.00	22 25 28

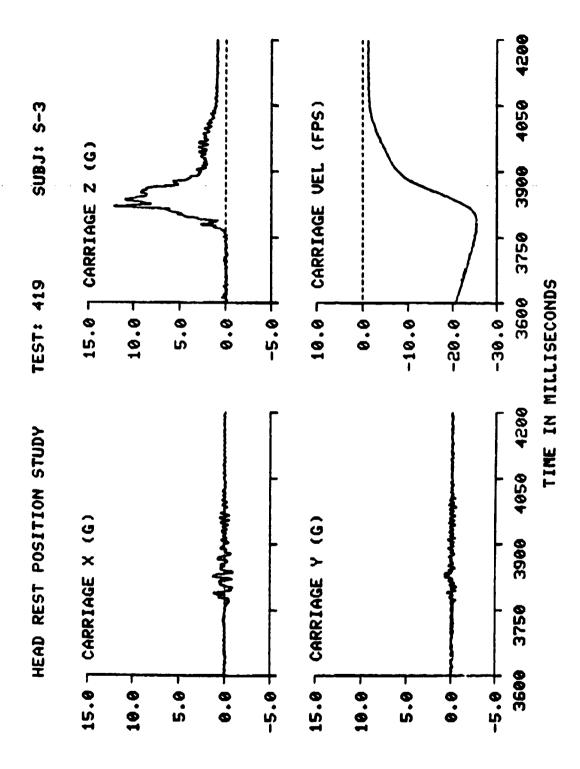
HEAD REST POS STUDY	TEST:	421	\$UBJ: H13	NT: 170.	0 G; 1C	GP: 1 CEL	
DATA ID			MAX	HIN			L: B
10V EXT PWR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE VEL			10.04 1.21 0.43 11.69	- 9862047881654893 7691 49756365852567699585554798567997:21259 - 98620530215197 3208 36927465994403205044998567997:21259 - 1-1-2-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	T - 7.0.1.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	72- 000000000000000000000000000000000000	E1 8611 9034 567 234 46 57 89 089 5129 036 147 258 200 200 200 200 200 200 200 200 200 20
					3922.00	3997.00	

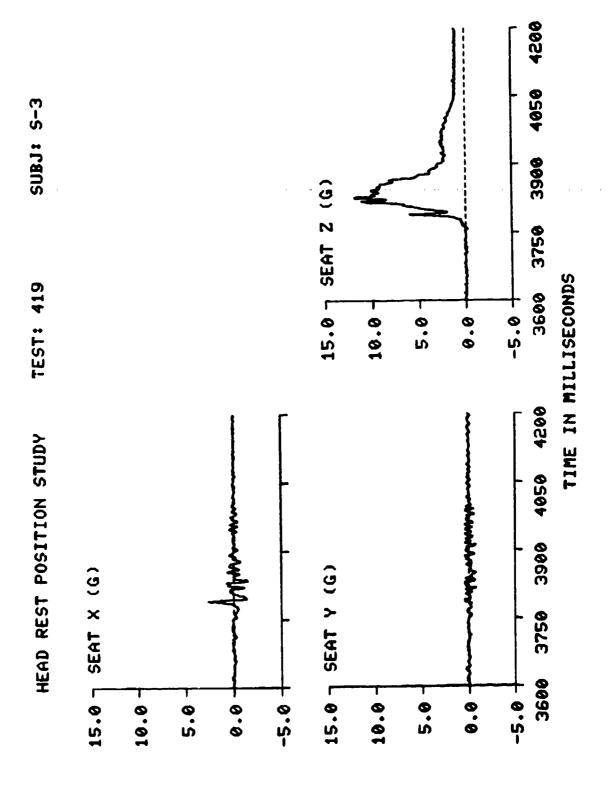
HEAD MEST POS STUDY	TEST: 379	\$UBJ: R-2	NT: 145.0	C: 10	GP: 1 CELL:	: B
DATA 10		MAX	HIN	T 1	15	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z (SH)		10.05 1.25 0.30 12.13 10.52	9.97 -0.78 -1.27 -0.22 -0.09	2313.00 3915.00 3912.00 3908.00 3924.00	1420.00 3924.00 4016.00 3696.00 3696.00	48 36 31 1
CARRIAGE VEL SEAT X SEAT Y SEAT Z SEAT Z (SM)		-1.16 2.04 0.91 12.46 10.93	-25.63 -1.45 -1.04 -0.19 -0.09	4141.00 3875.00 3982.00 3915.00 3916.00	3874.00 3923.00 3934.00 3699.00 3701.00	29 32 33 34
CHEST X CHEST Y CHEST Z CHEST RES CHEST SI		3.34 -0.20 15.33 15.61 22.76	-0.43 -2.08 -1.12 0.75	3917.00 3924.00 3947.00 3947.00 3877.00	3606.00 3945.00 3626.00 3740.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD RES HEAD SI		.93 1.36 15.76 13.79 19.18	-2.07 0.27 -1.15 0.80	3891.00 4055.00 3925.00 3925.00 3883.00	3954.00 3939.00 3845.00 4005.00 3992.00	2 3 4
HEAD HIC SHD REFL LF SHD REEL LF LF SHOULDER		15.52 48.30 33.35 79.76	20.43 9.46 40.20	3900.00 3546.00 4003.00 3947.00	3970.00 4012.00 3911.00 3910.00	14 16
SHD REFURT SHD REFURT AT SHOULDER TOTAL SHLO REFU TOTAL SHLO REEL TOTAL SHOULDER		90.72 30.63 68.63 87.01 62.66 146.92	17.10 9.55 36.38 38.54 20.01 80.25	3942.00 4013.00 3951.00 3945.00 4003.00 3951.00	3994.00 3996.00 4050.00 4011.00 3927.00	15 17
TOTAL SHD / NT LF LAP BELT BT LAP BELT TOTAL LAP TOTAL LAP / NT		1.01 47.80 58.54 105.17 0.73	0.55 8.08 19.96 29.39 0.20	3951.00 4014.00 4018.00 4017.00 4317.00	3910.00 3927.00 3932.00 3925.00 3925.00	8 9
CROTCH STRAP LF SEAT LNK X AT SEAT LNK X TOTAL SEAT X		20.99 61.50 58.32 67. 02	-38.03 -120.97 -53.64	4019.00 4022.00 3977.00	3924.00 3924.00 3921.00 3923.00	1 C 1 8 1 9
SEAT LAK Y LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE		78.14 267.24 326.53 950.01 1530.01 1539.00	-173.46 -7.81 12.10 20.86 85.98 132.69 138.28	3988.00 3979.00 3923.00 3926.00 3926.00 3925.00 3925.00	3917.00 3651.00 3601.00 3601.00 3601.00 3601.00	35 11 12 13
RES SEAT FORCE / WT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		10.61 1.75 10.03 23.58 32.72	0.95 -171.84 -133.60 -203.60 -499.35	3925.00 3676.00 3875.00 3876.00 3876.00	3601.00 3925.00 3927.00 3925.00 3925.00	56 53 50
LF F001 Y AT F001 Y C1 F001 Y T0TAL F001 Y		141.66 23.20 38.48 47.62	-19.93 -129.44 -53.18 -72.40	3920.00 3749.00 3876.00 3875.00	3895.00 3927.00 3928.00 3928.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		184.21 216.77 157.49 471.45 645.12	-4.79 -24.79 -98.90 -53.14 36.40	3919.00 3935.00 3941.00 3935.00	4038.00 3877.00 3887.00 3887.00 4004.00	22 25 28

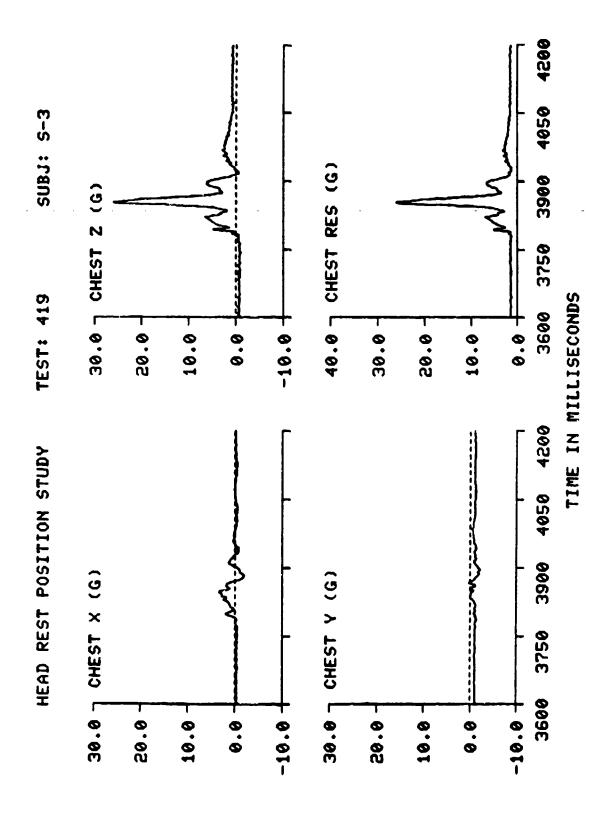
HEAD REST POS STUDY	TEST: 306	SUBJ: R-1	HT: 198.0	G: 10	GP: 2 CELL:	В
DATA ID		MAX	HIN	T1	15	CH
IDY EXT PWR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z		10.05 1.59 0.10 12.03 10.30	9.97 -1.26 -1.57 -0.27 -0.10	1037.00 3830.00 3865.00 3859.00 3874.00	842.00 3841.00 3814.00 3680.00 3656.00	48 36 31 1
CARRIAGE VEL SEAT X SEAT Y SEAT Z		-0.95 1.90 0.92 11.18	-25.85 -1.57 -1.22 -0.26	4187.00 3832.00 3826.00 3858.00	3825.00 3839.00 3636.00 3667.00	92 93 34
CHEST X CHEST T CHEST Z CHEST RES		10.12 7.58 0.33 16.28 19.73	-0.15 -0.66 -2.17 -1.58 0.94	3867.00 3891.00 3877.00 3893.00 3893.00	3641.00 3628.00 3895.00 3747.00 4164.00	5 6 7
CHEST SI HEAD X HEAD Y HEAD Z HEAD BES HEAD SI		94.10 2.39 1.31 11.49 11.74	-3.85 -1.26 -0.93 0.54	3825.00 3874.00 3969.00 3884.00 3884.00	3953.00 3920.00 3881.00 3747.00 4145.00 4063.00 3929.00	3
HEAD HIC SHD REFL LF SHD REEL LF LF SHOULDER		16.11 72.93 80.71	21.77 12.85 63.08	3856.00 3911.00 3910.00 3910.00	4100.00 3871.00 3869.00	1 4 1 6
SHD REFL RT SHD REEL RT AT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHOULDER		133.31 59.59 71.61 127.95 132.02 127.97 258.24	36.48 12.33 50.18 25.18 113.61 23.77 42.38	3905.00 3970.00 3906.00 3911.00 3908.00	3985.00 3871.00 3869.00 3986.00 3871.00 3869.00	15 17
TOTAL SHD / HT LF LAP BELT RT LAP BELT TOTAL LAP TOTAL LAP / HT		1.30 46.96 73.88 119.43 0.60		3909,00 3915.00 3915.00 3915.00 3915.00	3869.00 3859.00 3859.00 3859.00 3859.00	8 9
CROTCH STRAP LF SEAT LNK X AT BEAT LNK X		246.46 33.17 18.80	0.33 -82.83 -147.57 -138.31	3970.00 3962.00 3833.00	3888.00 3875.00 3876.00	10 18 19
TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT AES SEAT FORCE		17.61 46.49 449.77 690.91 762.16 1897.87 1917.98	-52.78 -52.78 48.62 55.63 184.69	4112.00 3958.00 3878.00 3876.00 3878.00 3878.00 3878.00	3875.00 3884.00 3672.00 3606.00 3600.00 3604.00 3604.00	35 11 12 13
RÉS SERT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		9,69 -52,51 -20,50 -67,42 -144,95	0.84 -257.86 -203.78 -306.23 -741.65	3878.00 3827.00 3830.00 3830.00 3830.00	3604.00 3674.00 3877.00 3876.00 3876.00	20 23 26
LF FOOT 1 AT FOOT T CT FOOT Y TOTAL FOOT Y LF FOOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		187. C4 24.89 32.48 72.30 295.53 286.33 146.35 632.02 942.13	-21.71 -182.97 -56.51 -77.58.20 -52.97 -189.89 -14.84 243.51	3870.00 4007.00 3853.00 3853.00 3877.00 5863.00 3879.00 3879.00	4094.00 3676.00 3882.00 3821.00 3821.00 4125.00 3821.00 4114.00	21 27 22 25 28

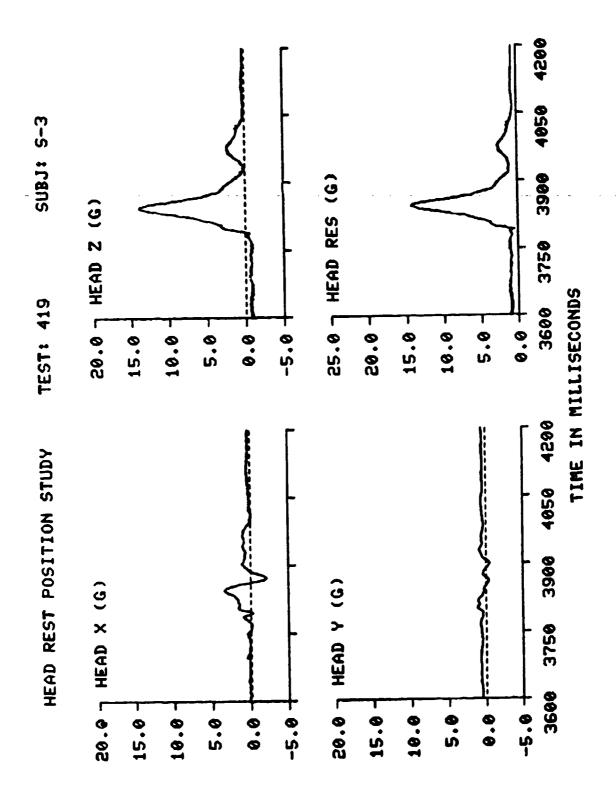
HERD REST POS STUDY	TEST: 440	SUBJ: R-3	MT: 147.0	G: 10	GP: 2 CELL:	8
DATA ID		MAX	MIN	T1	72	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z (SM)		10.05 1.60 0.62 12.04	9.98 -0.69 -0.30	634.00 3865.00 3663.00 3656.00	600.00 3838.00 3641.00 3669.00	48 36 31
CARRIAGE VEL SEAT X SEAT Y SEAT Z		10.55 -0.96 1.16 1.18 12.15	-0.15 -25.95 -1.20 -1.35 -0.15	9658.00 4114.00 3866.00 3824.00 3864.00	3668.00 3818.00 3871.00 3831.00 3877.00	32 32 39
CHEST X CHEST T CHEST Z CHEST RES		16.69 16.69	-0.10 -0.67 -3.50 -1.85 1.56	3864.00 3879.00 3873.00 3893.00 3893.00	3739.00 3916.00 3880.00 3857.00 4198.00	5 8 7
CHEST SI HEAD X HEAD Y HEAD Z HEAD RES HEAD SI HEAD HIC		27.62 1.19 2.09 19.71 19.76 19.97 15.23	-3.05 0.55 -1.18 1.24	3825.00 3977.00 4035.00 3676.00 3876.00 3833.00	3951.00 3919.00 3890.00 3722.00 4085.00	2 3 4
SHD REFL LF SHD REEL LF LF SHOULDER		15.23 38.72 19.16 54.55	7.91 5.24 15.71	3656.00 3907.00 4063.00 3910.00	3905.00 4087.00 3663.00 3956.00	1 4 1 6
SHD REFL RT SHD REEL RT RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL		39.07 20.23 48.42 73.08	12.46 2.31 25.92 23.05	3879.00 3966.00 3903.00 3883.00	3952.00 3869.00 4049.00 3954.00	15 17
TOTAL SHOULDER TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / HT		37.31 96.22 0.87 49.99 69.94 107.05	8.64 50.25 0.34 11.04 16.69 29.44	3925.00 3910.00 3910.00 3971.00 3967.00 3969.00	3864.00 3956.00 3956.00 3880.00 3879.00 3889.00	8 9
CROTCH STAAP LF SEAT LNK X BT SEAT LNK X		37.96 40.18 11.44	0.20 -57.37 -172.22 -64.64	3968.00 3967.00 3829.00	3875.00 3872.00 3877.00	10 18 19
TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z / HT RES SEAT FORCE		40.60 58.71 470.65 363.66 723.74 1572.24 10.70 1591.42	-235.62 -88.37 38.96 35.48 56.49 142.51 0.97	4194.00 3941.00 3878.00 3878.00 3878.00 3878.00	3872.00 3873.00 3835.00 3802.00 3805.00 3815.00	35 11 12 13
RES SEAT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		5.79 8.41 59.80 66.83	-113.56 -82.35 -139.65 -324.75	3878.00 3828.00 3805.00 3828.00 3825.00	3615.00 3671.00 3675.00 3875.00 3875.00	20 23 26
LF FOOT Y RT FOOT T CT FOOT T TOTAL FOOT Y		141.00 24.05 21.84 87.62 187.87	-15.36 -134.80 -38.68 -73.24	3860.00 4156.00 3823.00 3845.00	3833.00 3860.00 3879.00 3876.00	21 27
LF FOOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z MES FOOT FORCE		167.87 166.71 172.80 455.83 548.73	-9.31 -11.55 -61.56 -31.82 16.29	3560.00 3564.00 3566.00 3661.00 3664.00	3719.00 3682.00 3633.00 3834.00 3672.00	22 25 26

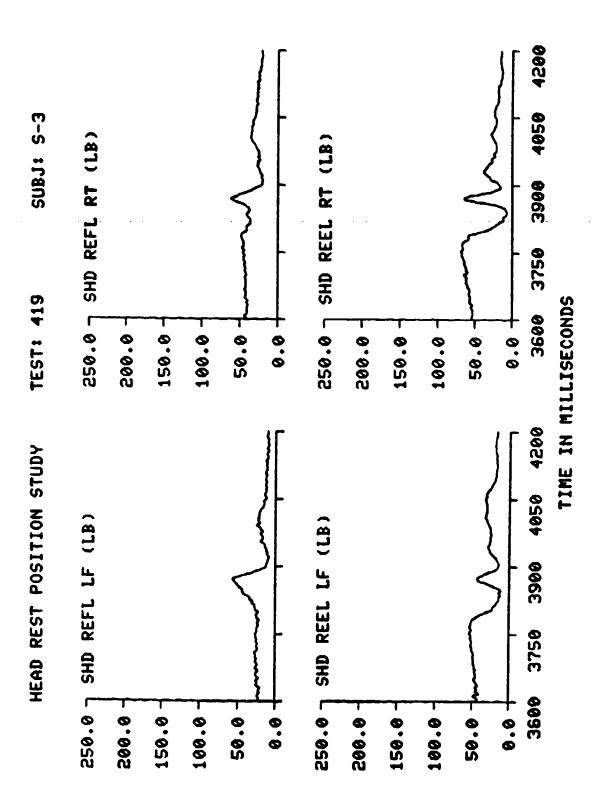
HEAD REST POS STUDY	TEST: 419	\$98Ji \$-3	WT: 166.0	G: 10	GP: 2 CELL:	В
DATA 10		HAX	MIN	T1	15	CH
IDV EXT PHR CARRIAGE X CARRIAGE T CHARIAGE Z CARRIAGE Z CARRIAGE Z (SM)		10.04 1.29 0.76 12.18 10.40	9.96 -0.95 -0.69 -0.26	139.00 3827.00 3833.00 3821.00 3821.00	3182.00 3836.00 3803.00 3710.00 3630.00	36 31
CARRIAGE VEL SEAT X SEAT T		-1.06 2.67 0.5! 11.84	-0.12 -25.55 -0.82 -0.23	4162.00 3790.00 3788.50 3827.00	3760.00 3835.00 3849.00 3758.00	29 32 -33 34
SERT Z SERT Z (SM) CHEST X CHEST T CHEST T CHEST RES CHEST SI		10.64 3.38 0.24 26.01 26.04	-0.13 -1.93 -2.17 -0.99	3828.00 3846.00 3867.00 3852.00 3852.00	3654.00 3882.00 3896.00 3742.00 3700.00	5 6 7
HERD X HERD Y HERD Z HERD RES HERD SI		45.04 9.47 1.14	-2.07 -0.50 -1.00 0.45	3845.00 3802.00 3844.00 3844.00 3795.00	3913.00 3872.00 3899.00 3603.00 3791.00	23
MEAD HIC SHD REFL LF SHD REEL LF LF SHOULDER SHD REFL RT		14.28 142.19 156.693 98.97	9.08 11.15 25.74	3818.00 3870.00 3874.00 3871.00	3871.00 3920.00 3846.00 3904.00	14
SHO REEL AT SHO REEL AT AT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER		61.93 64.21 124.78 118.11 106.66 223.37	20.54 6.33 38.01 10.472 64.72 0.39 14.22	3868.00 3871.00 3870.00 3869.00 3871.00 3870.00	3910.00 3839.00 3930.00 3920.00 3837.00 3902.00	15
LF LAP BELT MT LAP BELT TOTAL LAP TOTAL LAP CROTCH STRAP		1.35 43.67 53.16 95.97 0.58	38.01	3870.00 3927.00 3931.00 3929.00 3929.00 3939.00	3902.00 3853.00 3853.00 3853.00 3853.00	8 9
LF SEAT LNK X BT SEAT LNK X TOTAL SEAT X		116.46 24.35 26.26 25.25	-50.40 -213.95 -101.78 -315.15 -108.70	3607.00 3791.00 3607.00	3837.00 3635.00 3836.00	10 16 19
SEAT LNK Y LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z / HT RES SEAT FORCE		26.254 26	61.70 46.32 49.08 164.11	3938.00 3845.00 3846.00 3846.00 3846.00 3846.00	3844.00 3603.00 4200.00 3604.00 3604.00 3604.00	35 11 12 13
RES SEAT FORCE / HT LF FOOT X AT FOOT X CT FOOT X TOTAL FOOT X		4.43 14.45 3 5.10 48.69	166.56 1.00 -157.41 -142.40 -203.71 -489.05	3846.00 3768.00 3787.00 3788.00 3788.00	3604.00 3647.00 3847.00 3846.00 3847.00 3796.00	20 23 26
LF FOOT Y AT FOOT Y CT FOOT Y TOTAL FOOT Y		124.00 21.60 32.54	-28.24 -142.38 -53.79 -64.46	3823.00 3731.00 3643.00 3862.00 3847.00	3632.00 3632.00	21 27
LF FÖOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FOACE		201.13 201.13 258.06 170.05 558.45 741.44	-18.22 -5.15 -63.59 -45.58 42.15	3848.00 3843.00 3845.00 3847.00	3965.00 3951.00 3779.00 3779.00 3950.00	22 25 26

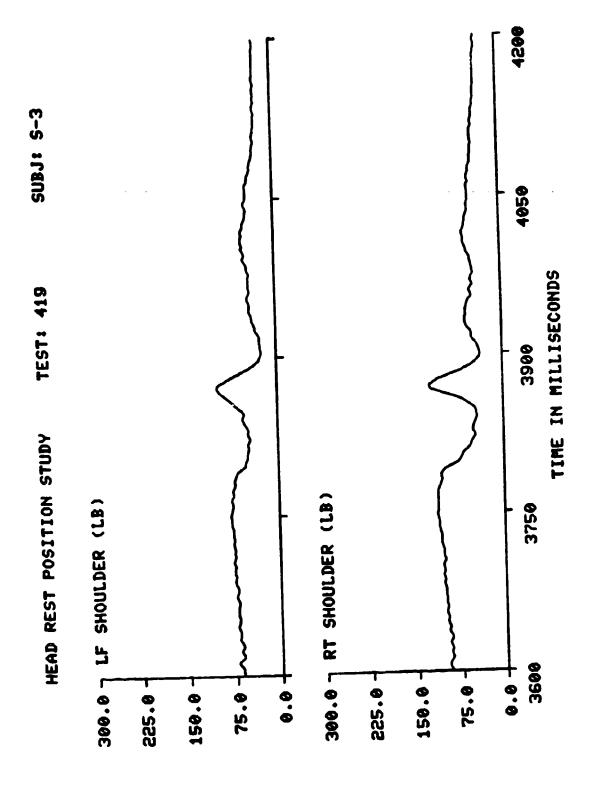


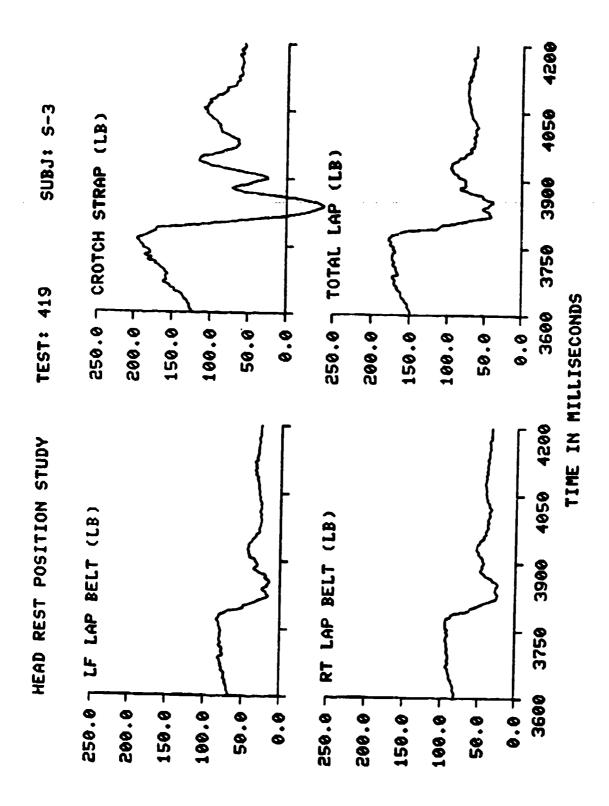






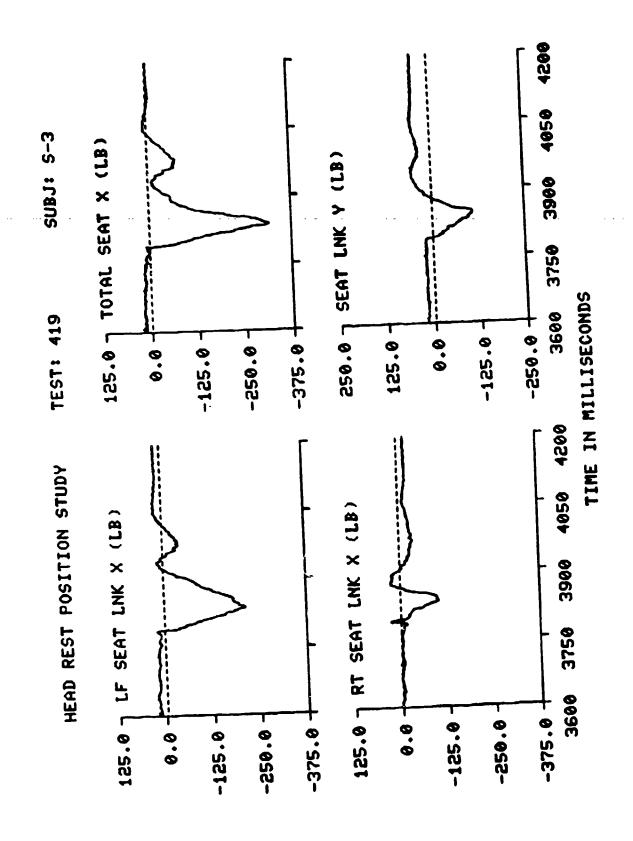


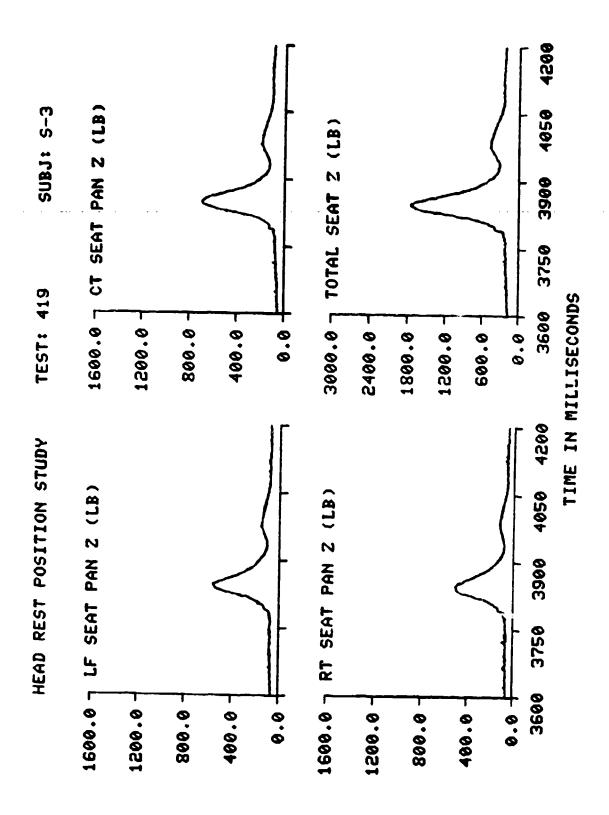


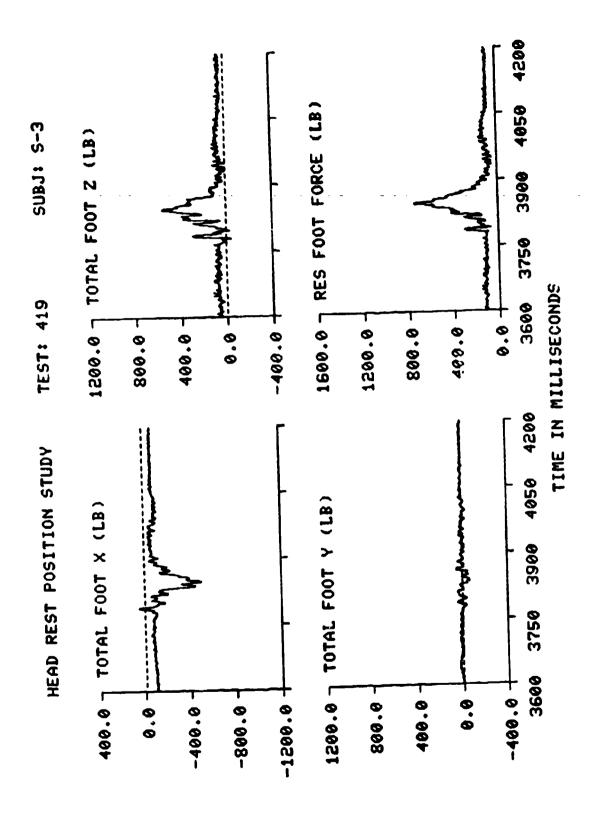


Trible Command

3-







HERD BEST PES STUDY	1257: 360	503J: 3-:	AT: 210.0	G: 10	G∂: 1 (2200:	c
DATA 10		MAX	HIN	T1	15	CH
10V EXT PAR CRRETAGE X CRRETAGE Y CHRETAGE Z		10.05 1.34 0.74 12.06	9.97 -0.91 -1.00 -0.24	2258.00 3865.00 3865.00 3858.00	435.00 3830.00 3609.00 3661.00	48 36 31
CARAIAGÉ Ž (SM) CARAIAGÉ VEL SEAT X SEAT Z		10.51 -1.11 1.93 0.81 11.57	-0.08 -25.82 -1.34 -0.99 -0.26	3858.00 4153.00 3823.00 3958.00 3863.00	3654.00 3832.00 3829.00 5844.00 3630.00	29 32 53 34
SERT Z (SM) CHEST X CHEST Z CHEST Z		10.59 5.23 -0.28 16.73	-0.16 -1.60 -3.22 -1.27 0.77	3864.00 3878.00 3856.00 3895.00	3687.00 3910.00 3897.00 3638.00	5 6 7
CHEST RES CHEST SI HERD X HERD Y HERD Z		17.17 27.57 .09 2.08	-4.62 0.28	3893.00 3827.00 3733.00 3868.00	4141.00 3953.00 3968.00 3980.00	2
HERD RES HERD SI MERD HIC SHO REFL LF		13.74 14.02 21.47 16.33 59.61	-1.32 0.67 23.19	3876.00 3876.00 3831.00 3850.00 3884.00	3698.00 3988.00 3964.00 3921.00 3973.00	14
SHD REEL LE LE SHOULDER SHD REEL RT SHD REEL RT		56.03 97.16 54.51 41.06	9.25 55.39 16.10 2.93	3931.00 3907.00 3902.00 3909.00	3872.00 3983.00 4100.00 3860.00	15 17
NT SHOULDER TOTRL SHLD REFL TOTRL SHLD REEL TOTRL SHOULDER		92.79 105.38 95.09 1 69.9 5	37.11 46.37 13.03 93.74	3907.00 3696.00 3909.00 3907.00	3850.00 3974.00 3869.00 3860.00	
TOTAL SHO / HT LA LAP BELT BT LAP BELT TOTAL LAP TOTAL LAP / HT		0.90 56.81 43.31 95.53 0.45	0.45 32.18 27.65 59.92 0.29	3970.00 3970.00 4052.00 3970.00	3860.00 3858.00 3859.00 3858.00 3858.00	8 9
CROTCH STRAP LF SEAT LNK X AT SEAT LNK X TOTAL SEAT X		263.31 52.29 30.01 69.06	-13.43 -172.19 -94.32 -265.36	3960.00 4095.00 3937.00 3937.00	3880.00 3878.00 3873.00 3873.00	10 18 19
SERT LNK T LF SERT PRN Z RT SERT PRN Z CT SERT PRN Z TOTAL SERT Z TOTAL SERT Z / NT RES SERT FORCE		76.12 587.40 457.49 1166.54 2210.54 10.53 2226.09	-42.33 38.59 35.90 91.54 173.85 0.83 175.45	3924.00 3876.00 3875.00 3876.00 3876.00 3876.00	3876,00 3695.00 3620.00 3515.00 3602.00 3602.00 3502.00	35 11 12 13
RES SERT FORCE / WT LF FOOT X AT FOOT X CT FOOT X TOTAL FOOT X		10.60 26.44 11.81 30.50 67.21	0.84 -154.13 -139.67 -207.42 -571.22	3876.00 3824.00 3823.00 3825.00 3824.00	3602.00 3875.00 3875.00 3876.00 3876.00	20 23 26
LF F00T T AT F00T T CT F00T T T0TAL F00T T		156.30 26.09 19.83 46.38	-23.64 -169.14 -37.13 -48.84	3859.00 3824.00 3896.00 3896.00	3832.00 3868.00 3835.00 3833.00	21 24 27
LF FOOT Z RT FCCT Z CT FCCT Z TOTAL FOOT Z RES FOOT FOACE		196.13 251.58 171.56 599.02 765.67	-34.90 0.89 -77.91 -37.04 40.29	3869.00 3861.00 3864.00 3869.00	3964.00 3972.00 3635.00 3810.00 3973.00	22 25 28

HEAD REST POS STUDY	TEST: 406	SUB J.	F-3	HT: 166.0	G: 10 C	P: 1 CELLI	С
DATA 10			MAX	MIN	T1	12	CH
TOTALL SHEET TOTAL SERT TOTAL SHEER TOTAL SHEER TOTAL SHEER TOTAL SHEET TOTAL SHEER TOTAL SHEER TOTAL SHEER TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET SHEET TOTAL SHEET			00005027623521869881295056422462969754320912339955277749862102 063240874401122554557593134958052687540625405913555777498621494 0102011030997 133960984424339165109897493174000813553287525 0102011030997 1339604442433916510887749317400081207328725 01102011030997 133960444243391651088774931691 257322328725	9904925077456686 5280 388385353415400068972100349687 9398 43888392867.1540004687 9398 43888392867.16527069.79.89.79.79.79.79.79.79.79.79.79.79.79.79.79	00000000000000000000000000000000000000	3912.00 3913.00 3924.00 3934.00 3854.00 3854.00	98611 9234 567 234 48 57 89 089 5123 036 147 258

HEAD REST POS STUDY	TEST: 422	SUBJ: F-2	WT: 161.9	G: 10	GP: 1 CECL:	ε
DATA 1D		MAX	MIN	T1	T2	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z (SM)		10.05 1.20 0.56 12.34	9.97 -0.85 -0.87 -0.15	128.00 3840.00 3839.00 3833.00	167.00 3809.00 3818.00 3641.00	48 36 31
CARRIAGE VEL SEAT X SEAT Y SEAT Z		10.52 -0.90 1.15 0.84	-0.06 -25.04 -1.34 -1.72	3834.00 4111.00 3799.00 3797.00	3691.00 3799.00 3848.00 3811.00	29 32 33 34 56 7
SÉRT Z (SM) Chest X		12.52 10.66 3.68	-1.72 -0.22 -0.13 -2.56	3840.00 3840.00 3860.00	3670.00 3669.00 3886.00	34 5
CHEST Y CHEST Z CHEST RES CHEST SI HEAD X		-0.03 22.68 23.17 38.10	-2.04 -0.78 0.71	3820.00 3856.00 3856.00 3797.00	3914.00 3673.00 3791.00	6 7
HEAD X HEAD Y HEAD Z HEAD RES		1.95 0.78 14.62	-4.47 -1.77 -0.78 0.56	3854.00 3899.00 3854.00 3854.00	3932.00 3687.00 3850.00 3674.00 4125.00	2 3 4
HEAD SI HEAD HIC SHD REFL LF SHD REEL LF		14.82 23.25 18.36 44.59	14.82	3805.00 3833.00 3869.00	3954.00 3894.00 3945.00	14
LF SHOULDER SHO REFL RT SHO REEL RT		62.49 98.11 64.46 95.08	6.41 26.04 24.93 9.86	3688.C0 3887.00 3873.00 3880.00	3847.00 3975.00 4097.00 3852.00	15 17
RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER		156.48 107.94 141.31 240.70	9.86 42.43 40.94 16.54 72.54 7.11	3880.00 3880.00 9871.00 3863.00 3861.00 3881.00	3852.00 3846.00 4100.00 3846.00 3846.00	• •
LF LAP BELT TO TAL LAP TOTAL LAP CROTCH_STRAP		30.36 34.60 62.81 0.39	7.11 14.43 22.38 0.14	3956.00 3942.00 3947.00 3947.00	3840.00 3843.00 3834.00 3834.00	8
CROTCH STRAP LF SEAT LNK X AT SEAT LNK X TOTAL SEAT X		156.17 20.27 8.62 11.90	-23.13 -268.10 -130.55	3692.00 4177.00 3680.00 3625.00	3851.00 3852.00	10 18 19
SEAT LNK Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z		54.61 504.76 407.75	-395.60 -112.45 17.53 8.48	3936.00 3857.00 3852.00	3855.00 3853.00 3852.00 3608.00 3611.00	35 11 12 13
TOTAL SEAT Z / HT RES SEAT FORCE		795.21 1706.14 10.60 1754.69	26.82 65.48 0.41 68.86	3855.00 3855.00 3855.00 3855.00 3855.00	3611.00 3611.00 3611.00	13
RES SERT FORCE / HT LF FOOT X RT FOOT X CT FOOT X		10.90 1.14 -4.71 -22.86 -30.83	0.43 -100.12 -150.10 -182.07	3801.00	3611.00 3849.00 3851.00 3851.00	20 23 26
TOTAL FOOT X LF FOOT Y RT FOOT Y CT FOOT Y		120.43 23.55	-182.07 -425.15 -35.92 -178.12 -14.08	3801.00 3836.00 4039.00 3875.00	3850.00 3808.00 3844.00 9993.00	21 24 27
TOTAL FOOT Y LF FOOT Z AT FOOT Z CT FOOT Z		84.42 209.04 201.53	-35.92 -178.12 -180.63 -80.63 -81.85 -81.85 -2.50	3815.00 3837.00 3844.00 3843.00	3845.00 3794.00 3952.00 3864.00	22 25 28
TOTAL FOOT Z RES FOOT FORCE		189.14 537.13 616.31	-2.50 104.25	3844.00 3844.00	3793.00 4188.00	<i>2</i> 0

HEAD REST POS STU	TEST: 387	SUBJ: G-3	MT: 159.0	G: 10	GP: 2 CELL:	С
DATA 10		MAX	MIN	T 1	12	CH
PXYZZEL PXXZZZEL PXYZZEL PXYZZEL PXYZZEL PXYZZEL PXYZZEL PXYZZEL PXXZZZEL PXZZEL PXXZZZEL PXZZEL PXXZZZEL PXZZEL PXXZZZEL PXXZZZEL PXZZEL P	T NT	92329467994906995823176994178652165275556177827708229958913078539078539000000000000000000000000000000000000	978428591903019 7493 979873596107775527405185227748570369 90000511001300 6010 1223426509330437908482227748565552348222774857045777686282829 12234265093314522329030133770457776862829 122342650933145223297777777777777777777777777777777777	00000000000000000000000000000000000000	3601.00 3601.00 3601.00 3900.00 3900.00 3900.00 3900.00 3900.00 3900.00 3900.00 3900.00 3900.00 3900.00 3900.00	935 035 567 234 46 57 89 089 5125 036 147 256 111 9111 91111 222 222 222

HERD REST POS STUDY	TEST: 380	SUBJ: G-2	HT: 120.0	G: 10	GP: 2 CELL:	C
DATA 10		MAX	HIN	T1	15	CH
IOV EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z		10.05 1.20 0.77 12.41	9.96 -1.02 -1.00 -0.18	2845.00 3856.00 3653.00 3847.00 3847.00	905.00 3846.00 3955.00 3763.00 8854.00	48 36 31
CARRIAGE Z (SM) CARRIAGE VEL SEAT X SEAT Z SEAT Z SEAT Z SEAT Z		10.66 -0.91 1.96 0.71	-0.10 -25.62 -1.37 -0.60 -0.27 -0.17	4151.00 3857.00 3967.00 3853.00 3854.00	3816.00 3862.00 3861.00 3663.00 3663.00	29 32 33 34
CHEST X CHEST Y CHEST Z CHEST RES		10.81 3.85 0.93 22.74 22.87 95.13	-2.13 -2.42 -0.88 0.63	3864.00 3886.00 3879.00 3879.00 8813.00	3910.00 3879.00 3786.00 9726.00 4062.00	5 6 7
CHEST SI HEAD X HEAD Y HEAD Z HEAD RES HEAD SI		0.54 0.83	-5.75 -0.87 -0.90 0.40	3973.00 3920.00 3868.00 3868.00	3910.00 3871.00 3621.00 4129.00 3943.00	3
HEAD HIC SHD REFL LF SHD REEL LF		12.42 18.48 15.37 45.28 78.74	13.18	3842.00 3888.00 3903.00	3921.00 3956.00 3646.00 3978.00	14 16
LF SHOULDER SHD REFL RT SHD REEL RT RT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHUDDER		57.45 53.32 88.38 72.40 98.47	24.44 15.70 2.81 19.94 31.40 9.92 46.43	3904.00 3911.00 3904.00 3904.00 3697.00 3904.00	3983.00 3852.00 3986.00 4089.00 3858.00	15 17
TÖTRL SHO / NT LF LRP BELT RT LAP BELT TOTAL LAP		25.95 25.95 26.92 54.69 0.46	0.39 2.28 6.60 10.05 0.08	3904.00 3926.00 3938.00 3938.00	3979.00 3847.00 3650.00 3647.00 3847.00	8
CROTCH STRAP LF SEAT LNK X AT 3FAT LNK X		41.98 41.51 92.97 49.04	-27.67 -123.11 -42.49 -163.13	3948.00 3969.00 3813.00 3790.00	3668.00 3662.00 3665.00	10 18 19
TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z		49.04 56.70 355.95 380.11 623.02 1329.03 11.08 1338.79	-25.62 17.04 15.26 36.73 82.45	3912.00 3865.00 3865.00 3670.00	3667.00 3681.00 3652.00 3667.00	35 11 12 13
RES SERT FORCE RES SERT FORCE / MT LF FOOT X RT FOOT X TOTAL FOOT X		11.15 15.91 7.91 19.32 24.23	90.65 0.76 -39.24 -118.98 -103.22 -246.99	3865.00 3865.00 3865.00 3943.00 3810.00 3811.00	3855.00 3855.00 3865.00	20 23 26
LF FOOT T MT POOT T CT FOOT Y TOTAL FOOT Y		65.39 17.77 50.07 34.70 119.82	-15.84 -97.60 -22.91 -41.51	3850.00 3829.00 3862.00 4018.00	3931.00 3858.00 3960.00 3915.00	21 24 27
LF FOOT Z NT FOOT Z CT FOOT Z TOTAL FOOT Z NES FOOT FORCE		119.82 151.38 181.70 389.29 395.06	-29.65 -20.92 -53.52 -68.76 7.68	3674.00 3859.00 3655.00 3657.00 8857.00	3959.00 3959.00 3959.00	22 25 28

HERD REST POS STUDY TEST: 371	SUBJ: K-1	WT: 175.0	G: 10	Ch: 5 CEFF:	С
DATA 10	HRX	MIN	T1	12	CH
IOV EXT PHR CARRIAGE X CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE VEL SEAT Y SEAT Z SEAT Z SEAT Z CHEST X CHEST X CHEST X CHEST X CHEST SI HEAD Y HEAD Z HEAD SI	10.06 1.444 10.474 10.610 10.867 110.631 110.6	9.97 -0.81 -0.94 -0.71 -0.20 -25.63 -1.15 -0.31 -1.75 -0.68 -1.75 -0.58	388822000000000000000000000000000000000	389.00 38837.00 38837.00 3803.00 3803.00 3897.00 3897.00 3911.00 3914.00 3914.00 3914.00 3937.00 3937.00 3937.00	98611 9N33 567 N34
HERD HIC SHO REFL LF SHO REEL LF SHO REEL LF LF SHOULDER SHD REEL RT RT SHOULDER TOTAL SHLO REFL TOTAL SHLO REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER	13.07 35.36 35.35 93.35 94.85 92.29 80.21 737.30 96.99	17.580 17.580 14.68 14.64 29.63 99.63 60.38	3881043116000000000000000000000000000000000	3948.00 4014.00 3884.00 3882.00 4002.00 3988.00 4000 3884.00 3884.00 3884.00 3884.00	14 16 15 17
AT LAP BELT TOTAL LAP TOTAL LAP TOTAL LAP TOTAL LAP LF SEAT LNK X AT SEAT LNK X SEAT LNK Y LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT FORCE	102.82 07.59 117.28 16.07 40.55 10.62 45.80 670.04 669.31 739.19 2064.17	9.633556202215393560063755 6.2355.3543935600655019 7.213874246.566665755 1.213874346.566663755 1.213874346.566663755	3734.00 3671.00 3967.00 3903.00 3906.00 3906.00	1050.00 1075.00 1075.00 3898.00 3901.00 3908.00 3908.00 3908.00 3607.00 3610.00 3603.00 3603.00 3603.00	9 10 18 19 35 11 12
RES SEAT FORCE / WT LF FOOT X RT FOOT X RT FOOT X TOTAL FOOT X LF FOOT Y AT FOOT Y TOTAL FOOT Y LF FOOT Z AT FOOT Z TOTAL FOOT Z RT FOOT Z RES FOOT FORCE	12.00 10.65 13.02 34.01 55.86 115.12 22.37 36.62 185.79 185.79 185.79 185.79 185.79	-91.53 -91.53 -91.57 -197.15 -296.99 -134.18 -557.46 -18.89 -8.79 -44.03 -34.03	3906.000 388476.000 388476.000 388476.000 388476.000 38835.000 38855.000 38855.000 38855.000	3603.00 3699.00 3900.00 3900.00 4038.00 3884.00 3894.00 3894.00 4145.00 4145.00	2036 2147 2558

HERD REST POS STUDY	TEST: 424	SUBJ: M-2	NT: 163.0	G: 10	GP: 1 CELL:	C
DATA 10		HAX	MIN	T1	12	CH
IOV EXT PWR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE VEL		10.05 0.97 0.77 12.25 10.43	9.96 -0.95 -0.68 -0.22 -0.11	1821.00 3867.00 3831.00 3860.00 3861.00	1474.00 3837.00 3836.00 3722.00 3757.00	48 36 31 1
SERT X SERT Z SERT Z SERT Z (SH)		-1.20 1.32 0.77 11.97 10.63	-25.85 -1.17 -0.98 -0.14 -0.09	4184.00 3830.00 3827.00 3867.00 3867.00	3818.00 3874.00 3834.00 3615.00 3717.00	32 33 34
CHEST X CHEST Z CHEST RES CHEST SI		1.93 0.24 20.08 20.15 33.38	-4.10 -1.28 -0.95 0.94	3867.00 3917.00 3898.00 3898.00 3827.00	3917.00 3848.00 3682.00 3811.00 3963.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD SI HEAD HIC		2.16 1.16 11.31 11.63 15.06 9.48	-5.99 -1.89 -1.23 0.55	3881.00 3951.00 3878.00 3878.00 3837.00 3857.00	3925.00 3883.00 3646.00 4148.00 4020.00 390!.00	3
SHD REFL LF SHD REEL LF LF SHOULDER SHD REFL RT		86.72 71.06 149.23 59.78	24.03 10.64 42.20 34.12	3920.00 3909.00 3911.00 3910.00	3990.00 3872.00 3862.00 3860.00	14 16 15
SHD REEL RT RT SHOULDER TOTAL SHLD REEL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHO / WT		84.29 143.54 142.92 152.73 292.51	12.99 48.52 62.21 24.30 91.82 0.56	3913.00 3912.00 3917.00 3911.00 3911.00	3868.00 3865.00 3990.00 3870.00 3863.00 3863.00 3867.00	17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP CROTCH STRAP		36.54 56.07 91.44 0.56 126.53	11.47 19.84 3!.33 0.19 -45.20	3974.00 3941.00 3967.00 3967.00 3950.00	3867.00 3868.00 3868.00 3068.00 3885.00	9
LF SEAT LNK K AT SEAT LNK K TOTAL SEAT X		44.81 26.21 35.57	-177.00 -91.91 -267.07	4124.00 5831.00 4124.00	3876.00 3882.00 3876.00	18
SEAT LNK T LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FOACE		78.45 363.10 403.62 904.02 1665.17 10.22 1686.06	-56.53 34.14 33.58 72.29 150.83 0.93 153.18	3949.00 3877.00 3877.00 3881.00 3881.00 3881.00	3882.00 3774.00 3623.00 3623.00 3623.00 3623.00	35 11 12 13
RES SEAT FORC / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		10.34 10.79 -6.78 0.30 -14.55	0.94 -57.01 -130.15 -135.65 -312.88	3681.00 3627.00 4181.00 3830.00 3828.00	3623.00 3875.00 3878.00 3877.00 3878.00	26 23 20
TT FOOT Y CT FOOT Y TOTAL FOOT Y LF FOOT Z RT FCOT Z		101.27 16.75 47.49 58.55 192.38 166.41	-26.26 -135.88 -30.83 -90.77 -25.40 -5.58	3862.00 3740.00 3899.00 3843.00 3864.00 3878.00	3835.00 3871.00 3927.00 3835.00 3834.00 3834.00	21 24 27 22 25
CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		172.21 431.83 504.36	-78.52 -24.68 83.17	3828.00 3872.00 3872.00	3844.00 3821.00 3654.00	28

TOUTS DECT DES STUDY	TEST: 378	SUBJ:	H11	HT: 157.0	G: 10 G	P: 1 CELL:	Ļ
HEAD REST POS STUDY DATA ID	16311 310		MAX	MIN	T 1	72	CH
10V EXT PHR CARRIAGE X CARRIAGE T			10.05 1.18 0.63	9.96 -1.29 -1.00 -0.27	215.00 3853.00 3855.00 3847.00	2460.00 3829.00 3895.00 3618.00	48 36 31
CARRIAGE Z (SM) CARRIAGE Z (SM) CARRIAGE VEL SEAT Y SEAT Y			10.39 -1.02 2.80 0.93	-0.12 -25.64 -1.37 -0.92 -0.21 -0.09	3861.00 4100.00 3816.00 3815.00 3854.00	3616.00 3621.00 3829.00 3900.00 3681.00	29 92 93 34
SERT Z (SH) SERT Z (SH) CHEST Y - CHEST Z			10.46 3.76 0.17 16.77 19.07	-0.09 -3.79 -1.52 -0.97 0.73	3854.00 3869.00 3840.00 3872.00	3663.00 3906.00 3928.00 3623.00 3840.00	5 6 7
CHEST RES CHEST SI HEAD X HEAD T HEAD Z HEAD RES			39.65 2,77 1.24 12.69 13.11 18.88	-3.93 -0.43 -1.42 0.68	3813.00 3866.00 3727.00 3869.00 3869.00	3958.00 3906.00 3878.00 4145.00 3819.00	2 3 4
HEAD SI HEAD HIC SHD REFL LF			14.75 51.17 49.44	5.48 5.05	3848.00 3898.00 3904.00	3895.00 4092.00 3653.00	14 16
SHO REEL LF LF SHOULDER SHO REFL RT SHO REEL RT RT SHOULDER TOTAL SHLD REFL			95.66 34.07 55.76 81.70	21.01 10.33 2.25 24.45 19.50 8.93	3901.00 3895.00 3909.00 3909.00 3697.00 3908.00	4093.00 3962.00 3997.00 3944.00 3963.00 3852.00	15 17
TOTAL SHID REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER			100.75 170.31 1.08 43.47 41.50 80.26	50.71 0.32 11.16 10.41 22.80	3907.00 3907.00 3971.00 3906.00 3965.00	4083.00 4083.00 3856.00 3850.00 3850.00	8 9
TOTAL LAP TOTAL LAP / HT CROTCH STRAP LF SEAT LNK X AT SEAT LNK X			0.51 48.60 34.95 29.27	0.15 -36.92 -178.02 -153.20	3968.00 3917.00 4097.00 3818.00 3751.00	3850,00 3865.00 3868.00 3869.00 3869.00	10 18 19
TOTAL SEAT X SEAT LANK Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z			30.14 54.05 451.77 559.94 759.67 1769.95 11.22	-330.65 -50.06 19.08 21.08 34.85 87.79 0.56	3731.00 3871.00 3872.00 3869.00 3872.00 3872.00	3872.00 3625.00 3614.00 3628.00 3614.00 3614.00	95 11 12 13
RES SERT FORCE / WILL FOOT X	ſ		11.40 7.25 10.93	-106.87 -104.51	3872.00 3616.00 3817.00	3614.00 3666.00 3876.00	20 23 26
RT FOOT X CT FOOT X TOTAL FOOT X			39.96 55.43 115.19 24.30	-131.77 -334.84 -24.56	3817.00 3817.00 3849.00 3667.00	3876.00 3923.00	21
LF FOOT Y AT FOOT Y CT FOOT Y TOTAL FOOT Y			62.35	-141.65 -25.99 -61.64	3838.00 3837.00 3850.00	3935.00	27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE			171.66 194.08 147.68 464.64 504.75	-30.93 -33.79 -72.45 -100.99 18.32	3867.00 3861.00 3850.00 3850.00	3936.00 3607.00 3807.00	22 25 28

10V EXT PHR 10.06 9.97 536.00 3980.00 CARRIAGE X 1.85 -1.76 3816.00 3002.00 CARRIAGE Y 0.46 -1.17 3839.00 3803.00 CARRIAGE Z 12.46 -0.32 5821.00 3722.00 CARRIAGE Z 12.46 -0.35 5821.00 CARRIAGE Z	29 33 31 29 33 34
CARRIAGE X 1.85 -1.76 3816.00 3002.00 CARRIAGE T 0.46 -1.17 3839.00 3603.00 CARRIAGE Z 12.46 -0.32 5821.00 3722.00 CARRIAGE Z (SM) 10.56 -0.15 3823.00 3721.00	36 31 29 32 33
SERT X 2.27 -1.68 3793.00 3802.00 SERT Y 0.58 -0.73 3869.00 3824.00 SERT Z 11.26 -0.24 3828.00 3606.00 SEAT Z (SM) 10.36 -0.17 3829.00 3643.00 CHEST X 5.16 -2.17 3845.00 3870.00 CHEST X 0.23 -1.75 3879.00 3863.00	5 6 7
HERD X 2.09 -3.43 3849.00 3852.00 HERD Y 1.73 -1.31 3891.00 3855.00 HERD Z 14.37 -1.20 3841.00 3981.00 HERD SI 44.49 0.54 3841.00 3794.00 HERD SI 22.92 3797.00 3936.00 HERD SI 7.94 3820.00 3862.00	34
FOR SHOREEL RT 42.37 -3.30 3063.00 3977.00 RF SHOREEL RT 42.37 -3.30 3063.00 3977.00 RT SHOREEL RT 42.37 -3.30 3063.00 3976.00 RT SHOREEL RT 75.98 18.09 3662.00 3976.00 TO SHOREEL RT 75.98 18.00 TO SHOREEL RT 75.00 TO SHOREEL RT 7	14 16 15 17
LF LAP BELT 37.62 12.40 3879.00 3821.00 AT LAP BELT 52.43 14.27 3691.00 3831.00 TOTAL LAP 69.12 27.22 3879.00 3830.00 TOTAL LAP / NT 0.49 0.19 3879.00 3830.00 CROTCH STRAP 118.65 -26.46 4055.00 3844.00 LE SERTINE Y 50.24 148.92 4055.00 3835.00	89 10 18
TOTAL SERT X SEAT LNK Y ST. 26 -33.53 3894.00 3834.00 LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL S TOTAL SEAT Z TOTAL S 35 11 12 13	
TOTPL FOOT X 83.60 -353.10 3792.00 3840.00 LF FOOT Y 133.33 -19.53 3833.00 3781.00 FT FOOT Y 17.22 -139.86 3653.00 3841.00 CT FOOT Y 36.76 -42.45 3612.00 3838.00	20 23 26 21 27 22 25 28

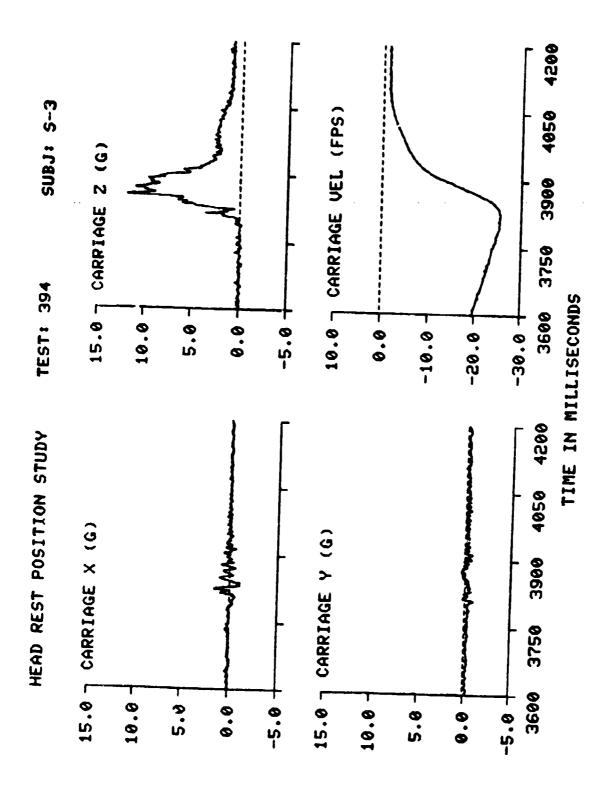
HEAD REST POS STUD	TEST:	405	SUBJ:	M13	MT: 170.0	G: 10	GP: 1 CELL:	C
DATA ID				MAX	MIN	T1	12	CH
PWX Y Z Z Y Y E E E E E E E E E E E E E E E	_			023342098667566574312651131990962888806199529232808165684440756024415602041656019866520988665209886852098868520988685209886852098868520988685209886852098868520988685209886852098868520988685536886552897887	91132619911866 8704 458881615928138448660894251526902271160 911219503201866 3208 0776665253078039628114846447604448361887 91100511002420 5010 7418616450235060543413406076245475938387 911002420 5010 12284450235060543411377 74166245475938387 911002420 5010 7418616450235060543411377 74166245475938387	00000000000000000000000000000000000000	3932.00 3621.00 3634.00 3602.00 3602.00 3621.00 3621.00 3621.00 3621.00 3928.00 3928.00 3928.00 3912.00 3912.00 3928.00	98911 9294 567 294 46 57 89 089 5120 036 147 258 222 222

HERD REST POS STUDY	1EST: 392	SUBJ: 3-2	WT: 146.0	G: 10	GP: 1 CELL:	C
DATA 10		MAX	MIN	† 1 	15	CH
10V EXT PHR CRBRIAGE X CRRAIAGE Z CARRIAGE Z CARRIAGE Z (SM)		10.04 1.38 0.79 12.73 10.71	9.96 -1.10 -0.72 -0.17 -0.10	1457.00 3628.00 3626.00 3621.00 3621.00	1428.00 3820.00 3771.00 3606.00 3629.00	48 36 31
CARRIAGE YEL SEAT X SEAT T SEAT Z		10.71 -0.95 1.13 0.59	-25.67 -1.60 -0.74 -0.24	4126.00 3782.00 3782.00 3828.00	3629.00 3786.00 3820.00 3845.00 3559.00	29 32 33 34
SEAT Z (SM) CHEST X CHEST Y CHEST Z CHEST RES		10.77 5.69 1-06 16.25 18.75 32.99	-0.11 -0.79 -2.38 -1.26 0.28	3829.00 3840.00 3834.00 3856.00 3857.00	3646.00 3882.00 3856.00 3690.00 3690.00	5 8 7
CHEST SI HEAD Y HEAD Y HEAD Z HEAD RES HEAD SI		32 1.14 14.21 14.41 20.90	-4.49 -1.16 -0.76 0.37	3785.00 3637.00 3909.00 3839.00 3839.00 3793.00	3881.00 3881.00 3603.00 4182.00 4052.00	3
HEAD HIC SHD REFL LF SHD REFL LF LF SHOULDER SHD REFL BT		14.43 33.01 27.90 51.99 32.39	11.48 5.96 26.29 15.15	3818.00 3869.00 3929.00 3869.00 3860.00	3861.00 4094.00 3828.00 4100.00 4062.00	14
SHD REEL RT RT SHOULDER TOTAL SHLO REEL TOTAL SHOULDER TOTAL SHOULDER		40.12 69.06 65.21 62.10 120.70	1.59 25.32 28.19 7.66 53.70	3875.00 3873.00 3849.00 3876.00 3869.00	3829.00 3825.00 4080.00 3828.00 3823.00	15
TOTAL SHO / NT LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / NT		0.83 94.00 59.74 73.47 0.50	0.37 0.00 4.75 7.57 0.05	3869.00 3933.00 3934.00 3933.00 3933.00	3823.00 3834.00 3829.00 3832.00 3832.00	8
CROTCH STRRP LF SERT LNK X RT SERT LNK X TOTAL SERT X		28.20 54.82 52.35 77.04	-34.16 -119.01 -53.42 -171.85	3915.00 3936.00 3792.00 3694.00	3846.00 3838.00 3837.00 3837.00	10 16 19
SERT LNK Y LF SERT PAN Z RT SERT PAN Z CT SERT PAN Z TOTAL SERT Z TOTAL SERT Z / HT RES SERT FORCE		71.21 274.53 940.17 979.76 1578.04 1567.72	-8.09 11.26 6.00 76.80 106.76 0.73	3088.00 3637.00 3847.00 3839.00 3839.00 3839.00	3795.00 3602.00 3651.00 3653.00 3602.00 3602.00	35 11 12 13
RES SERT FORCE / NT LF FOOT X RT FOOT X CT FOOT X		10.87 -5.17 -5.2 1.31 1.18	115.40 0.79 -175.15 -124.42 -195.47 -495.03	3839.00 3675.00 3787.00 4200.00 3787.00	3649.00 3639.00 3838.00 3839.00 3839.00	20 23 26
TOTAL FOOT X LF FOOT Y AT FOOT Y CT FOOT Y TOTAL FOOT Y		147.70 22.75 16.66 59.64	-16.51 -129.00 -53.65 -62.77	3833.00 3891.00 3789.00 3814.00	4026.00 3822.00 3842.00 3842.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		186.53 196.30 130.90 430.27 585.77	-6.72 -7.42 -91.00 -67.71 22.88	3849.00 3850.00 3849.00 3841.00	3916.00 3798.00 3778.00 3778.00 3925.00	22 25 28

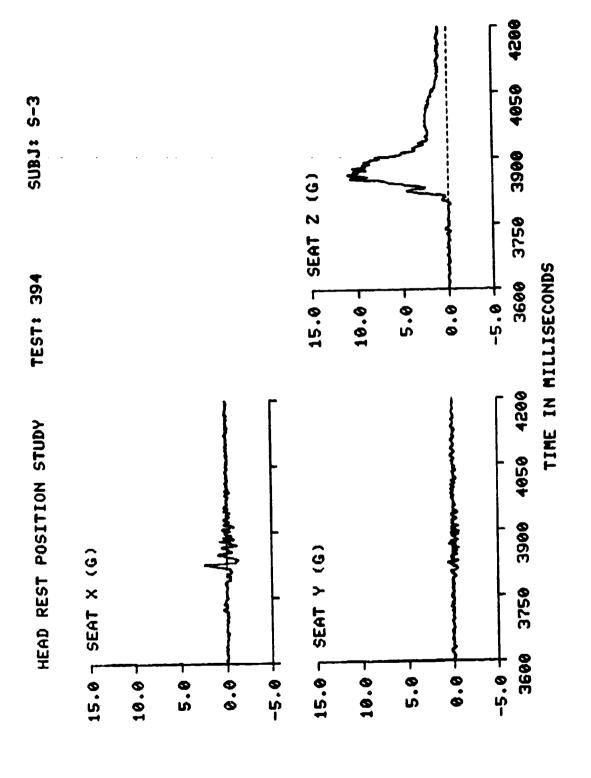
HERD REST POS STUDY	TEST: 370	SUBJ: A	1-1	h1: 194.0	G: 10 G	P: 2 CELL:	С
DATA ID			MAX	MIN	T1	 15	CH
IOY EXT PHR CRRRINGE X CRRRINGE Y CRRRINGE Z CRRRINGE Z CRRRINGE VEL SERT X SERT X SERT Z SERT Z SERT Z SERT Z CHEST Y CHEST Y CHEST Y CHEST X CHEST SI HERO X	- · · ·	1	10.08 1.56 10.66 10.98 10.98 11.69 11.69 11.69 11.69 11.69 11.69 11.69 11.69 11.69	9.97 -1.102 -0.34 -0.105 -25.75 -1.60 -0.19 -0.19 -1.005 -1.005 -3.84	11.00 3830.00 3830.00 3825.00 3825.00 3825.00 3825.00 3825.00 3825.00 3825.00 3835.00 3835.00 3861.00 3861.00 3861.00	2813.00 38245.00 3935.00 3638.00 3639.00 3699.00 3784.00 3784.00 39643.00 39643.00 39643.00	#851 9254 567 N34
HEAD Y HEAD Z HEAD AES HEAD SI HEAD SI HEAD SI HEAD SI HEAD HIC SHD REFL LF SHO REEL TOTAL SHLD REFL TOTAL SHLD REFL TOTAL SHLD AT TOTAL SHLD AT TOTAL SHLD AT TOTAL SHLD AEFL TOTAL SHLD AFFL TOTAL LAP AFFL TOTAL SHLD AFFL TOTAL SHLD TOTAL SHL		1 1 2	12.509 12.5299 12.5	-0.795 14.195 14.195 14.195 15.5587 16.858 15.688 16.858 16.858 16.858 16.858	\$651.00 3848.00 \$7821.00 \$7821.00 \$7821.00 \$7821.00 \$7821.00 \$7912.00	5654	14 18 15 17 8 9
AT SEAT LNK X TOTAL SEAT X SERT LNK Y LF SEAT PAN Z AT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z ASS SEAT FORCE / HT ASS SEAT FORCE / HT ASS SEAT FORCE / HT ASS SEAT FOOT X AT FOOT X CT FOOT X TOTAL FOOT Y LF FOOT T CT FOOT Z AT FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z	,	18	111.3956620270991611591770991867899988789161159177099188789998878911128878999889789988978988	-293.352 -293.352 -293.352 -293.352 -293.352 -293.352 -293.352 -293.352 -293.352 -193.523 -19	\015.000 \015.000 \015.000 \015.000 \00000 \0000 \0000 \0000 \00000 \00000 \0000 \0000 \0000 \0000 \0000 \0000 \00000 \0000 \0	3845.00 38056.00 3856.00 3800.00 3800.00 3800.00 3842.00 3842.00 3842.00 3842.00 3842.00 3843.00 3848.00 3848.00 3848.00 3848.00	35 1123 203 203 203 203 203 203 203 203 203 2

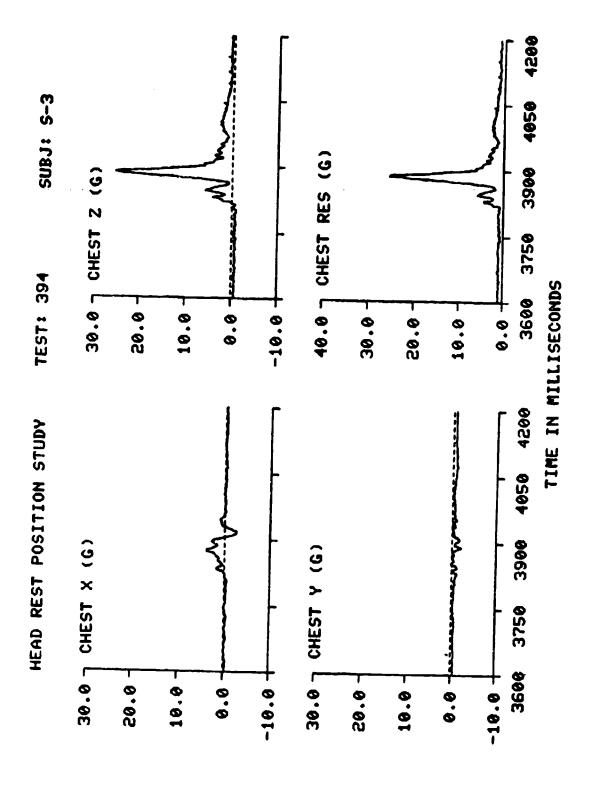
DATA 1D MAX MIN T1 T2 10V EXT PHR CARRIAGE X CRRNIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE V CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE VEL T1.15 T2 T2 10.05 9.96 1308.00 2156.00 3870.00 2156.00 2156.00 3870	HEAD REST POS STUDY	TEST: 400	SUBJ: R-3	NT: 146.	0 6- 10	CD 0 00	_
10V EXT PHR CRRRIAGE X CRRRIAGE T CRRRIAGE T CRRRIAGE Z CRRRIAGE Z CRRRIAGE Z CRRRIAGE Z CRRRIAGE Z CRRRIAGE Z CRRRIAGE Z CRRRIAGE VEL 10.01 -0.26 3893.00 3655.00 CRRRIAGE VEL 10.41 -0.11 3908.00 3655.00 CRRRIAGE VEL 11.5 -25.55 4119.00 3859.00 SERT X SERT Z SERT Z SERT Z SERT Z SERT Z SERT Z SERT Z SERT Z SERT X SERT Z SERT X SERT Z SERT X SERT Z SERT X SERT Z S SERT Z S SERT Z S S S S S S S S S S S S S S S S S S S	DATA 10			MIN	• • • •		ı C Ch
THERD X HEAD Y HEAD RES HEAD SI HEA	CRARAIRAGE Y SHANIAGE Y CRARAIRAGE Y SHANIAGE Y CRARAIRAGE Y SHANIAGE Y		525-1-15004526204062329473230270404466130969285768264562 0.1.0.1.13893373332602339008855932800599971071647788664562 1105-1617701-1398248740441668599971071647788664562 11112 112 1138248740441688599971071647788664562 1112 112 11382487404416885999710716477856647755577184745864562	91721568168413 9713 5096531447542058781444610311351780307	00000000000000000000000000000000000000	00000000000000000000000000000000000000	C. 4331 2333 567 234 46 57 89 089 5123 036 147 258

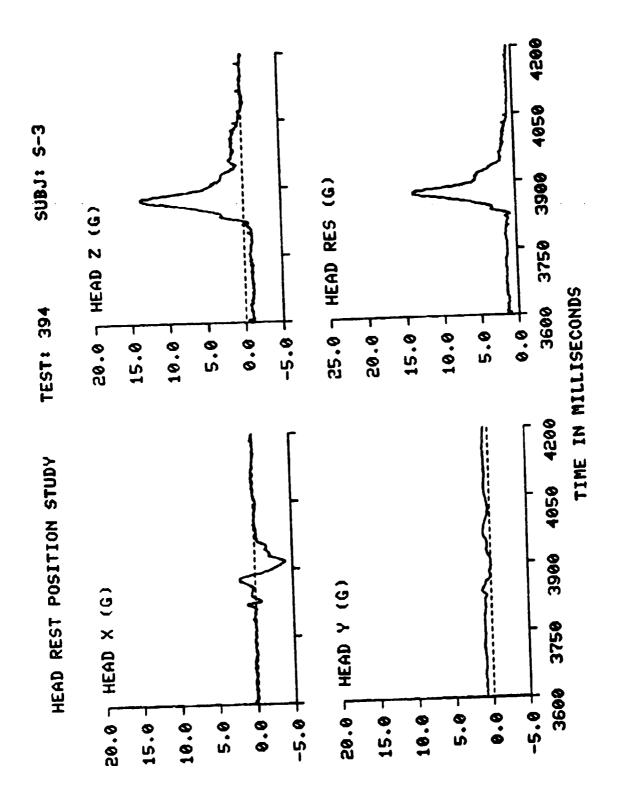
				165 D	c. in GP	, 2 CELLI	С
HERD REST POS STUDY	TEST: 394	2087:	5-3	MIN MIN	T1	15	CH
DATA ID			MAX			3431.00	48
10V EXT PHR			10.05	9.97	1439.00 3825.00 3877.00	3838.00	96 91
CARRIAGE Y			0.97 11.84	-0.95 -0.31 -0.18	3856.00 3857.00	3702.00 3700.00	59 J
CARRIAGE Z (SM)			10.37	-25.55 -1.32	4149.00 3825.00	3820.00 3837.00	32 33
CARRIAGE VEL			2.46 0.68 11.09	-0.65 -0.31	3824.00 3863.00	3896.00 3795.00 3664.00	34
SEAT Z SEAT Z SEAT Z (SM)			10.39	-5.65	3864.00 3875.00	3917.00 3890.00	5 6 7
CHEST X CHEST Y			25,39	- 2.16 - 2.98	3855.00 3887.00 3887.00	3658.00 3743.00	7
CHEST Z CHEST RES			25.49 43.06	0.51 _u_0?	3821.00 3877.00	3966.00 3917.00	3
CHEST 51 HEAD X HEAD Y			2,17 1,25 13.69	-4.02 -0.10 -1.24	3836.00 3877.00	3893.00 3609.00 4200.00	ŭ
HEAD Y HEAD Z Head bes			13.87	0.57	3877.00 3831.00	3952.00 3898.00	
HEAD SI HEAD HIC			80.03	13.44	3853.00 3903.00 3909.00	4082.00 3870.00	14 16
SHB REFL LF			47.88 104.16 47.02	8.53 31.97 18.38	3906.00 3903.00	4098.00 3960.00	15 17
LF SHOULDER SHO REFL AT			47.02 69.48 109.68	1.60	3913.00 3912.00	3870.00 3989.00 4098.00	.,
SHO REEL RT RT SHOULDER TOTAL SHLD REFL			107.03		3912.00	3870.00 3990.00	
TOTAL SHLD KEEL			209.19	U.44	3911.00 3911.00 3911.00	3990.00 3876.00	8
TOTAL SHU / MI			41.81 50.61	16.60 30.98 49.12	3920.00	3860.00 3859.00	9
BT LAP BEL!			101.50	0.30 -66.22	3920.00 3959.00	3659.00 3671.00	10
TOTAL LAP / HT CROTCH STRAP LF SEAT LNK X			77.82 48.72	-165.40	3961.00	3871.00 3872.00 3871.00	iš
RT SERT LNK X TOTAL SERT X			25.69 27.90 82.30	-,0	4085.00 3942.00 3872.00	3876.00 3789.00	35 11
SERT LNK T			406.35 488.73	31.74 u1.84	3887.00	3643.00 3800.00	13
RT SEAT PAN Z			837.50 1689.28	22.33	3873.00 3873.00	3612.00 3612.00	
TOTAL SERT Z TOTAL SERT Z / HT RES SERT FORCE			1716.94 10.4		3873.00 3873.00	3012.30	20
RES SEAT FORCE /	нT		15.6	7 -95.73 7 -46.01	3619.00	3884.00	23 26
AT FOOL X			55.0 68.4	3 -282.10	3827.00	3874.00 3834.00	21
LE FOOT Y			79.3 27.0	8 -62.3	3 3907.00 3827.00	3889.00	24 27
AT FOOT T CT FOOT Y			30.4 58.7	2 -92.2	3847.00 3849.00	3877.00	22 25
TOTAL FOOT Y LF FOOT Z RT FOOT Z			151.5 109.5 390.1	9 -135.2	2 3824.0	0 3037.00	28
CT FOOT Z			446.7 482.0	n -135.2	1 3849.0 1 3875.0		
RES FOOT FORCE							

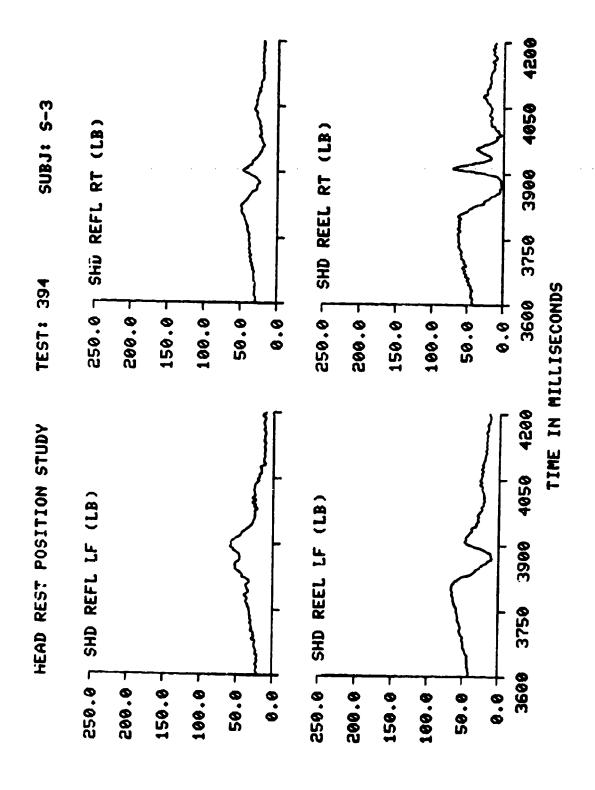


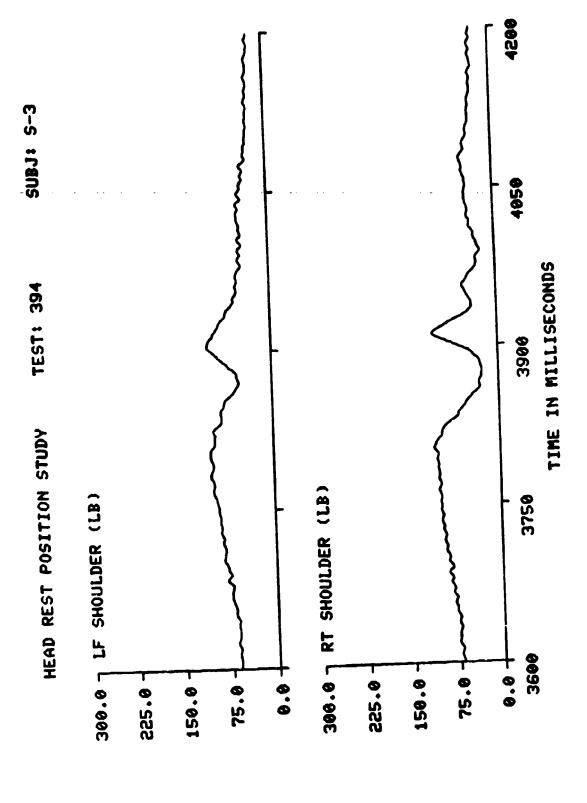
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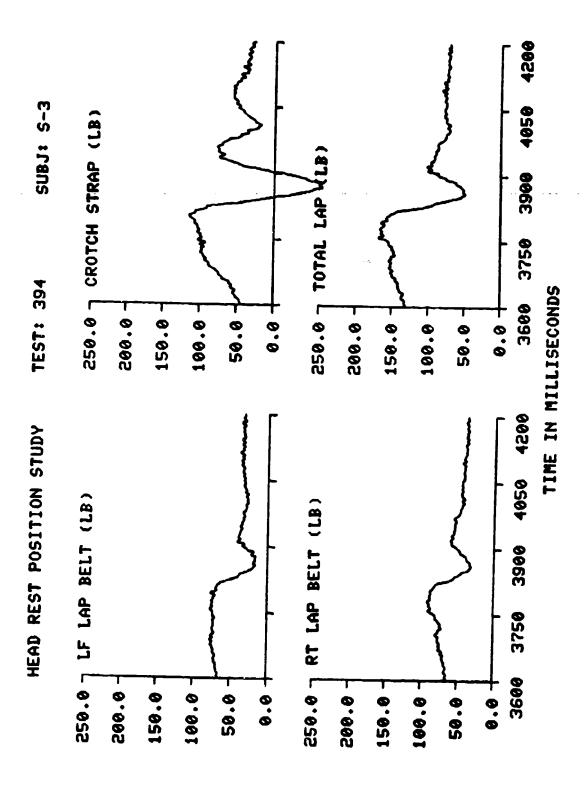


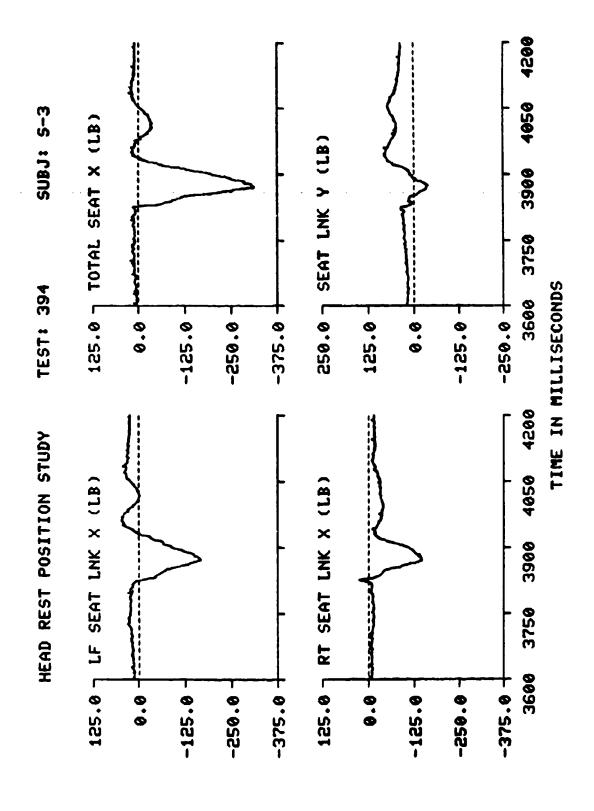






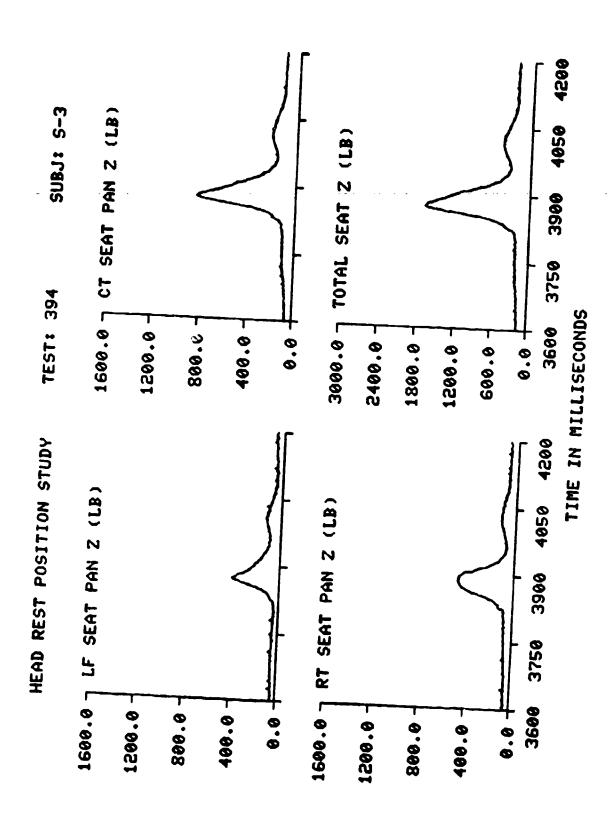




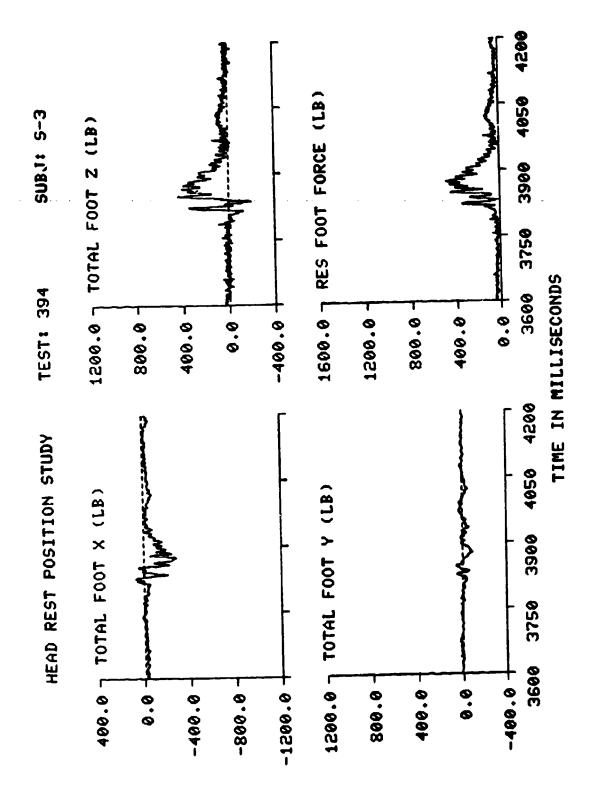


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HEAD REST POS STUDY	TEST: 373	SUBJ: D-1	NT: 209.	0 6. 10	55 4 65.	
DATA ID		MAX	MIN	T1	GP: 1 CELL:	D CH
IORANGE Y CSH) CRARRIAGE Y CSH) CCARRIAGE Y CS		10.48551991519945343395559883370872013774581008661230884484555598833708720137745843845555988337088720137745843845555988337088712217744849.30991922612307698833983708838455598833708838838370883837088388383708838838370883883837088388383708838838370883883837088388383708838838370883883837088388383708838838370883883838383	91.0838424111107202 9462 21516988483167202 9462 21516988483167763855385072358908670.469684316121791078855385072358908670.4696843161217910788563647747200 1945523358908670.46968431612179102358358908670.46968431612179102358910786869697863647747255	- 0.00000000000000000000000000000000000		1 86 1 923 4 567 234 46 57 89 089 5129 036 147 258 222 222 222

HEAD REST POS STUDY	TEST: 365	SUBJ: E-1	MT: 189.0	G1 -10	GP: 2 CELL:	D
DATA 10		MAX	H1N	<u>T1</u>	12	CH
	TEST; 365	MAX - 0.7769528899784407784000000000000000000000000000	HIN	Tì	2- 000000000000000000000000000000000000	
TOTAL SEAT X SEAT LAK Y LF SEAT PAN Z BT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z / HT RES SEAT FORCE / HT		22.77 46.68 436.80 538.13 1031.07 1967.38 1041 1986.07	-311.30 -54.40 36.94 67.41 169.46 172.12	4111.00 3962.00 3891.00 3893.00 3900.00 3900.00 3900.00	3889.00 3620.00 3616.00 3760.00 3613.00 3613.00 3600.00	35 11 12 13
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y RT FOOT Y TOTAL FOOT Y LF FOOT Z RT FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z RT FOOT Z RES FOOT FORCE		-13.07 -3.60 -17.81 159.27 21.182 45.33 213.36 209.43 578.46 750.19	-159.54 -149.87 -29.85 -501.85 -37.26 -169.68 -40.51 -32.12 -100.25 -75.99	9844.00 9844.00 9844.00 9886.00 9886.00 9886.00 9899.00 9899.00 9899.00	3904.000 38994.000 38994.000 38975.000 38976.000 38976.000 38976.000 38976.000	2036 227 227 228 228

HEAD REST POS STUDY	TEST: 377	SUBJ: F-3	HT: 167.0) G: 10	SP: 1 CELL:	D
DATA 10		HAX	HIN	T1	12	СН
10V EXT PWA CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z (SM)		10.05 1.77 0.85 12.71 10.80	9.97 -1.23 -0.96 -0.22 -0.08	494.00 3920.00 3919.00 3913.00	496.00 3913.00 4022.00 3726.00	48 36 31
CARRIAGE VEL SEAT X SEAT Y SEAT Z SEAT Z (SM) CHEST X		-1 00	-25.77 -1.68 -1.03 -0.22 -0.09	4197.00 3879.00 3877.00 3920.00	3619.00 3877.00 3912.00 3609.00 3747.00	29 32 33 94
HEAD X			-2.31 -2.03 -1.00 1.21	3934.00 4002.00 3946.00 3946.00 3883.00	3961.00 3948.00 3731.00 3599.00 4002.00	5 6 7
MEAD Y HEAD Z HEAD RES HEAD SI HEAD HIC		9.65 1.97 12.25 12.78 117.14	-0.27 -0.19 -1.39 0.95	3937.00 4002.00 3937.00 3937.00 3893.00 3910.00	4196.00 3541.00 3774.00 4196.00 3995.00 3974.00	3
SHD REFL LF SHD REEL LF LF SHOULDER SHD REFL RT		67.88 50.39 118.27 78.03	22.14 9.53 46.65 33.42	3957.00 3957.00 3957.00 3955.00	4047.00 3931.00 4030.00	14
SHD REEL RT RT SHOULDER TOTAL SHLD REEL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER TOTAL SHOULDER LEFT SHOULDER		72.17 150.20 145.78 122.11 267.89 1.60	19.31 77.73 61.19 29.60 130.16 0.78	3955.00 3955.00 3956.00 3956.00 3956.00	3987.00 3926.00 3925.00 3997.00 3927.00 4046.00	15 17
MI LAP BELT TOTAL LAP TOTAL LAP / HT CAOTCH STRAP		64.77 72.37 135.46 0.81	21.71 26.79 49.30 C.30	4055.00 4055.00 4050.00	3922.00 3920.00 3921.00 3921.00	8 9
LF SEAT LNK X NI SEAT LNK X TOTAL SEAT X SEAT LNK Y		95.59 48.97 32.24 63.90 61.33	-84.29 -169.18 -71.06 -238.38	4021.00 4007.00 3635.00 3722.00	3930.00 3929.00 3926.00 3929.00	10 18 19
LF SERT PAN Z RT SERT PAN Z CT SERT PAN Z TOTAL SERT Z TOTAL SERT Z / HT RES SERT FORCE RES SERT FORCE / HT		446.40 365.85 725.81 1515.37 9.07 1534.18	118.36	3991.00 3935.00 3939.00 3930.00 3935.00 3935.00	3935.00 3604.00 3606.00 3706.00 3604.00 3604.00	35 11 12 13
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		9.19 -40.13 -4.92 -80.89 -147.17 162.99	-232.94 -555.48	3935.00 3881.00 3880.00 4190.00 3881.00	3604.00 3929.00 3914.00 3931.00	20 23 26
RT FOOT Y CT FOOT Y TOTAL FOOT Y LF FOOT Z		22.36 25.27 63.07 231.42	-184.41 -46.81	3914.00 3823.00 4022.00 3962.00	4000.00 3914.00 3926.00 3931.00	21 24 27
RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		230.84 132.61 506.57 713.87	43.29 -114.72	3915.00 3941.00 3920.00 3923.00 3815.00	4000.00 3910.00 3872.00 3872.00	22 25 28

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HEAD REST POS STUDY	1EST: 368	SUB 1: 0-3	MT: 161.0	G: 10	GP: 2 CELL	. 0
DATA ID		HAX	MIN	T1	12	CH
IOV EXT PHR CRRMINGE X CHRMINGE T CRRMINGE Z CARMINGE Z		10.05 1.15 0.84 12.26 10.47	9.96 -1.09 -0.59 -0.31 -0.13	1572.00 3910.00 3926.00 3917.00 3917.00	2454.00 3893.00 3897.00 3685.00	48 36 91
CARRIAGE VEL SERT X SERT Y SERT Z SERT Z (SM)		-0.90 1.84 0.66 11.39	-25.70 -1.06 -0.97 -0.23 -0.17	4176.00 3883.00 3882.00 3923.00 3924.00	3868.00 3930.00 9903.00 3608.00	29 32 33 34
CHEST X CHEST Z CHEST RES CHEST SI		1.49 0.41 17.63 18.01 29.44	-3.44 -3.24 -1.	3891.00 3926.00 3957.00 3957.00 3883.00	3971.00 3957.00 3731.00 4173.00 4027.00	5 6 7
HERD X HERD Y HERD Z HERD RES MEAD SIC		2.59 1.99 11.85 11.91 20.05 17.62	-3.24 -0.55 -1.71 0.82	4015.00 4034.00 3940.00 3940.00 3891.00	3974.00 3957.00 4025.00 4199.00 3999.00	3
SHO REFL LF SHO REEL LF LF SHOULDER		79.85 59.34 135.80	15.34 7.54 31.86	3913.00 3969.00 3963.00 3963.00	3981.00 4031.00 3919.00 4021.00	14
SHD REEL AT SHD REEL AT AT SHOULDER TOTAL SHLD REFL TOTAL SHLD REEL TOTAL SHOULDER TOTAL SHOULDER		62.19 65.54 127.20 140.36 123.58 261.91 1.63	21.80 3.50 34.29 59.26 11.64 74.79	3966.00 3966.00 3966.00 3967.00 3963.00 3964.00	4076.00 3924.00 3920.00 4046.00 3936.00 3919.00	15 17
LF LAP BELT BT LAP BELT TOTAL LAP TOTAL LAP / HT CROTCH STRAP		38.31 59.45 97.58 0.61 175.59	6.68 13.84 21.70 0.13	4039.00 4036.00 4039.00 4039.00	3917.00 3923.00 3924.00 3924.00	8 9
LF SEAT LAK X AT BEAT LAK X TOTAL SEAT X SEAT LAK Y		35.24 20.29 42.48 43.78	-20.49 -134.56 -100.95 -229.75 -56.70	4029.00 4193.00 3883.00 3734.00 4007.00	3941.00 3932.00 3939.00	10 18 19
LF SEAT PAN Z RT SEAT PAN Z ST SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z HT RES SEAT FORCE RES SEAT FORCE / HT		602.52 640.25 464.19 1696.38 10.54 1711.49 10.63	48.27 30.73 24.11 116.38 0.74 123.15 0.76	73941 00.00 1496 00.1496 00.1496 00.1496 3941.00	3945.00 3616.00 3622.00 3610.00 3610.00 3610.00	35 11 12 13
LF F001 # RT F001 # RT F001 X T01RL F001 X LF F001 T RT F001 T		3.44 18.22 26.05 41.46 137.33 28.24	-109.58 -96.33 -127.78 -322.22 -21.64 -134.16	3885.00 3886.00 3884.00 3886.00 3928.00	3929.00 3935.00 3931.00 3929.00 4000.00	20 23 26 21
CT FÖÖT Y TIPL FOOT Y LF FOOT Z BT FOOT Z CT FOOT Z		17.39 41.96 142.23 185.42	-40.46 -82.37 -38.82 -8.27	3971.00 3956.00 3971.00 3920.00 3948.00	3937.0u 3936.00 3938.00 3697.00 3870.00	24 27 22 25
TOTAL FOOT Z RES FOOT FORCE		154.61 436.65 528.17	-81.38 -98.63 53.90	3923.00 3928.00 3928.00	3897.00 3877.00 4031.00	26

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HEAD REST POS STUDY TEST: 374 SUBJ: G-2 NT: 121.0 G: 10 GP: 2 CELL: D
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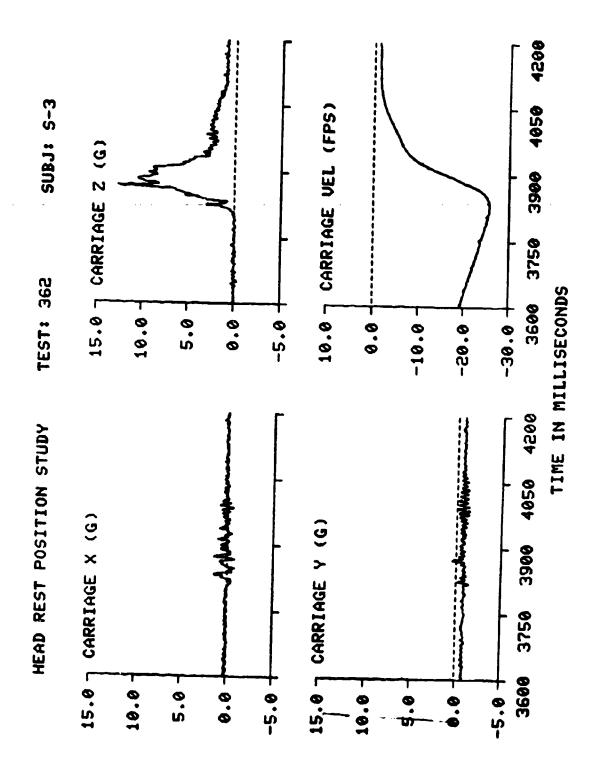
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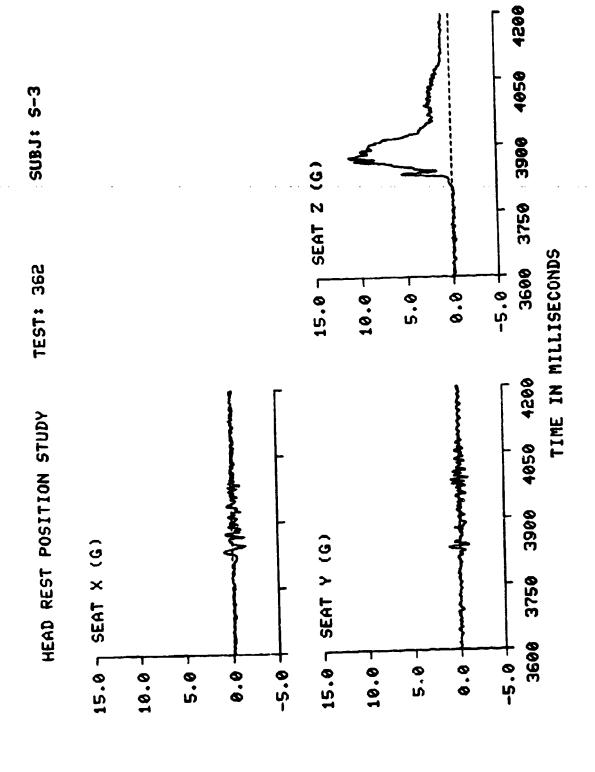
MERO REST POS STUDY TEST: 418 SUBJ: M10 MT: 140.0 G: 10 DPT 2 LELL	CH
10V EXT PHR CARRIAGE X 109 -0.16 3844.00 3890.00 CARRIAGE Y 12.66 -0.19 3836.00 3606.00 CARRIAGE Z CARRIAGE Z CARRIAGE VEL 109 -0.08 3836.00 3606.00 CARRIAGE VEL 1002 -25.45 4167.00 3811.00 SEAT X 1002 -25.45 4167.00 3811.00 SEAT X 11.64 -0.28 3843.00 3638.00 SERT Z 11.65 -0.05 3855.00 3808.00 SERT Z 11.65 -1.51 3858.00 3639.00 CHEST X 10.78 -0.12 3843.00 3639.00 CHEST X 10.78 -0.12 3843.00 3639.00 CHEST X 10.78 -0.12 3843.00 3639.00 CHEST X 10.78 -0.12 3868.00 3639.00 CHEST X 10.78 -1.51 3858.00 3866.00 CHEST X 10.16 -1.04 3868.00 3636.00 CHEST X 10.17 3868.00 3636.00 CHEST X 10.18 3868.00 3636.00 CHEST X 10.18 3868.00 3636.00 CHEST X 10.18 3868.00 3891.00 CHEST X 10.18 3868.00 3891.00 CHEST X 10.18 3868.00 3636.00 CHEST X 10.18 3868.00 CHEST X	
LF SHOULDER SHD REFL RT SHOULDER TOTAL SHOULDER TOT	#8611 9234 567 234 46 57 89 089 5123 036 147

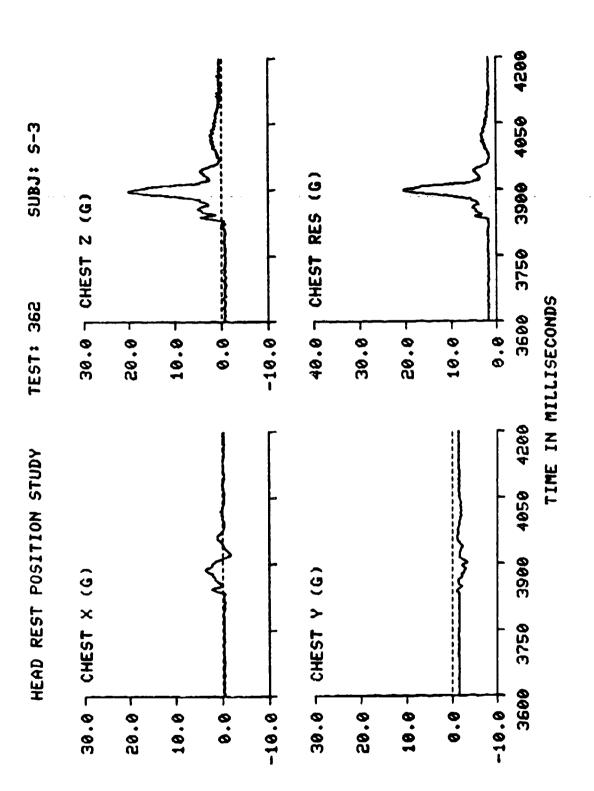
HERO REST POS STUDY	7EST: 367	SUBJ: R-2	HT: 148.0	G: 10	GP: 1 CELL:	D
DATA ID		MAX	HIN	71	15	CH
OVERTED TO THE STATE OF THE STA		091194214984990186750498000176972149326448590375897138582215348489901887504881167697214921648916688116769721489316881167698113466168176889168811893168893188931	9.1.22770077791073 2300 7861990829782199110073 2300 200465182978219935075476356418 9.1.0051.1.5088 5676 200465112978770389588653607547878787878787878787878787878787878787	00000000000000000000000000000000000000	3853.000 3866.000 386	18611 8234 587 234 48 57 89 189 5123 036 147 258

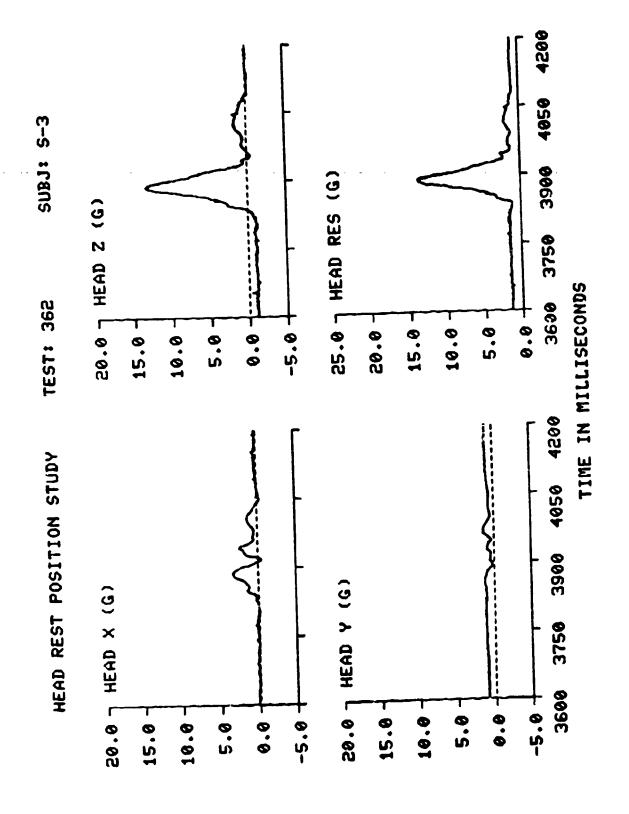
HEAD REST POS STUDY	TEST: 372	SUBJ: R-3	NT: 146.	0 G: 10	CO. 3 CD.	_
DATA 10		нах	MIN	נל	GP1 2 CELLI	CH D
10V EXT PHR				•-		~-
CARRIAGE X		10.08	9.97 -1.05	152.00 3824.00	637.00	ų e
CARRIAGE Y CARRIAGE Z		1.49 0.75 12.91	-0.95	3884.00	3838.00 3812.00	36 31
CARRIAGE Z (SM) CARRIAGE VEL		10.81	-0.21 -0.09	3857.00 3857.00	9645.00 3647.00	1
SEAT Y		-1.04 1.09	-25.72 -1.23	4132.00 9826.00	3800. nn	58
SEAT Z		0.93 00.51	~1.56 -0.24	3822.00	3836.00 3829.00	32
CHEST Y		10.71	-O. 18	3864.00 9864.00	3672.00 3672.00	34
CHEST T CHEST Z CHEST RES		5,36 0,22 20,70	-2.28 -2.77	3877.00 3873.00	3918.00 3899.00	29 32 33 34 56 7
CHEST RES		20.70 21.14	-1.06 0.99	3091.00 3891.00	3657.00 3700.00	7
CHEST SI HEAD X		37. 70		3823.00	3966.00	
HEAD T Head Z		2.87 1.75	-3.17 0.68	3883.00 3928.00	3922.00 3896.00	2 3 4
HERD RES		11.91 12.25	-1.D7 0.94	3873.00 3873.00	3683.00	ű
HEAD HIC		12.25 19.78 15.13	0.01	3829.00	9959.00 9951.00	
SHO REFL LF SHO REEL LF		52.42	15.10	3847.00 3911.00	3929.00 4100.00	14
LF SHOULDER SHO REFL RT		58.46 110.45	7.12 37.04	3914.00 3913.00	3683.00 4100.00	iš
SHN REFL RT		98.90 60.88	19.82 10.46	3910.00	3987 00	15
AT SHOULDER TOTAL SHLD REFL		97.48	33.20	3916.00 3917.00	3876.00 3977.00	17
TOTAL SHLD REEL TOTAL SHOULDER		91.14 118.15	35.89 18.69 72.59	3911.00	4099.00 3884.00	
TOTAL SHO / NT LF LAP BELT		206.60	72.59 0.50	3914.00 3914.00	3987.00	
MI LAP BELT		48. 07	10.81	3960.00	3987.00 3881.00	8
TOTAL LAP		53.62 100.21	18.12 30.78	3969.00 3960.00	3866.00 3882.00	8
CROTCH STRAP		107.67	0.21 -40.69	3960.00 3972.00	3882.00	
LF SEAT LNK X AT SEAT LNK X		45.33	-129.07	4096.00	3874.00 3871.00	10 18
TOTAL SEAT X SEAT LNK Y		10.42	-105.87 -234.37	4072.00 4096.00	3872.00 3872.00	19
LE SEAT PAN Z		50.28 407.43	-41.73 43.04	3946.00	3876.00	35
AT SEHT PRN Z CT SEHT PAN Z		946.31 735.86	46.56	3873.DD	3639.00 3600.00	11 12
TOTAL SEAT Z / HT		1550,07	84.05 165.69	3660.00 3877.00	3601.00 3600.00	12
RES SEAT FORCE		10.67 1575.59	1.13	3877.00 3877.00 3876.00	3600.00	
RES SEAT FORCE / HT LF FOOT X		10.79 1 3. 89	1.14	3876.00	3600.00 3600.00	
RT FOOT X CT FOOT X		29 90	-103.85 -82.44	5826.00 3824.00	3874,00 3874,00	53 50
TOTAL FOOT X		96.17 68.66 119.47	-108.73 -294.12	3824.00 3825.00 3825.00	3875.00 3874.00	26
LF FOOT Y		119.47 24.76	-21.16	3859.00	3956.00	21
CT FOOT Y Total Foot Y		17.46	-124.31 -39.50	4013.00 3994.00	3858.00 3869.00	24 27
LF FOOT Z		48.31 153.93	-59.96 -29.65	3845.00 3861.00	3879.00 3813.00	
CT FOOT Z		138.04 165.65	-11.83	3867.00	4053.00	22 25 28
TOTAL FOOT Z RES FOOT FORCE		395.33	-96.81 -95.93	3822.00 3867.00	3836.00 3835.00	28
		425.05	11.36	3867.00	9628.00	

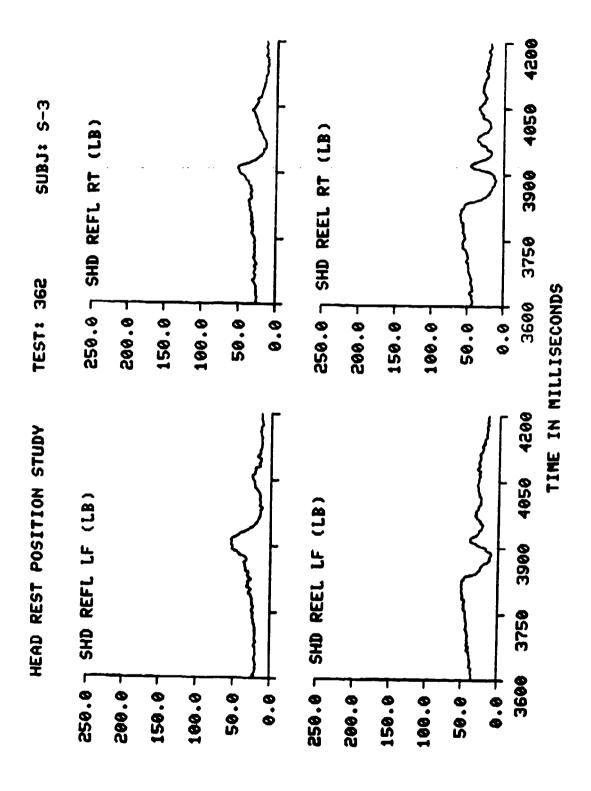
HEAD REST POS STUDY	TEST: 362	\$U8J: 5-3	NT: 166.0	G: 10	GP: 2 CELL:	D
DATA ID		HAX	HIN	T 1	12	CH
10V EXT PHR CARRIAGE X CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE VEL SEAT X SEAT X SEAT Z		10.05 1.39 0.44 12.72 10.60 -1.11 0.90 1.11	9.95 -0.83 -1.51 -0.35 -25.79 -1.43 -0.37	523.00 3873.00 9873.00 3867.00 3867.00 4195.00 3833.00 3834.00 3874.00	777.00 3847.00 3987.00 3651.00 3652.00 3819.00 3846.00 3839.00	48 36 31 29 33 34
SERT Z (SM) CHEST X CHEST T CHEST Z		10.57 3.68 -1.03 20.20 20.48	-0.25 -1.71 -3.28 -1.09 1.43	3875.00 3888.00 3837.00 3897.00 3898.00	3683.00 3923.00 3902.00 3658.00 3978.00	5 6 7
CHEST SI HERD X HERD T HERD RES HERD SI		36.05 3.29 1.40 13.34 13.74 20.90	-0.47 0.22 -1.40 0.82	3835.00 3888.00 3971.00 3889.00 3889.00	3958.00 3918.00 3896.00 3678.00 4082.00 3849.00 3921.00	2 3 4
MEAD HIC SHO REFL LF SHO RESL LF LF SHOULDER		17.29 54.44 39.49 92.91 51.99	11.64 9.63 38.00 13.66	3865.00 3914.00 3917.00 3916.00 3910.00	3986.00 3886.00 4012.00 3958.00	14 16
SHD REFL RT SHD REEL RT RT SHOULDER TOTAL SHLO REFL TOTAL SHLO REEL TOTAL SHDOULDER TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT		45.67 89.60 105.59 84.55 182.50	10.59 33.06 28.82 20.30 73.06 0.44	3921.00 3916.00 3912.00 3920.00 3916.00	3887.00 3954.00 3967.00 3887.00 3854.00 3954.00	15
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / HT CROTCH STRAP		54.92 48.07 100.13 0.60 98.17	20.02 21.06 42.02 0.25 -65.92	3970.00 3967.00 3969.00 3969.00 3978.00	3879.00 3688.00 3878.00 3878.00 3889.00	10
LF SEAT LNK X AT SEAT LNK X TOTAL SEAT X		32.58 7.47 26.24 48.54	-182.12 -136.03 -312.67 -80.99	4115.00 3857.00 3657.00 3951.00	3886.00 3881.00 3885.00 3891.00	18 19 35
SEAT LNK T LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE / WT RES SEAT FORCE / WT		586.68 468.68 739.52 1764.78 10.75 1811.34	150.89 44.58 42.91 149.64 0.83	3891.00 3891.00 3893.00 3890.00 3890.00 3890.00	3620.00 3601.00 3614.00 3602.00 3602.00 3602.00	112
LF FOOT X RT FOOT X CT FOOT X		9.84 22.06 41.75 68.34	-114.93 -73.10 -131.77 -281.03	3834.00 3835.00 3835.00 3834.00	3898.00 3868.00 3896.00 3896.00	58 53 50
TOTAL FOOT X LF FOOT Y RT FOOT Y CT FOOT Y		119.74 23.55 36.95 45.76 161.18	-16.53 -124.65 -41.37 -66.49	3869.00 3993.00 4008.00 3854.00	3961.00 3886.00 3381.00 3888.00	21 24 27
TOTAL FOOT Y LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		161.18 152.18 293.24 487.39 554.77	-43.66 -33.29 -80.22 -90.46	3894.00 3869.00 3876.00 3894.00	3007.00 3065.00 3025.00 3025.00 4155.00	22 25 28

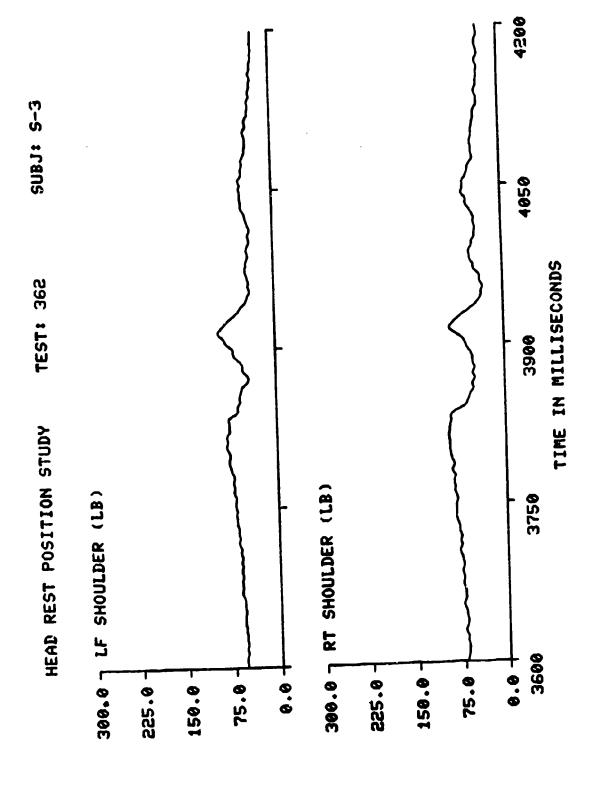




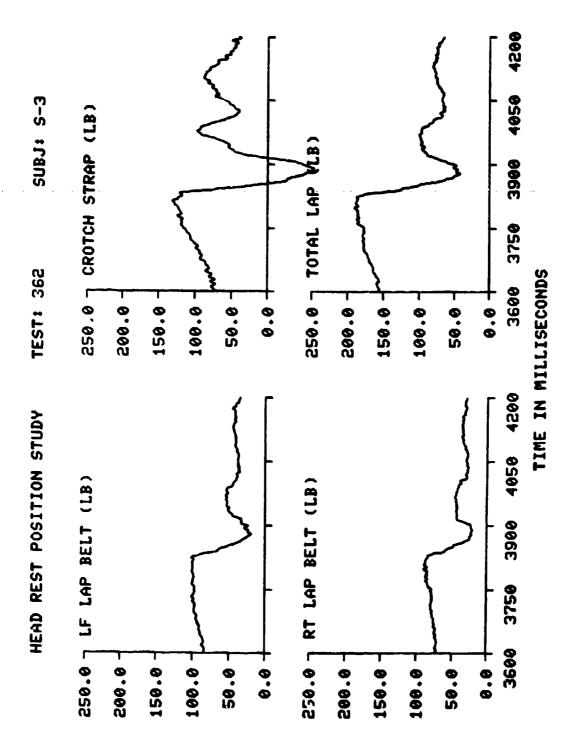




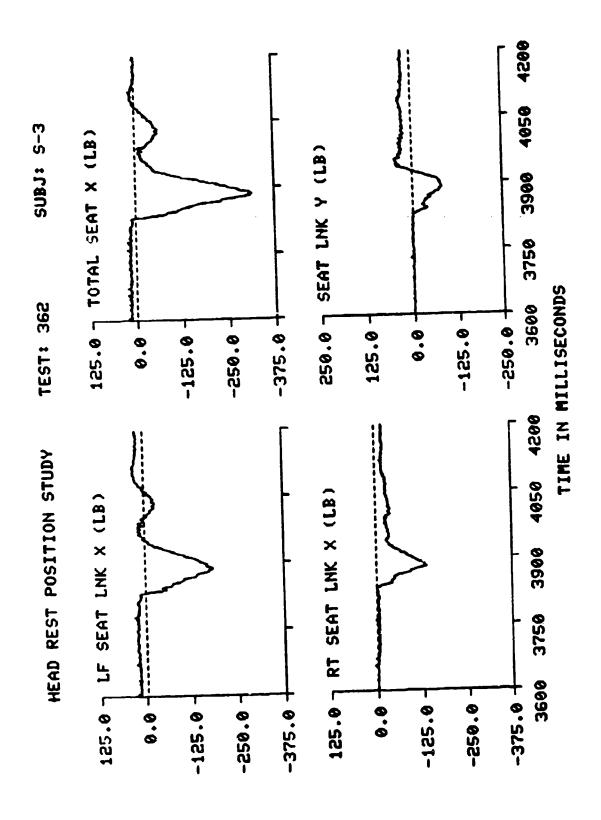


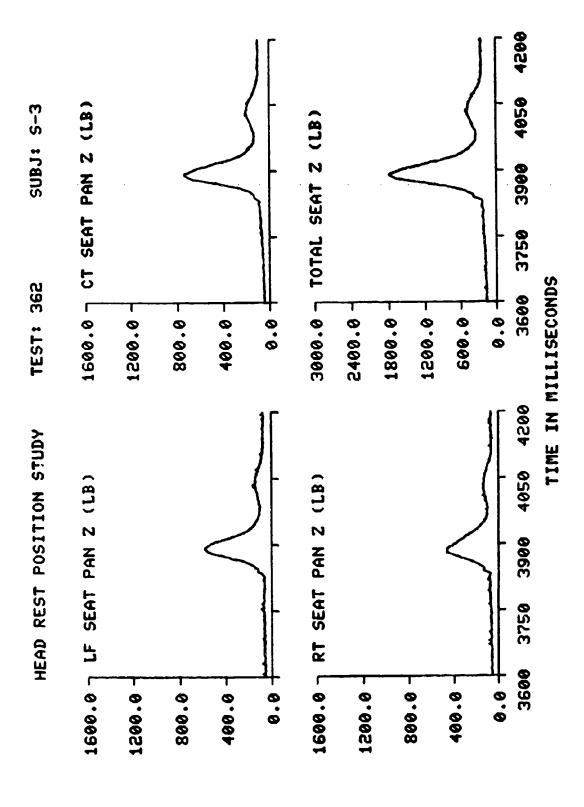


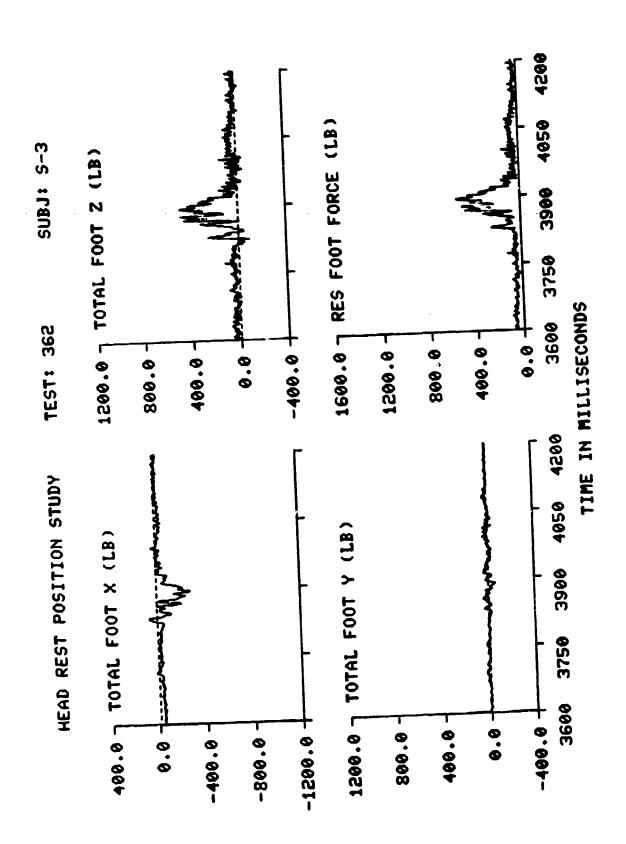
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DRIH ID
10V EXT PHR CARRIAGE X CARRIAGE X CARRIAGE T CARRIAGE Z
TOTAL SHOULDER

HERD REST POS STUDY	TEST: 412	\$09J: F-3	NT: 164.0	G: 10	GP: 1 CELL:	Ε
DATA 10		MAX	MIN	<u>T1</u>	12	CH
LOV EXT PHR CARRIAGE X CARRIAGE Y CARRIAGE Z		10.05 1.47 1.07 12.13	9.96 -1.15 -0.32 -0.24	1906.00 3630.00 3668.00 3860.00 3860.00	628.00 3838.00 3611.00 3633.00 3758.00	48 36 31 1
CARRIAGE Z (SM) CARRIAGE VEL SERT X SERT X SERT Z		10.38 -1.10 1.86 0.64 11.63	-0.10 -25.78 -1.12 -0.86 -0.29 -0.14	4168.00 3831.00 3924.00 3867.00	3819,00 3837,00 3880,00 3638,00	65 55 56 75 75 75
SEAT Z (SM) CHEST X CHEST Y CHEST Z CHEST RES CHEST SI	-	10.47 2.87 -0.32 16.52 16.70 87.64	-1.73 -2.37 -0.67 0.84	3867.00 3880.00 4033.00 3898.00 3898.00	3639.00 3920.00 3681.00 3684.00 3994.00	- 5 - 6 7
HEAD X HEAD X HEAD Z HEAD RES HEAD SI		1.12 1.48 13.87 13.97 24.80	-3.43 -1.65 -0.87 0.60	3986.00 3988.00 3881.00 3882.00 3839.00	3920.00 3982.00 3632.00 3610.00 3958.00	3
HEAD HIC LF SHOULDER BT SHOULDER TOTAL SHOULDER TOTAL SHO / HT		21.47 89.04 73.77 159.65 0.97	12.19 20.38 32.87 0.20	3861.00 3896.00 3902.00 3900.00	3920.00 3985.00 3997.00 3985.00 3985.00	16 17
LÊ LÂP BÊLT BI LAP BELT TOTAL LAP TOTAL LAP / HT LE SERT LNK X		53.36 50.64 103.17 0.63 16.36	15.66 10.37 26.70 0.16 -223.66	3955.00 3959.00 3958.00 3958.00 3972.00	3862.00 3868.00 3862.00 3862.00 3876.00	8 9 18
RT SEAT LNK X TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z		12.20 1.34 52.10 447.59	-95.43 -319.09 -56.85 9.04	3832.00 3972.00 3941.00 3891.00	3877.00 3877.00 3681.00 3666.00	19 35 11
RT SEAT PAN 2 CT SEAT PAN 2 TOTAL SEAT Z TOTAL SEAT Z / NT RES SEAT FORCE		369.46 912.79 1721.58 10.50 751.60	1.78 11.96 36.47 0.22 41.89	3883.00 3880.00 3881.00 3881.00	3722.00 3694.00 3669.00 3669.00 3669.00	13
RES SEAT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		10.68 -32.33 13.20 -18.71 -45.77	0.26 -192.36 -119.86 -223.53 -527.61	3881.00 3674.00 3829.00 3830.00 3830.00	3669.00 3877.00 3878.00 3878.00 3878.00	56 53 50
LF FOOT T RT FOOT T CT FOOT T TOTAL FOOT T LF FOOT Z		162.88 24.79 18.37 54.75 255.25	-20.54 -143.82 -47.49 -62.36 17.95	3862.00 3740.00 3852.00 5850.00 3863.00	3816.00 3879.00 3880.00 3890.00 3820.00	21 24 27
AT FOOT Z CT FOOT Z TOTAL FOOT Z NES FOOT FORCE		228.40 144.77 535.24 709.55	23.06 -113.74 -28.74 105.21	3878.00 3829.00 3864.00 3863.00	4061.00 3842.00 3840.00 4196.00	22 25 28

HEAD REST POS STUDY	TEST: 432	\$U8J: F-2	WT: 161.0	G: 10	GP: 1 CELL	: E
DATA ID		MAX	MIN	11	15	СН
10V EXT PHR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE Z		10.05 1.55 0.79 11.77 10.38	9.98 -0.85 -0.81 -0.26 -0.09	1945.00 3847.00 3809.00 3839.00 3840.00	677.00 3814.00 3623.00 3766.00	48 36 31
CARRIAGE VEL SEAT X SEAT T SEAT Z SEAT Z SEAT Z CHEST X		-0.90 1.18 0.79 11.64 10.41 3.21	-25.67 -1.27 -0.94 -0.14 -2.45	4135.00 3848.00 9876.00 3847.00 3847.00	3657.00 3809.00 3853.00 3633.00 3683.00	29 32 33 - 34
CHEST T CHEST Z CHEST RES CHEST SI HEAD X		-0.32 25.66 23.79 54.90	-2.03 -0.74 0.74	3861.00 3887.00 3867.00 3867.00	3891.00 3918.00 3945.00 3952.00 3931.00	5 6 7
HEAD T HEAD Z HEAD RES HEAD SI HEAD HIC LF SHOULDER		2.68 1.79 16.68 17.24 28.17 23.84	-4.14 -2.07 -1.35 0.97	3865.00 3907.00 3864.00 3864.00 3831.00 3846.00	3891.00 3861.00 3679.00 3958.00 3920.00 3889.00	3
AT SHOULDER TOTAL SHOULDER TOTAL SHD / HT LF LAP BELT		73.22 90.11 162.83 1.01 42.25	12.44 4.60 17.60 0.11 9.10	3877.00 3876.00 3877.00 3877.00 3955.00	3962.00 3964.00 3963.00 3963.00 3845.00	1 5 1 7
RT LAP BELT TOTAL LAP TOTAL LAP / NT LF SEAT LNK X RT SEAT LNK X		47.91 85.88 0.53 4.75 2.33	10.80 20.24 0.13 -283.62 -174.58	3949.00 3951.00 3951.00 4127.00	3848.00 3847.00 3847.00 3863.00	8 9 18
TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z / NT TOTAL SEAT Z / NT RES SEAT FORCE / NT		-5.61 34.67 54.37 543.04 8004.65 2012.05 2059.05	-458.20 -116.08 2.34 2.62 2.94 17.86 0.11	3727.00 3608.00 4057.00 3862.00 3864.00 3863.00 3862.00 3862.00	3863.00 3863.00 3858.00 3632.00 3707.00 3746.00 3632.00 3632.00	19 35 11 12 13
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		12.79 4.01 -11.16 -14.11 -91.93 125.13	0.13 -105.38 -146.86 -178.69 -430.93 -30.34	3862.00 3808.00 3806.00 3806.00 3807.00 3842.00	3632.00 3857.00 3657.00 3857.00	20 23 26
RT FOOT Y CT FOOT Y TOTAL FOOT Y LF FOOT Z RT FOOT Z		21.16 70.41 61.14 216.12 219.88	-174.08 -13.24 -62.46 17.67	3736.00 3880.00 3821.00 3843.00	3923.00 385;,00 3925,00 3925,00 3812.00	21 27 28
CT FOOT Z TOTAL FOOT Z BES FOOT FORCE		168.50 567.32 657.93	4.C6	3850.00 3847.00 3850.00 3851.00	3896.00 3799.00 3799.00 4194.00	25 28

	TEST: 409	SUBJ:	6-3	MT: 159.0	61 10 6	SFI & DELLE	_
HEAD REST POS STUDY	15211 409	3000.	XAX	MIN	Ti	15	CH
	47		- 05357733311237765043316173503.61031776503.61031776503.61031776503.61031776503.61031776503.61031776588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.0123503.61796588.017965888.01796588.01796588.01796588.01796588.01796588.01796588.017965888.01796588.01796588.01796588.01796588.01796588.01796588.017965888.01796588.01796588.01796588.01796588.01796588.01796588.017965888.01796588.01796588.01796588.01796588.01796588.01796588.017965888.01796588.01796588.01796588.01796588.01796588.01796588.017965888.01796588.01796888.0179688.01796888.01796888.01796888.01796888.01796888.01796888.01796888.01796888.01796888.01796888.017968888.0179688888.0179688888.01796888888888888888888888888888888888888	79021307255115004 R251 700313027300602853068 42275.3311 75.3897700602853068 42275.3311 75.38977009 75.331184.3.106.07.5335358942 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.389778078 75.38978 75.389778078 75.389778 75.	00000000000000000000000000000000000000	3629.00 3676.00 3677.00 3627.00 3627.00 3627.00 3907.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3898.00 3899.00 389	48611 9233 567 234 67 89 89 5123 036 147 258

HERO REST POS STUDY	TEST: 437	S UBJ: G-2	MT: 120.0	G: 10	GP: 2 CELL:	E
DATA ID		MAX	HIN	11	1 è	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z (SM)		10.05 1.34 0.84 12.35 10.73	9.98 -0.90 -0.73 -0.22 -0.11	200.00 3848.00 3893.00 3887.00 3887.00	871.00 3886.00 3839.00 3699.00	1 36 48
CARRIAGE VEL SEAT X SEAT Y		-0.85 1.26 0.71	-25.75 -1.07 -1.06 -0.22 -0.12	4191.00 3849.00 3967.00 3894.00 3894.00	3846.00 3901.00 3902.00 3724.00 3707.00	33 33 36 59
CHEST X CHEST Z CHEST Z CHEST RES CHEST SI		4.61 -0.53 17.47 17.53 30.45	-1.51 -1.64 -0.88 1.11	3911.00 3904.00 3925.00 3925.00 3851.00	3947.00 4008.00 3819.00 4115.00 3970.00	5 6 7
MEAD X MEAD Z MEAD Z MEAD RES MEAD SI MEAD HIC		0.68 1.58 14.05 14.08 29.08	-4.78 0.40 -1.04 0.51	3692.00 3963.00 3912.00 3912.00 3859.00 3889.00	3938.00 3919.00 3721.00 4195.00 3986.00 3981.00	2 3 4
LF SHOULDER AT SHOULDER TOTAL SHOULDER TOTAL SHO / HT		35.98 58.54 91.13 0.76	6.03 7.59 15.07 0.13 2.27	3923.00 3915.00 3923.00 3923.00	4042.00 4062.00 4061.00 4061.00 3895.00	16
LF LAP BELT RT LAP BELT TOTAL LAP TOTAL LAP / NT LF SEAT LNK X		26.90 44.63 71.45 0.60 25.74	5.06 7.35 0.06 -123.91	3996.00 3995.00 3995.00 4155.00	3896.00 3895.00 3895.00 3916.00	8 9 18
RT SEAT LNK X Total seat X		31.16 19.33 38.65	-65.33 -186.77 -20.66	3881.00 3989.00 3970.00	3917.00 3916.00 3857.00	18 19
SEAT LNK T LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE / HT		348.77 989.68 586.42 1307.93 10.90 1319.64	13.49 16.45 3.90 47.12 0.29 47.20	3906.00 3910.00 3912.00 3910.00 9910.00	3621.00 3652.00 3629.00 3627.00 3627.00 3627.00	35 1! 12 13
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		11.59 -0.48 5.87 7.14 97.53	-87.85 -125.60 -137.24 -345.34 -23.88	3851.00 3851.00 3959.00 3851.00 3889.00	9904.00 3905.00 3904.00 3905.00 3859.00	20 23 26
LF F001 Y RT F001 Y CT F001 Y T01PL F001 T		28.06 55.94 56.69 153.87	-125.46 -29.49 -55.20 -25.54	3703.00 3872.00 3671.00 3890.00	3898.00 3971.00 3909.00 3862.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		193.07 148.16 142.31 984.46 487.16	-8.32 -73.90 -43.61 17.98	3896.00 3894.00 3896.00 3890.00	3972.00 3844.00 3972.00 4162.00	22 25 28

		HT: 175.0	G: 10 G	P: 2 CELL:	E
HERD REST POS STUDY TEST: 408 SUBJ:	K-1	M1N	71	12	Сн
DRTR 1D	MHX			••	
IDATA 1D IOY EXT PWA CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Y CARRIAGE Y SEAT Y SEAT Y SEAT Z SEAT Z SEAT Z CHEST RES CHEST RES CHEST RES CHEAD X HEAD AIC HEAD AIC HEAD AIC HEAD AIC HEAD BELT TOTAL LAP BELT TOTAL LAP BELT TOTAL LAP AN Z LF LAP BELT TOTAL LAP / NT LF LAP BELT TOTAL LAP / NT LF SEAT PAN Z TOTAL SEA	X: 58924550941699.3883803075788847886182625779663514798208 R: 0.1584142556048030925182085897729935626257796634129604479820505060450450450450450450450450450450450450450				48611 9234 567 234 167 89 189 51123 036 147 228 222 222 222

HEAD REST POS STUDY TEST:	139 SUBJ: M-2	MT: 164.0	G: 10	GP: 1 CELL:	Ε
DATA ID	MAX	MIN	T1	15	СH
10V EXT PNR CARRIAGE X CARRIAGE T CARRIAGE Z	10.05 1.05 0.94 12.03	9.98 -0.78 -0.75 -0.20 -0.09	516.00 3910.00 3872.00 3903.00 3903.00	397.00 3879.00 3887.00 3733.00	46 36 31 1
10V EXT PNR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z SEAT X SEAT X SEAT Z SEAT Z SEAT Z CHEST Y CHEST T	10.46 -1.18 1.17 0.87 12.07 10.65	-25.61 -1.30 -1.08 -0.36	4181.00 3874.00 3868.00 3909.00 3910.00	3655.00 3817.00 3817.00 3737.00 3737.00	29 32 33 34
CHEST RES	0.93 -0.27 16.46 18.54 41.53	-3.18 -2.21 -0.93 0.77		3958.00 3938.00 3832.00 3864.00 3991.00	5 6 7
CHEST SI MERO X MERO T MERO RES HERO SI	0.94 1.29 13.39 13.42 18.68	-5.57 -1.05 -1.16 0.57	3830.00 4000.00 3921.00 3921.00 3881.00	3953.00 3927.00 3819.00 4200.00 4006.00	3
HEAD HIC LF SHOULDER NT SHOULDER TOTAL SHOULDER TOTAL SHOULDER	15.39 82.65 117.35 197.82 1.21	20.35 35.62 56.81 0.35	3903.00 3945.00 3940.00 3944.00	3968.00 3903.00 4070.00 3905.00 3905.00	16 17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / NT LF SEAT LNK X	64.44 82.76 146.56 0.89 37.37	16.13 18.25 35.76 0.22	4015.00 4011.00 4014.00 4014.00 4138.00	3905.00 3911.00 3911.00 3911.00 3926.00	8 9 18
RT SEAT LNK X TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z	10.71 28.01 70.65 435.90 396.18	-108.67 -286.57 -40.72 14.56 9.48	3873.00 4006.00 3979.00 3926.00	3927.00 3927.00 3924.00 3633.00 3634.00	19 35 11 12
RT SERT PAN Z CT SERT PAN Z TOTAL SERT Z TOTAL SERT Z / NT RES SERT FORCE	926.19 1756.02 10.71 1779.60	22.73 63.24 0.39 64.16	3925.00 3926.00 3926.00 3926.00	3613.00 3610.00 3610.00 3610.00	iŝ
RES SEAT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X	10.85 0.98 -12.85 -42.66 -85.04	0.39 -104.81 -189.96 -218.86 -507.35	3926.00 3872.00 3604.00 4191.00 4179.00	3610.00 3918.00 3920.00 3921.00 3920.00	20 23 26
LF FOOT Y RT FOOT Y CT FOOT Y TOTAL FOOT T	128.07 31.52 49. 07 57. 56 197.03	-30.03 -150.40 -41.70 -97.21 -0.69	3904.00 3961.00 3886.00 3886.00	3875.00 3913.00 3914.00 3927.00 3876.00	21 24 27 22
LF FOOT Z RT FJOT Z CT FOOT Z TOTAL FOOT Z MES FOOT FORCE	249.58 154.26 507.96 655.92	15.65 -94.30 0.39 97.46	3929.00 3910.00 3912.00 3921.00	4163.00 3884.00 3862.00 4172.00	22 25 28

		ur. 152 fi	G: 10 GP	: 1 CELL:	E
MERO REST POS STUDY TEST: 435	SUBJ: MII	MIN	11	72	CH
DATA 1D	***	~ -	•-		48
10V EXT PHR CARBIAGE X CARBIAGE T	10.04 1.21 0.70	9.97 -1.11 -0.71 -0.18	649.00 3892.00 3896.00 3884.00	3914.00 3860.00 3859.00 3723.00	36 31
CARRIAGE Z (SM) CARRIAGE Z (SM) CARRIAGE VEL SEAT X	10.47 -1.02 0.59	-0.08 -25.93 -1.56 -0.75	3885.00 4175.00 3893.00 4070.00 3891.00	3723.00 3855.00 3898.00 4060.00 3712.00	34 33 39 29
DATA 1D LOVERT PAR CARALAGE X CARALAGE X CARALAGE Z CHEST	11.76 10.59 4.89 0.07	-0.23 -0.13 -2.28 -2.26 -0.87	3892.00 3905.00 3959.00 3910.00	9711.00 3940.00 3908.00 3710.00 3981.00	5 6 .
CHEST Z CHEST RES CHEST SI	20.20 38.96 1.67	0.87 -4.42	3910.00 3849.00 3895.00	3972.00 3941.00 3918.00	2
HEAD X HEAD Z HEAD Z HEAD RES	1.41 12.67 12.83 21.16	-2.30 -1.67 0.66	4026.00 3910.00 3910.00 3865.00	4178.00 4200.00 3967.00 3945.00	4
HEAD SI HEAD HIC LF SHOULDER	18.35 53.49 88.73	6.89 11.69 21.31	3884.00 3925.00 3918.00 3920.00	4003.00 3977.00 3978.00	16 17
RT SHOULDER TOTAL SHOULDER TOTAL SHOULDER LE SHO / HT LE LAP BELT	0.98 52.80 67.26	0.14 8.47 11.54	3920.00 3999.00 3994.00 3997.00	3978.00 3885.00 3895.00 3886.00	8 \$
RT LAP BELT TOTAL LAP TOTAL LAP / HT LF SEAT LNK X	117.60 0.75 -0.33	20.85 0.13 -199.88 -128.03	3957.00 4169.00 3845.00	3886.00 3912.00 3907.00 3907.00	1 8 1 9
RT SEAT LNK X TOTAL SEAT X SEAT LNK Y	-4.61 21.71 428.45	-321.76 -70.90 5,50 5,69	3736.00 4154.00 3910.00 3910.00	3906.00 3625.00 3692.00	35 11 12
LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z	594.37 714.92 1730.17 11.02	14.75 41.33 C.26	3914.00 3910.00 3910.00 3910.00	3605.00 3618.00 3618.00 3618.00	13
TOTAL SEAT 2 / HT RES SEAT FORCE RES SEAT FORCE / HT LF FOOT X	1760.25 11.21 1.88	42.69 0.27 -177.14 -159.25	3910.00 3852.00 3852.00	3618.00 3903.00 3912.00 3912.00	20 23 26
RT FOOT X CT FOOT X TOTAL FOOT X	19.72 30.80 147.70	-187.52 -517.70 -25.24	3853.00 3852.00 3886.00 4088.00	3903.00 4057.00 3895.00	21 24 27
F FOOT Y RT FOOT Y CT FOOT Y	22.65 25.50 42.20	-154.80 -28.71 -60.20	4020.00 3925.00 3886.00	3897.00 3880.00 4017.00	27 22 25 28
TOTAL FOOT Y LF FOOT Z RT FOOT Z CT FOOT Z	210.00 246.60 106.7 445.2	6 -5.56 7 -96.38 9 -42.56	3912.00 3851.00 3910.00	4000.00 3865.00 3861.00	28
TOTAL FOOT Z RES FOOT FORCE	674.6	8 30.24	3912.00	4000.00	

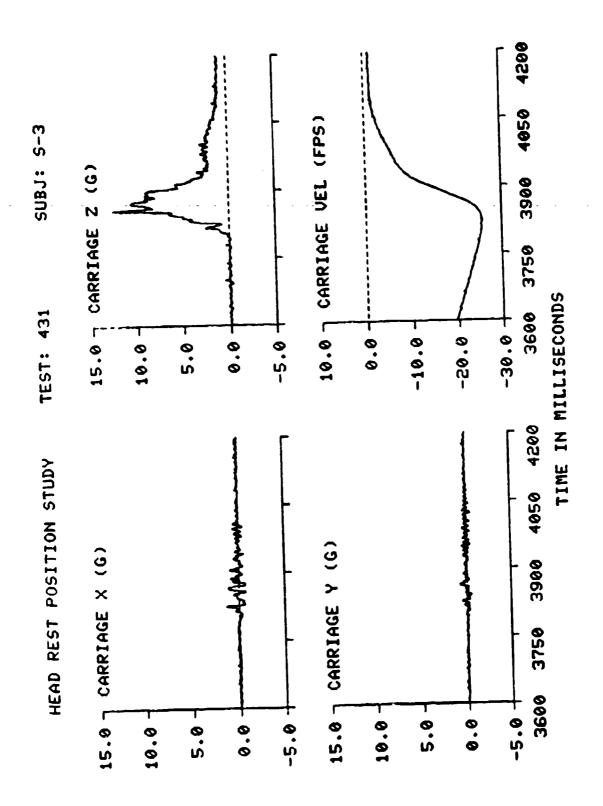
HEAD REST POS STUDY	TEST: 434	SUBJ: M10	HT: 147.0	G: 10	GP: 2 CELL:	Ε
DATA 10		MAX	H1N	<u>T1</u>	15	CH
10V EXT PHR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z CARRIAGE Z		10.05 1.56 0.90 12.28 10.49 -1.19	9.98 -1.05 -0.82 -0.21 -0.10 -25.99	9790.00 3905.00 3867.00 3698.00 3898.00 4155.00	73.00 3872.00 3872.00 3634.00 3633.00	48 36 31 1
SEAT X SEAT T SEAT Z SEAT Z (SM) CHEST X		1.16 1.09 12.07 10.70	-1.42 -1.15 -0.20 -0.14 -4.51	3907.00 3864.00 3904.00 3905.00 3920.00	3859.00 3911.00 387000 3622.00 3623.00 3947.00	39 32 34 5 5 5
CHEST Z CHEST RES CHEST SI		22.32 43.86	-4.24 -1.04 1.00	4006.00 3923.00 3923.00 3861.00	3923.00 3625.00 4005.00 3990.00	- 6 7
MEAD X MEAD T MEAD Z MEAD RES MEAD SI MEAD HIC		3.18 1.18 15.42 15.76 27.64	-2.79 -2.04 -1.21 0.39	3918.00 3968.00 3918.00 3918.00 3871.00 3897.00	3959.00 3929,00 4093.00 3866.00 4007.00 3548.00	2 3 4
LF SHOULDER AT SHOULDER TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT		22.04 53.25 43.46 96.14 0.65	4.65 3.52 8.43 0.06	3942,00 3938.00 3940.00 3940.00	4059.00 4057.00 4057.00 4057.00	1 6 1 7
RT LAP BELT TOTAL LAP TOTAL LAP TOTAL LAP / WT LF SCAT LNK X		34.73 53.35 83.60 0.57 13.58	8.20 11.30 20.86 0.14 -212.05	3941.00 4011.00 4012.00 4012.00	3693.00 3905.00 3699.00 3699.00	8
AT SEAT LNK X TOTAL SEAT X SEAT LNK T LF SEAT PAN Z		7,57 2,02 32.61 391,63	-110.57 -322.62 -69.46 4.17	4152.00 3971.00 4177.00 4118.00	3913.00 3913.00 3913.00 3923.00	18 19 35
RT SEAT PAN Z C1 SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z NT RES SEAT FORCE / HT		428.61 900.70 1719.42 11.70 1751.04	-0.85 13.48 25.94 0.18 28.13	3914.00 3914.00 3914.00 3914.00 3914.00 3914.00	3691.00 3523.00 3633.00 3633.00 3633.00 3633.00	1 I 1 2 1 3
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		\$.12 6.59 12.84 13.94 102.09	-78.06 -134.40 -150.83 -359.69 -26.31	3653.00 3802.00 3864.00 3863.00 3899.00	3913.00 3915.00 3916.00 3915.00 4053.00	20 23 26
AT FOOT Y CT FOOT Y TOTAL FOOT T LF FOOT 7		16.54 59 .29 6 0.98 172.85	-154,73 -22.59 -65.93 -42,85	3878,00 3882.00 3879.00 3925.00	3908.00 3898.00 3873.00 3872.00	24 27 22
RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		157.57 187.32 459.30 520.54	-22.08 -51.89 -59.94	3910,00 3907.00 3908.00 3910.00	3677.00 3856.00 3856.00 4191.00	25 28

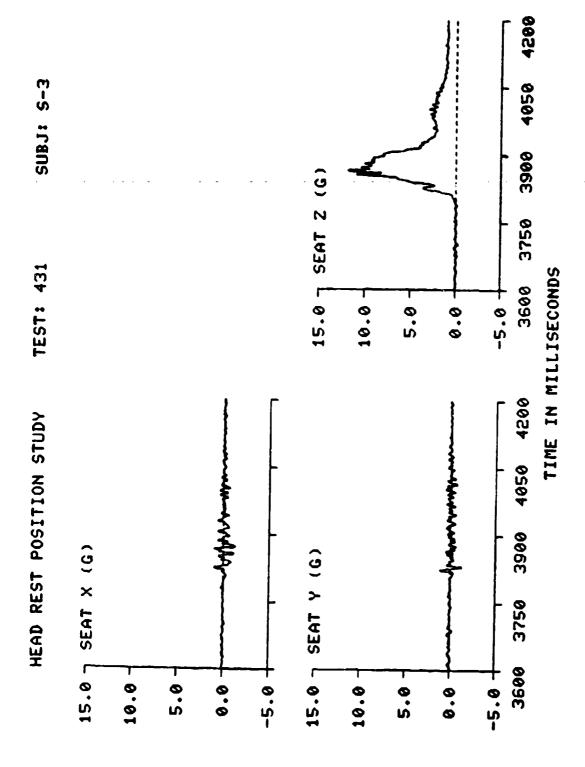
HEAD REST POS STUDY TEST: 438	SUBJ: MI3	HT: 171.0	G: 10 GP	15 1 CELL!	E CH
IDV EXT PHR CARRIAGE X CARRIAGE Y	10.05 1.36 1.29 12.04	9.98 -0.94 -0.59 -0.28 -0.10	61.00 3841.00 3882.00 3874.00 3874.00	10.00 3854.00 3855.00 3794.00 3796.00 3831.00	48 36 31
CARAJAGE Z (SM) CARAJAGE VEL SEAT X SEAT T	-1.12 1.20 0.64 11.93	-25.61 -1.37 -0.92 -0.15 -0.10	4181.00 3921.00 3655.00 3681.00	3687.00 3647.00 3714.00 3717.00	29 28 39 34 5
SENT Z (SM)	0.05 0.06 25.92 25.93	2.43 -1.96 -0.65 0.29	3892.00 3986.00 3902.00 3902.00	-3928.00 -3892.00 -3607.00 -3985.00 -3978.00	6·- 7
CHEST BES CHEST SI HEAD X HEAD I HEAD I HEAD BES	17.54 0.64 2.17 16.20 16.29 28.51	-4,37 0.33 -1,16 1.18	3701.00 3992.00 3694.00 3894.00 3855.00 3873.00	3928.00 3916.00 3633.00 4199.00 4097.00 3935.00	594
HEAD SI HEAD HIC LF SHOULDER AT SHOULDER TOTAL SHOULDER	19.63 101.26 111.17 212.49	30.58 5.59 36.37 0.21	3909.00 3909.00 3909.00 3909.00 3987.00	3974.00 3976.00 3975.00 3975.00 3882.00	16 17 8
TOTAL SHD / H! LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP HT	55.07 79.74 127.93 0.75 12.66	14.57 21.72 0.13 -212.97	3984.00 3985.00 3985.00 4117.00 3653.00	\$880.00 \$661.00 \$881.00 \$890.00 \$888.00	9 18 19
DATA 1D ORTA 1D ORTA 1D ORTA 1D IDVENTE PHR CRARIAGE Y CRARIAGE Y CRARIAGE Z CRARIAGE Z CRARIAGE Z CRARIAGE Z CRARIAGE Z SERT Z SERT Z SERT Z SERT Z SERT Z SERT Z SERT Z SERT Z CHEST X CHEST Y CHEST Y CHEST Y CHEST X HEAD Y HEAD X HEAD	-6.45 -4.67 -4.67 346.10 476.13 924.48 1736.30	-393.89 -37.86 -0.61 7.91 9.09 31.35	1184.00 1957.00 1890.00 1892.00 3692.00 1692.00	3888.00 3682.00 3609,00 3768.00 3610.00 3616.00 3616.00	95 11 12 13
TOTAL SERT L/ N' RES SERT FORCE / HT LF FOOT X RT FOOT X	1780.04 10.41 -23.72 -10.01 -50.21	0,25 -158.44 -120.16 -182.26	3892.00 3841.00 3847.00 3840.00 3842.00	3616.00 3891.00 3891.00 3900.00 3891.00	2C 23 26
CT FOOT X TOTAL FOOT X LF FOOT Y AT FOOT Y CT FOOT Y	-70.18 142.34 24.90 26.08	-453.70 -29.73 -129.51 -47.79 -54.60	3876.00 3784.00 3690.00 3639.00	3831.00 3876.00 3884.00 3684.00 3832.00	21 24 27 22
TOTAL FOOT Y LF FOOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z NES FOOT FORCE	215.62 232.32 145.41 520.1 671.5	7.40 24.57 4 -141.71 3 -57.81 113.44	3901.00 98.00 98.00 99.00 99.00 9901.00	3931.00 3852.00 3832.00	22 25 28

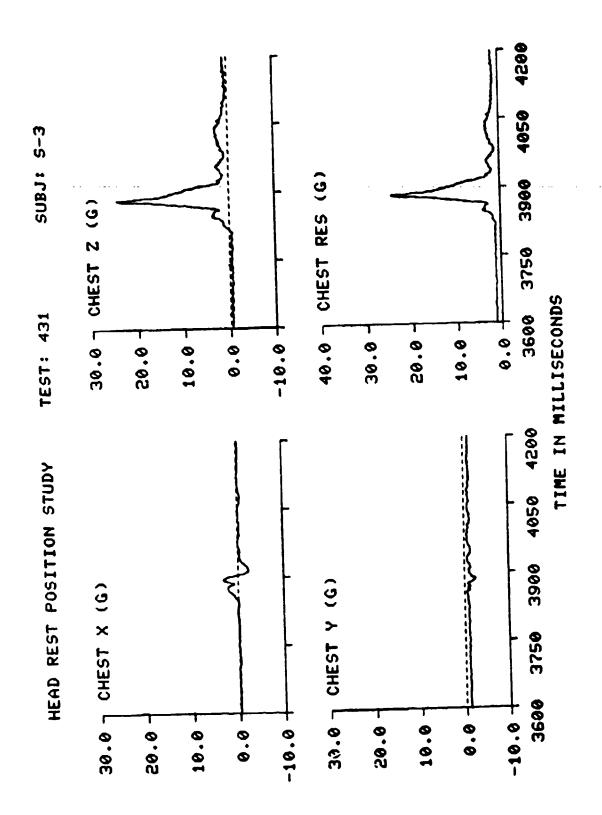
HEAD REST POS STUDY	TEST: 416	SUBJ: R-2	HT: 145.0	G: 10	GP: 1 CELL:	E
DATA ID		MAX	MIN	T 1	15	CH
LOV EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z (SM)		10.05 1.61 0.56 12.25	9.96 -1.05 -0.98 -0.21 -0.10	1441.00 3918.00 3918.00	318.00 3890.00 3891.00 3645.00	48 36 31
CARRIAGE VEL SEAT X		10.59 -1.03 1.36 0.87 11.29	-25.62 -1.36 -0.86 -0.27	3912.00 4197.00 3918.00 3875.00	3684,00 3878,00 3924,00 3883,00 3653,00 3722,00	29 32 33 34
BERT Z (SM) CHEST X CHEST T CHEST Z CHEST RES CHEST SI		10.65 2.58 -0.28 18.21 18.21 18.33	-0.17 -1.09 -2.71 -1.10 0.72	3918.00 3929.00 3920.00 3937.00 3937.00	3967.00 3949.00 3678.00 3669.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD RES HEAD SI		0.39 0.95 14.86 14.93	-4.91 -1.21 -0.59 0.64	3853.00 3766.00 3929.00 3929.00 3883.00	3970.00 3956.00 3758.00 3719.00 4146.00	2 3 4
HEAD HIC LF SHOULDER AT SHOULDER TOTAL SHOULDER TOTAL SHOULDER		17.05 \$9.32 39.66 95.47 0.66	19.18 11.27 30.68 0.21	3909.00 3947.00 3958.00 3949.00	3956.00 3915.00 3913.00 3913.00 3913.00	16 17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / HT LF SEAT LNK X		40.38 62.69 102.95 0.71 38.42	8.52 15.29 25.65 0.18 -140.02	4012.00 4008.00 4008.00 4008.00 4151.00	3913.00 3920.00 3913.00 3913.00 3924.00	8 9 18
RT SEAT LNK X TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z		26.83 48.53 58.66 282.97	-82.03 -210.54 -7.51 3.66	3985.00 3998.00 3975.00 3926.00	3933.00 3933.00 3501.00 3618.00	19 35
RT SERT PRN 2 CT SERT PRN 2 TOTAL SERT 2 TOTAL SERT 2 / HT RES SERT FORCE		415.80 1020.30 1679.60 11.58 1692.18	1.84 39.01 60.77 0.42 60.83	3935.00 3934.00 3934.00 3934.00	3656.00 3604.00 3625.00 3625.00 3625.00	12 13
RES SERT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		11.67 9.46 18.01 51.11 79.67	0.42 -168.66 -136.19 -197.38 -496.83	3934.00 3878.00 3878.00 3879.00 3879.00	3625.00 3928.00 3929.00 3930.00 3929.00	28 28 28
LF FOOT T RT FOOT T CT FOOT T TOTAL FOOT T		130.11 25.10 29.40 68.65	-14.88 -124.88 -50.69 -61.02	3914.00 4119.00 3899.00 3898.00	4135.00 3922.00 3927.00 3943.00	21 24 27
LF FOOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		173.02 203.02 133.34 435.55 824.39	-32.74 -27.68 -85.07 -104.40 32.16	3915.00 3930.00 3933.00 3915.00 3930.00	3870.00 3894.00 3870.00 3870.00 3722.00	22 25 28

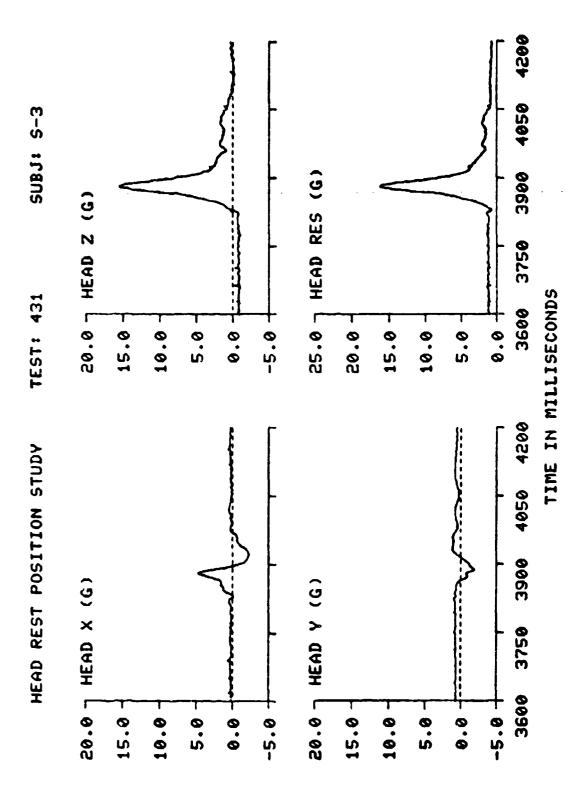
							P: 2 CELL:	F
HEAD REST POS STUDY	TEST: Y	145 2	16 J :	R-3	HT: 146.0	••••	72	CH
DATA ID				MAX	HIN	T1	16	
****				10.02	9,97	63.00	4083.00	48
IOV EXT PHR CARRIAGE X				1.59	-1.08 -0.44	3870.00 3869.00	3836.00 3887.00	31 31
CARRIAGE T				15.01	-0.19 -0.09	3863.00 3863.00	3658.00 3659.00	1
CARRIAGE Z (SH)				-0.98	-26.00	4197.00 3829.00	3829.00 3877.00	29 32 33
CARRIAGE VEL				1.70 0.8 0	-1.38 -0.93	9937.00	3878.00 3677.00	93 34
SERT T SERT Z				12.21	-0.21 -0.12	3869.00 3870.00	3678.00	3¥
SERT Z (SM)	•			นี้ นั้น	-1.18 -3.25	3893.00 3875.00	3923.00 3883.00	5 6 7
CHEST T				15.43	-0.86 1.28	3882.00 3882.00	3854.00 4112.00	,
CHEST RES				32.26	-4.54	3831.00 3826.00	3954.00 3929.00	2
CHEST SI HEAD X HEAG Y				2.16	0.60	3886.00 3884.00	3913.00 3771.00	3 4
HEAD Z				14.55	-0.88 1.14	3886.00 3835.00	3831.00 4061.00	
HEAD RES HEAD SI				22.47 15.66		3861.00	3906.00 4010.00	16
HEAD HIC LF SHOULDER				72.95	16.68 22.05	3922.00	4029.00	iř
AT SHOULDER				178.36	42.13 0.29	3921.00 3921.00	4051.00	8
TOTAL SHO / HT				54.02	28.75 32.83	3956.00 39 5 7.00	3872.00 3871.00	9
AT LAP BELT				125.91	61.61 0.42	3956.00 3956.00	3872.00 3872.00	
TOTAL LAP / HT				31.76	-166.82 -93.61	4152.00 3830.00	3879.00 3885.00	18 19
AT SEAT LAK X				18.20	-255.70	3976.00 3972.00	3884.00	35
TOTAL SEAT X SEAT LNK T				37.58 430.84	-91.97 16.63	3880.00	3617.00 3600.00	11
LF SEAT PAN Z				456.00 783.78	29.15 39.50	3881.00 3883.00	3655.00	13
CT SEAT PAN Z TOTAL SEAT Z				1657.83	93.05 0.64	3882.00 3882.00	3600.00	
TOTAL SEAT Z / HT				1678.09	94.24	3882.00 3882.00	3600.00 3600.00	20
RES SERT FORCE / HT	Γ			6.49	-120.99 -55.68	3829.00 3868.00	3879.00 3876.00	23
RT FOOT X				72.66	-104.43 -270.62	3830.00 3830.00	3878.00 3879.00	26
CT FOOT X TOTAL FOOT X				77.95 116.91	-16.74	3865.00 3925.00	3837.00 3866.00	21 24 27
LF FOOT Y				20.85 17.21	-74.10 -59.32	3992.00	3882.00 3882.00	
CT FOOT Y TOTAL FOOT Y				138.60	-55.65 -26.22	3849.00 3873.00	3967.00	22 25
LF FOOT Z				123.35	-40.46 -110.56	3866.00 3871.00	3839.00	28
CT FOOT Z TOTAL FOOT Z				337.16	-125.92 2.70	3873.00 3889.00		
DATA 1D OATA 1D IONAL SERVER TO EXAMPLE SERVER				300.00				

HEAD REST POS STUDY	TEST: 431 SUBJ	: 5-3	MT: 166.0	G: 10	SP: 2 CELL:	E
DATA ID		MAX	MIN	T1	T2	CH
10V EXT PHR CRARIAGE X CARRIAGE Y CARRIAGE Z		10.04 1.39 0.78 12.57	9.98 -0.79 -0.56 -0.29	159.00 3825.00 3863.00 3858.00 3858.00	24.00 3857.00 3840.00 3694.00 3694.00	48 36 31 1
CARRIAGE Z (SM) CARRIAGE VEL SERT X SERT Y SERT Z		10.50 -0.89 1.02 1.16 11.90	-0.19 -25.78 -1.32 -1.26 -0.30	4164.00 3867.00 3823.00 3864.00	3821.00 3872.00 3872.00 3631.00 3701.00 3702.00	39 39 34
ŠĒAT Ž (SH) CHĒST X CHĒST Z CHĒST Z CHĒST RES		10.61 9.26 -0.53 24.40 24.54	-0.20 -2.31 -2.50 -0.74 0.96	3865.00 3893.00 3982.00 3684.00 3884.00	3915.00 3885.00 3701.00 4144.00	5 6 7
CHEST SI HEAD X HEAD Y HEAD Z HEAD RES		49.99 4.71 1.19 15.59 16.26	-2.25 -1.96 -1.09 0.57	3827.00 3879.00 3937.00 5881.00 3881.00 3839.00	3874.00 3920.00 3887.00 3774.00 4193.00 3960.00	3
MEAD SI MEAD HIC LF SHOULDER AT SHOULDER TOTAL SHOULDER		25.14 20.26 77.40 47.11 121.02 0.73	13.00 5.59 24.24 0.15	\$663.00 3896.00 3907.00 3906.00 3905.00	3904.00 4095.00 3997.00 4095.00 4095.00	16 17
TOTAL SHO / HT LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / HT		40.94 80.48 80.48	14.01 12.15 27.67 0.17	3921.00 3949.00 5955.00 3955.00	3864.00 3867.00 3865.00 3865.00	8 9
LF SEAT LNK X RT SEAT LNK X TOTAL SEAT X		17.65 -3.84 -0.69	-213.17 -159.09 -370.49	4113.00 3671.00 4139.00	3874.00 3876.00 3875.00	18
SEAT LNK T LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE		\$2.49 504.59 543.27 847.06 1884.95 11.96	-83.12 19.99 17.80 9.76 64.81 0.89 68.44	4013.00 3882.00 3877.00 3881.00 3878.00 3878.00 3878.00	3686.00 3808.00 3798.00 3602.00 3602.00 3602.00	35 11 12 13
RES SERT FORCE / HT LF FOOT X RT FOOT X CT FOOT X		11.58 5.75 11.37 59.44	0.41 -123.54 -75.87 -148.96 -295.48	3878.00 3825.00 3822.00 3826.00 3825.00	3602.00 3886.00 3875.00 3884.00 3886.00	20 23 26
TOTAL FOOT X LF FOOT Y RT FOOT Y CT FOOT Y		64.17 111.79 18.51 42.75	-27.97 -88.87 -65.82	3860.00 3825.00 4003.00	4034.00 3860.00 3870.00	21 24 27
TOTAL FOOT Y LF FOOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		40.20 175.45 192.96 932.07 514.97 591.16	-52.80 -40.16 -29.06 -74.08 -65.69 14.67	3846.00 3886.00 3861.00 3882.00 3885.00 3885.00	5870.00 3855.00 3997.00 3834.00 3834.00 4098.00	22 25 28

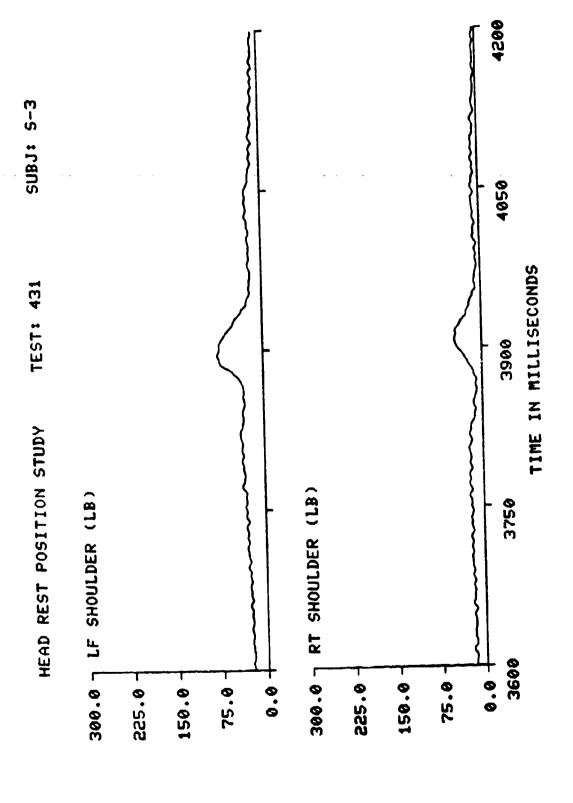


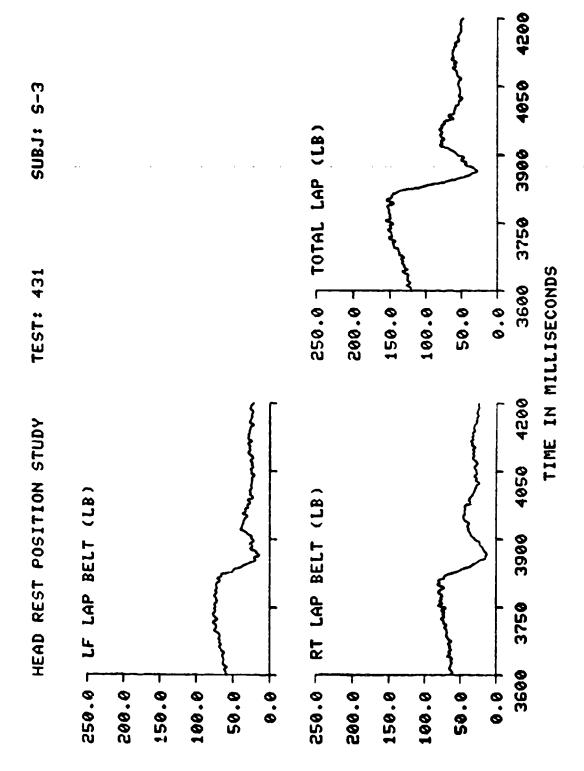


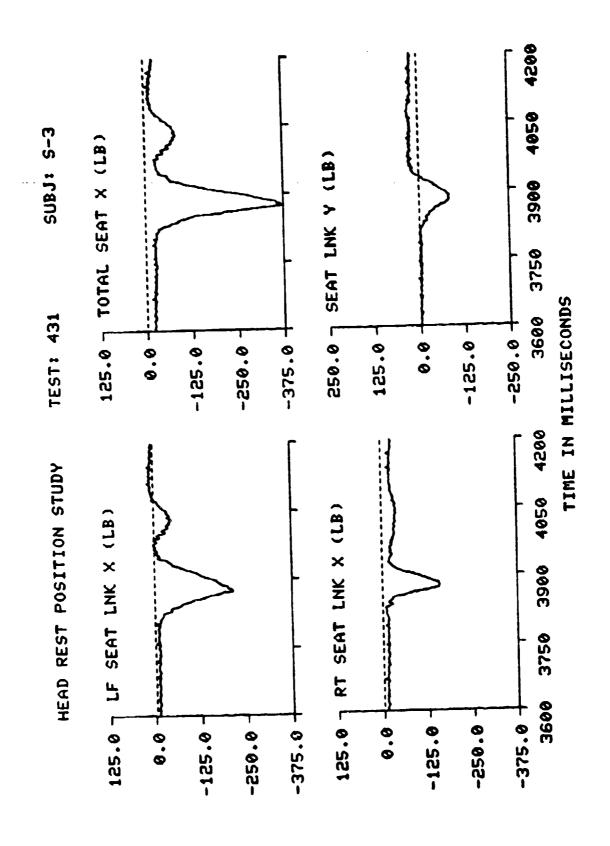


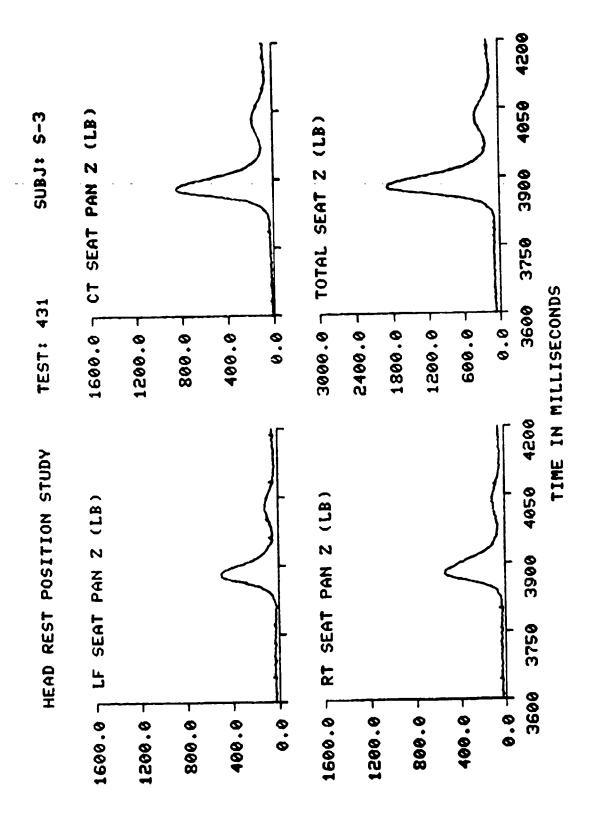


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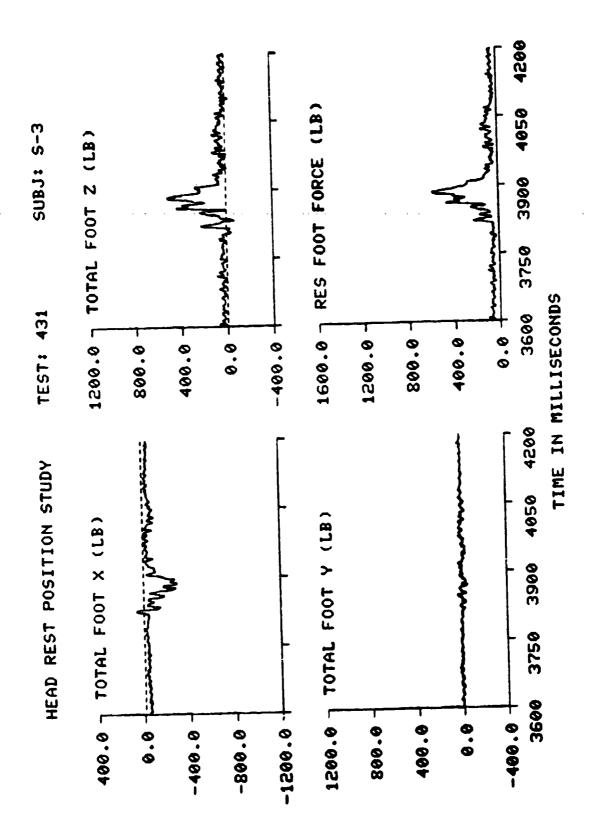






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HEAD REST POS STUDY	TEST: 415	SUBJ: D-1	NT: 209.0	G: 10	GP: 1 CELL:	F
DATA ID		HAX	HIN	<u> 1</u>	T2	C H
10V EXT PHR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z (SM)		10.05 1.60 0.58 12.72 10.47	9.96 -1.17 -0.50 -0.30 -0.19	1167.00 3888.00 3887.00 3881.00	97.00 3681.00 3958.00 3796.00 3671.00	48 36 31 1
CARRIAGE VEL		-1.00	-25.34 -1.57 -1.15 -0.23 -0.11	4190.00 3876.00 3845.00 3888.00 3889.00	3841.00 3881.00 3852.00 3663.00 3664.00	29 32 33 34
CHEST X CHEST Y CHEST Z CHEST RES CHEST SI HEAD X		6.50 -0.15 20.05 21.05 5.22	-1.49 -2.59 -0.60 0.40	3902.00 3984.00 3906.00 3905.00 3847.00	3933.00 3905.00 3976.00 3606.00 3984.00	5 6 7
MERD Y MERD Z MERD RES MERD SI MERD HIC		1.83 13.68 14.56 25.33 21.78	-0.16 -0.06 -0.94 0.90	3902.00 3958.00 3899.00 3899.00 3859.00	3939.C0 3917.00 3721.00 4176.00 3981.00	2 3 4
LF SHOULDER AT SHOULDER TOTAL SHOULDER TOTAL SHD / HT LF LAP BELT		98.04 85.87 161.07 0.77 60.05	21.47 5.92 27.98 0.13 19.48	3917.00 3923.00 3921.00 3921.00 3983.00	3942.00 4092.00 4075.00 4075.00 3887.00	16 17
RT LAP BELT TOTAL LAP TOTAL LAP / NT		67.14 125.18 0.60	29.02 48.99 0.23	3995.00 3995.00	3890.00 3888.00 3888.00	8 9
RT SEAT LNK X TOTAL SEAT X SEAT LNK Y		95.28 20.21 47.93 59.02	-200.71 -83.08 -283.79 -66.28	4112.00 3970.00 3980.00 3963.00	3896.00 3896.00 3896.00 1 95.00	1 8 1 9
LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE		525.79 507.99 1249.34 2275.22 10.89 2292.45	9.11 10.51 38.38 72.58 0.35	3898.00 3904.00 3900.00 3899.00 3899.00	3644.00 3606.00 3625.00 3627.00 3627.00	13
RES SEAT FORCE / HT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X		10.97 2.60 -11.01 -7.76 -16.19	73.32 0.35 -194.50 -176.67 -261.80 -625.84	3899.00 3899.00 3848.00 3848.00 3848.00 3848.00	3627.00 3627.00 3898.00 3899.00 3900.00 3998.00	20 23 26
LF FOOT Y RT FOOT Y CT FOOT Y TOTAL FOOT Y		165.64 27.63 19.60	-21.28 -152.51 -50.71 -67.19	3883.00 3799.00 3941.00 3940.00	3990.00 3892.00 3901.00 3901.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		51.95 219.32 279.24 209.80 621.44 821.45	-14.12 12.69 -93.82 -6.99 78.52	3884.00 3905.00 3903.00 3904.00 3907.00	3969,00 4137,00 3839,00 3839,00 4120,00	22 25 28

HERD REST POS STUDY TEST: 433 SUBJ:	F-3	HT: 164.0	G; 10 (GP: 1 CELL:	F
ORTH ID	MAX	H1N	Ti	T2	CH
10V EXT PHR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE Z (SH) CARRIAGE VEL SERT X SERT Z SERT Z SERT Z CHEST X	10.04 1.36 0.65 12.09 10.41 -0.92 1.20 0.82 11.51 10.57 5.08	9.98 -0.72 -0.62 -0.13 -1.19 -0.80 -0.11 -2.95	14.00 3914.00 3915.00 3907.00 3908.00 4181.00 3872.00 4020.00 3915.00 3915.00 3918.00	2405.00 3886.00 4020.00 3824.00 3865.00 3865.00 4026.00 3737.00 3737.00 3737.00 3737.00	48 39 1 29 23 34 5 6 7
CHEST Z CHEST RES CHEST SI HEAD X HEAD Y HEAD Z HEAD RES	18.17 43.84 5.75 1.79 15.93 17.07	0.62 -0.01 -2.23 -1.27 0.94	3942.00 9871.00 9931.00 4026.00 3931.00 3931.00 3895.00	3884.00 4104.00 3938.00 3753.00 4141.00 3991.00	2 3 4
HEAD MIC LF SHOULDER RT SHOULDER TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT RI LAP BELT	23.57 56.56 93.38 143.23 0.87 50.82 53.47	4.71 12.50 19.88 0.12 5.48 9.83 16.77	3950.00 3943.00 3944.00 3944.00 4016.00 4012.00 4017.00	4046.00 4041.00 4046.00 4046.00 3918.00 3911.00	16 17 8
TOTAL LAP TOTAL LAP / HT LF SEAT LNK X RT SEAT LNK X TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z / HT	0.63 24.99 8.82 45.89 495.08 970.57 865.62 1726.52	0.10 -253.21 -72.21 -322.93 -84.74 5.73 5.73 5.04 22.92 0.114	4017.00 4173.00 3978.00 4185.00 4001.00 3924.00 3927.00 3927.00 3927.00	3918.00 3923.00 3925.00 3926.00 3913.00 3613.00 3609.00 3609.00	18 19 35 11 12 13
DATA ID ORTA ID ORTA ID TOV EXT PHR CARRIAGE Y CARRIAGE Y CARRIAGE Y CARRIAGE Y CARRIAGE VEL SERT Y SERT Z SERT Z SERT Z CHEST Z CHEST Z CHEST X CHEST SI HERD X HERD X HERD SI HERD SI HERD Y HERD ES HERD SI HERD Y HERD ES HERD Y HERD ES HERD Y HERD Y HERD Y HERD Z HERD NI LAP BELT TOTAL LAP TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z TOTAL FOOT Z RES FOOT FORCE	17.72 -38.71 -0.892 -153.47 23.61 24.99 47.10 219.11 211.61 119.59	-185.58 -1237.76 -1237.76 -237.23 -551.76 -23.23 -135.53 -59.606 258.84 -80.575 177.88	3977.00 3875.00 3875.00 3875.00 3875.00 3909.00 3911.00 4028.00 3916.00 3916.00	3925.00 3925.00 3927.00 3909.00 39224.00 4022.00 4022.00 3966.00	20 23 28 21 227 227 228

HEAD REST POS STUDY	TEST: 444	SUBJ: F-2	HT: 160.0	G: 10	GP: 1 CELL:	F
DATA 10		MAX 	MIN	T1	T2	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z (SM)		10.05 1.13 0.65 12.42 10.53	9.97 -1.04 -0.69 -0.17 -0.04	20.00 3828.00 3829.00 3820.00 3821.00	756.00 3635.00 3801.00 3697.00 3632.00	46 36 31
			-25.73 -1.54 -1.09 -0.22 -0.12	4109.00 3784.00 3783.00 3827.00 3827.00 3842.00	3775.00 3775.00 3834.00 3793.00 3708.00	29 32 33 34
CHEST X CHEST Y CHEST Z CHEST RES CHEST SI HERD X		22.8 3 45. 75	-0.64 -1.77 -0.60 0.66	3829.00 3850.00 3850.00 3785.00	3876.00 3848.00 3678.00 3778.00 3910.00	5 6 7
HEAD Y NEAD Z HEAD RES HEAD SI HEAD HIC		1.41 1.51 15.39 15.45 23.74 19.75	-2.69 -0.45 -1.20 0.95	3843.00 3924.00 3843.00 3843.00 3807.00 3821.00	3861.00 3836.00 3652.00 4079.00 3893.00 3875.00	3
LF SHOULDER RT SHOULDER TOTAL SHOULDER TOTAL SHO / WT LF LAP BELT		31.30 83.05 104.22 0.65 79.74	11.35 27.55 43.90 0.27 28.23	3871.00 3852.00 3857.00 3857.00 3857.00	3838.00 4085.00 4083.00 4093.00 3830.00	16
AT LAP BETT TOTAL LAP TOTAL LAP / NT LF SEAT LNK X BT SEAT LNK X		88.10 186.90 1.04 12.81 7.60	29.21 57.44 0.36 -234.69	3919.00 3925.00 3925.00 4078.00 3613.00	3830.00 3830.00 3830.00 3841.00 3842.00	8 9 18 19
TOTAL SEAT X SEAT LNK T LF SEAT LNK T LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT FORCE RES SEAT FORCE / HT		-3.00 23.38 551.36 472.28 775.08 1795.98 11.22 1836.69	-362.56 -137.63 13.77 11.93 47.50 0.30 48.61	3646.00 4048.00 3644.00 3843.00 3840.00 3840.00 3840.00	3842.00 3638.00 3662.00 3613.00 3623.00 3623.00 3629.00	35 11 12 13
LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y RT FOOT Y TOTAL FOOT Y TOTAL FOOT Y		13.45 -9.90 -13.76 -21.66 118.37 15.73 56.79	-95.04 -15.32 -169.38 -395.46 -37.98 -152.66 -65.90	3840.00 3787.00 3786.00 3786.00 3787.00 3822.00 3652.00 3651.00 3785.00	3629.00 3935.00 3838.00 3835.00 3835.00 3793.00 3820.00 3962.00	20 23 26 21 24 27
LF FOOT Z DT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		214.81 206.80 197.59 526.64 578.86	1.99 6.42	3822.00 3832.00 3825.00 3829.00 3832.00	3904.00 4016.00 3619.00 3779.00 4063.00	22 25 28

HEAD REST POS STUDY	TEST: 414	\$UBJ: G-3	HT: 160.0	G: 10	GP: 2 CELL:	F
DATA 1D		HAX	HIN	Ti	12	CH
10V EXT PHR CRRAJAGE X CRRAJAGE T CRRAJAGE Z CARRIAGE Z CARRIAGE Z (SM)		10.05 1.44 1.07 12.40 10.47	9.96 -1.06 -0.62 -0.26 -0.12	1782.00 3848.00 3860.00 3855.00 3856.00	188.00 3810.00 3972.00 3676.00 3660.00	48 36 31 1
CARRIAGE Z (SM) CARRIAGE VEL SEAT X SEAT T SEAT Z SEAT Z (SM)		-1.11 1.36 1.01 11.86 10.64	-25.54 -1.27 -1.61 -0.20 -0.08	4162.00 3648.00 3821.00 3862.00 3863.00	3821.00 3835.00 3827.00 3771.00 3770.00	34 35 35 59
CHEST X CHEST Y		2.55 0.36	-3.63 -4.16 -2.29	3878.00 3980.00 3899.00 3901.00 3821.00	3926.00 3903.00 3994.00 3982.00 3983.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD RES HEAD SI		2.11 1.24 19.28 13.43 27.47 24.42	-4.32 -0.74 -1.26 0.80	3883.00 4018.00 5678.00 3878.00 3827.00	3924.00 3905.00 3976.00 3968.00 3960.00	4 E S
HEAD HIC LF SHOULDEA AT SHOULDEA TOTAL SHOULDEA TOTAL SHO / HT		24.42 115.10 97.40 210.05 1.91 59.71	15.67 2.80 19.63 0.12	3654.00 3904.00 3909.00 3906.00	3934.00 3983.00 4008.00 3996.00	16 17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / WT LF SEAT LAK X		89.98 149.46 0.93 13.64	14.07 32.00 46.67 0.29 -170.35 -108.47	3937.00 3936.00 3936.00 4167.00	3861.00 3863.00 3862.00 3862.00 3872.00	8 9 18 19
AT SEAT LNK X TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z AT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z / NT RES SEAT FORCE		5.85 -2.34 41.16 561.05 539.46 644.60 1742.60 1764.46	-100.47 -275.11 -84.74 22.80 16.83 21.41 73.19 0.46 73.68	3714.00 4143.00 9989.00 3878.00 3879.00 3879.00 3879.00	3875.00 3880.00 3623.00 3619.00 3619.00 3609.00 3609.00	35 11 12 13
RES SERT FORCE / NT LF FOOT X RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		11.03 13.78 26.52 44.88 67.19 121.57	0.46 -132.69 -84.50 -153.68 -364.64 -17.31	3679.00 3624.00 3622.00 3623.00 3623.00 3956.00 3911.00	3609.00 3881.00 3873.00 3675.00 3881.00 3835.00	20 23 28 21
RT FOOT Y CT FOOT Y TOTAL FOOT Y LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		37.17 11.18 37.92 172.83 190.67 136.66 438.88 570.81	-111.92 -54.68 -37.58 -33.74 -15.07 -80.42 -114.80 22.04	3669.00 3620.00 3881.00 3883.00 3862.00 3881.00	3859.00 3652.00 3833.00 3816.00 3816.00 3816.00	24 27 22 28

HEAD REST POS STUDY TEST: 443	SUBJ: G-2	NT: 118.0	G: 10	GP: 2 CELL:	F
DATA ID	MAX	MIN	T 1	15	CH
IOV EXT PHR CARRIAGE X CARRIAGE Y CARRIAGE Z CARRIAGE Z CARRIAGE Z (SM)	10.05 1.33 0.89 13.06 10.79	9.97 -1.30 -0.88 -0.54 -0.17	59.00 3863.00 3863.00 3856.00 3857.00	609.00 3856.00 3811.00 3777.00 3778.00	48 36 31 1
CARRIAGE VEL SEAT X SEAT Y SEAT Z SEAT Z (SM)	-1.07 1.65 0.97 11.62 10.61	-25.88 -1.68 -0.69 -0.24 -0.14	4152.00 3821.00 3820.00 3864.00	3618.00 3856.00 3925.00 3674.00 3672.00	29 32 33 34
CHEST X CHEST Z CHEST Z CHEST RES CHEST SI HEAD X	20.86 20.94 37.64	-1.00 - -2.10 -0.86 0.51	3881.00 3886.00 3895.00 3895.00 3823.00	3916.00 3904.00 3791.00 3780.00 3960.00	5 6 7
HEAD Y HEAD Z HEAD RES HEAD SI HEAD HIC	1,34 0.98 15.14 15.16 27.72 23.52	-3.45 -0.10 -0.74 0.68	3950.00 4033.00 3880.00 3881.00 3829.00 3860.00	3905.00 3883.00 3772.00 3977.00 3940.00 3916.00	3
LF SHOULDER RT SHOULDER TOTAL SHOULDER TOTAL SHOULDER LF LRP BELT	54.60 71.28 122.27 1.04 52.41	11.56 8.07 22.20 0.19 24.93	3900.00 3893.00 3894.00 3894.00 3965.00	4100.00 3960.00 4100.00 4100.00 3856.00	16 17 8
RT LAP BELT TOTAL LAP TOTAL LAP / HT LE SEAT LNK X	62.44 113.47 0.96	18.85 45.71 0.39	3972.00 3965.00 3965.00	3868.00 3860.00 3860.00	9
RT SEAT LNK X TOTAL SEAT X SEAT LNK Y	13.95 20.51 2.92 16.85	-158.15 -66.09 -221.89 -59.42	4102.00 3852.00 4124.00 4092.00	3888.00 3892.00 3891.00 3873.00	18 19 35
LF SCAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE RES SEAT FORCE / HT	366.00 372.14 481.89 1218.63 10.33 1238.58 10.50	22.32 21.07 3.30 61.59 0.52 0.52	3881.00 3882.00 3881.00 3881.00 3881.00 3881.00	3601.00 3638.00 3658.00 3653.00 3653.00 3653.00	35 11 12 13
LF F00T X BT F00T X CT F00T X T0TAL F00T X	5.04 ~6.73 ~7.82	-98.93 -129.22 -155.40 -380.02	3823.00 3822.00 4167.00 3823.00	3874.00 3858.00 3874.00 3874.00	20 23 26
LF F00T T RI F00T T CT F00T T T0TAL F00T T	-29.09 97.62 22.20 47.72 55.39	-38.64 -146.41 -11.02 -58.48	3859.00 3787.00 3897.00 3897.00	3830.00 3857.00 3946.00 3831.00	21 24 27
LF FOOT Z RT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE	183.91 177.71 148.60 392.97 523.47	-3.28 1.95 -76.67 -31.26 45.72	3860.00 3859.00 3865.00 3865.00	3947.00 3954.00 3811.00 3947.00 4136.00	22 25 28

OATA ID	HEAD REST POS STUDY	TEST: 413	SUBJ: K-1	MT: 175.0	G: 10 G	P: 2 CELL:	F
10 EXT PHR							
TOTAL FOOT Z 486.75 15.60 3848.00 4114.00	PHR CRARIAGE Z CRARIAGE Z VEL CRARIAGE Z CRARIAGE Z VEL CRARIAGE Z VEL SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S SEAT X S S S S S S S S S S S S S S S S S S S		5719769382415665988733884241057399233353806744479712573953884156695988735411979602775996244797971256991111111111111111111111111111111111	999332147392805 4174 1290403276776403970228142466105 91100511001210 4211 42705684002778886335687794393779 113588633567794393379 113588633567794393379	00000000000000000000000000000000000000	00000000000000000000000000000000000000	551 9254 567 234 667 89 89 5123 036 147 202 222

HERD REST POS STUDY	TEST: 449	SUBJ: N-2	MT: 165.0) G: 10	GP: 1 CELL	
DATA ID		MAX	HIN	Ţi	15	CH
10V EXT PWA CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z (SM) CARRIAGE VEL		10.05 1.36 1.10 11.99 10.59	9.97 -1.27 -0.78 -0.14 -0.05	77.00 3856.00 9856.00 3847.00 3848.00	65.00 3823.00 3832.00 3645.00 3699.00	48 36 31
SERT X SERT Y SERT Z SERT Z (SM) CHEST X		-1.17 1.95 1.51 11.62 10.57 2.06	-25.85 -1.74 -1.45 -0.20 -0.11 -2.70	4191.00 3857.00 3814.00 3854.00 3855.00 3863.00	3817.00 3817.00 3821.00 3711.00 3711.00 3906.00	34 35 53 59
CHEST RES CHEST SI		-0.16 25.03 25.84 47.12	-1.74 -1.01 0.59	4005.00 3684.00 3884.00 3813.00	3891.00 3643.00 3964.00	5 6 7
HERD X HERD T HERD L HERD RES HERD SI HERD HIC		0.60 1.49 12.72 12.73 19.27 16.30	-4.82 -1.24 -0.96 0.78	3647.00 3956.00 3864.00 3864.00 3827.00 3847.00	3938.00 3908.00 3686.00 3623.00 4145.00 3960.00	2 3
LF SHOULDER AT SHOULDER TOTAL SHOULDER TOTAL SHO / WT LF LAP RFIT		67.33 97.66 164.33 1.00	8.29 27.49 36.52 0.22	3892.00 3895.00 3894.00 3894.00	3912.00 4084.00 4078.00 4083.00	16 17
AT LAP BELT TOTAL LAP TOTAL LAP / WT		57.23 76.74 1 33. 68 0.81	11.97 23.50 35.83 0.22	3962.00 3956.00 3956.00 3956.00	4083.00 3859.00 3856.00 3856.00	8
ŘT SEAT LNK X TOTAL SEAT X SERT LNK Y		27.34 2.68 11.47 37.93	-185.63 -128.45 -314.08 -100.08	4118.00 9644.00 4118.00 5973.00	3856.00 3870.00 3870.00 3870.00	1 8 1 9
LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z TOTAL SEAT Z / NT RES SEAT FORCE RES SEAT FORCE / HT LF FOOT X		486.39 495.88 859.35 1832.31	26.59 18.74 26.89 85.76 0.52 86.66	3869.00 3867.00 3867.00 3872.00 3872.00 3872.00 3872.00	3615.00 3615.00 3602.00 3616.00 3616.00 3616.00 3602.00	35 11 12 13
RT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y		11.58 10.58 -8.53 -3.85 96.97	-382,02	3816.00 3814.00 3616.00 3816.00	3862.00 3865.00 3862.00 3862.00	20 23 26
RT FOOT Y CT FOOT T TOTAL FOOT Y LF FOOT 7		34.73	-37.54 -141.24 -29.14 -72.04	3849.00 3816.00 3972.00 5831.00	3824.00 3868.00 3827.00	21 24 27
AT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		192.44 196.57 175.60 477.62 584.78	-7.36 7.24 -57.47 -11.71	3839.00 3872.00 3870.00 3869.00	3823.00 4192.00 3827.00 3800.00	22 25 28

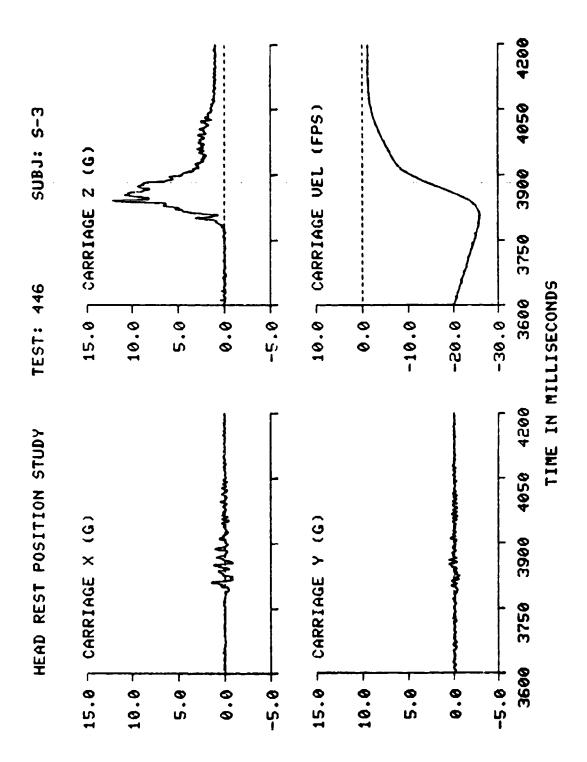
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DATA 10		MAX	HIN	T 1	 T2	CH
LOV EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z CARRIAGE Z (SK)		10.05 1.57 0.93 12.28 10.67	9.97 -1.16 -0.61 -0.28 -0.10	370.00 3904.00 3906.00 3697.00 3898.00	397.00 3912.00 3880.00 3716.00 3714.00	48 96 91 1
CARRIAGE VEL		-1.10	-25.71 -1.49 -1.10 -0.26 -0.16	4164.00 3891.00 3959.00 3905.00	3850.00 3857.00 38924.00 3924.00 3736.00	29 32 33 34
CHEST RES CHEST SI		17.99 42.69	-2.93 -1.89 -1.53 0.78	3921.00 4050.00 3926.00 3926.00 3871.00	3958.00 3946.00 4007.00 3883.00 3993.00	5 6 7
HEAD X HEAD Y HEAD Z HEAD SI HEAD SI HEAD HIC		1.55 1.04 18.09 16.09 31.31 26.94	-9.29 -1.92 -0.79 0.29	3916.00 3989.00 3923.00 3923.00 3873.00 3902.00	3946.00 3960.00 3678.00 41572.00 3952.00	3
LF SHOULDER BT SHOULDER TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT		53.86 87.05 120.77 0.75 97.83	1.73 4.58 8.34 0.05 3.63	3938.00 3937.00 3937.00 4024.00	3972.00 4025.00 3999.00 3999.00	1 6 1 7
RT LAP BELT TOTAL LAP TOTAL LAP / HT LF SEAT LNK X RT SEAT LNK X		48.59 67.36 0.55 6.33 4.47	10.31 14.19 0.09 -183.61 -127.90	4023.00 4023.00 4023.00 4162.00 3794.00	3907.00 3900.00 3900.00 3920.00 3921.00	9 18 19
TOTAL SEAT X SEAT LNK T LF SEAT PAN Z RT SEAT PAN Z CT SEAT PAN Z TOTAL SEAT Z / HT RES SEAT FORCE		1.69 24.68 46.22 614.65 710.25 1788.23 11.10 1815.75	-310.90 -73.37 5.21 6.62 34.53 0.22 35.01	3607.00 4012.00 3920.00 3922.00 3923.00 3922.00 3922.00	3920.00 3922.00 3619.00 3671.00 3619.00 3619.00	95 11 12 13
RES SERI FORCE / HT LF FOOT X RI FOOT X CI FOOT X TOTAL FOOT X LF FOOT Y RI FOOT Y		11.35 -17.21 1.57 -2.52 -19.98 148.56 15.88	0.22 -198.04 -142.06 -196.61 -531.35 -24.39 -150.95	3922.00 4140.00 3865.00 3865.00 3899.00 3958.00	3619.00 3914.00 3916.00 3915.00 3915.00 3983.00	20 23 26 21 24 27
CT FOOT Y TOTAL FOOT Y LF FOOT Z AT FOOT Z CT FOOT Z TOTAL FOOT Z NES FOOT FOOCE		46.54 64.89 234.88 228.10 147.82 469.35 681.36	-34.44 -79.50 5.09 -12.60 -92.50 -12.66 52.05	3897.00 3955.00 3901.00 3904.00 3904.00 3901.00	3922.00 3918.00 3983.00 3980.00 3877.00 3990.00 4144.00	27 22 25 28

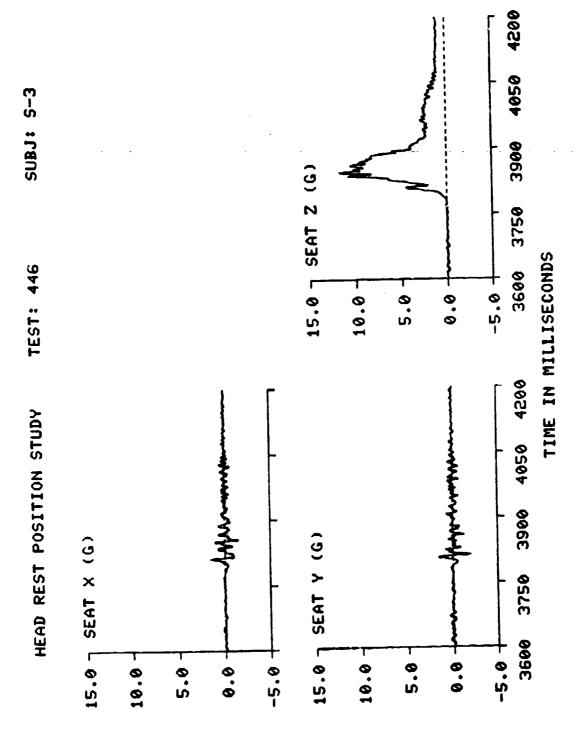
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10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z (SM)		10.05 1.51 1.18 12.35 10.45	9.97 -1.26 -0.69 -0.36	685.00 3863.00 3907.00 3899.00	214.00 3880.00 3857.00 3864.00	31 36 49
CARRIAGE VEL SEAT X SEAT Z SEAT Z SEAT Z (SM) CHEST X		-1.11 1.91 0.58 11.97	-0.08 -25.88 -1.48 -1.02 -0.24 -0.17	3899.00 4188.00 3869.00 3865.00 3905.00	3661.00 3861.00 3882.00 3871.00 3708.00 3709.00	39 39 39 39
CHEST RES CHEST SI HEAD X	`	7.52 0.04 17.51 18.30 37.63 1.42	-2.81 -4.06 -0.83 0.99	3924.00 4002.00 3939.00 3938.00 3867.00	3953.00 3928.00 3770.00 3878.00 3986.00	5 6 7
MERD T MERD Z HERD RES HERD SI MERD HIC LF SHOULDER		1.80 17.32 17.36 27.61 20.55	-1.29 -0.98 0.63	3928.00 3994.00 3916.00 3916.00 3879.00	3974.00 3948.00 3679.00 3672.00 4002.00 3933.00	3 3 2
AT SHOULDER TOTAL SHOULDER TOTAL SHO / HT LF LAP BELT AT LAP BELT		51.56 70.52 109.52 0.76 50.24	8.97 9.97 19.82 0.14 12.35	3937.00 3937.00 3947.00 3947.00 3958.00	3999.00 4049.00 4061.00 4061.00	16 17
TOTAL LAP TOTAL LAP / HT LF SEAT LNK X RT SEAT LNK X		58.63 108.59 0.75 15.98	15.07 27.43 0.19 -205.63	3962.00 3364.00 3964.00 4169.00	3899.D0 3899.D0 3899.O0 3899.OD 3914.D0	16
TOTAL SEAT X SEAT LNK Y LF SEAT PAN Z		2.86 93.47 402.37 382.08	-73.31 -278.94 -71.85	3870.00 3631.00 3989.00	3914.00 3914.00 3920.00	19 35
AT SEAT PAN Z CI SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / HT RES SEAT FORCE / HT RES SEAT FORCE / HT LF FOOT X		382.08 82.08 1598.19 11.02 1622.46 11.19	6.92 0.59 14.33 39.87 0.27 40.09 0.28	3922.00 3915.00 3922.00 3921.00 3921.00	3728.00 3761.00 3709.00 3628.00 3628.00 3628.00	11 12 13
AT FOOT X CT FOOT X TOTAL FOOT X LF FOOT Y BT FOOT Y		8.48 27.81 105.22 136.82 141.78	-160.59 -82.34 -181.21 -420.60 -14.57	3867.00 3867.00 3868.00 3867.00 3901.00	3911.00 3912.00 3912.00 3911.00	26 23 26
CT F001 Y TOTAL F001 Y LF F001 Z		21.90 17.62 48.57 163.18	-112.10 -60.69 -30.39 -48.34	3600.00 3871.00 3888.00 3901.00	3803.00 3910.00 3906.00 3894.00 3860.00	21 24 27
AT FOOT Z CT FOOT Z TOTAL FOOT Z RES FOOT FORCE		182.88 196.73 425.91 585.98	-31.25 -97.72 -156.92 24.96	3911.00 3867.00 3925.00 3925.00	3877.00 3860.00 3860.00 3899.00	22 25 28

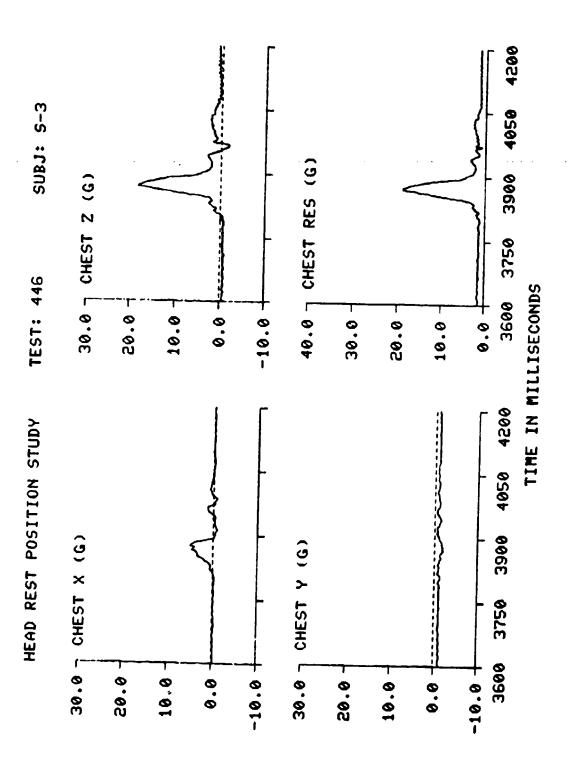
				ur. 170 0	G: 10 GP	, 1 CELL:	F
HEAD REST POS STUDY	TEST: 448	\$U8J:	W13	MIN NIN	11	12	СН
DATA 10			MRX	# 1 m	<u>: -</u>	• •	
			10.05	9.96	234.00 3879.00	190.00 3874.00	48 36
10V EXT PHR CARRIAGE X			0.88	-0.80	3880.00	3996.00 3702.00	3 1 1
CARRIAGE Z			10.46	-0.12	3874.00	3702.00 3821.00	59
CARRIAGE Z (SM) CARRIAGE VEL			1.28	-1.46	3842.00	3873.00 3848.00	32
SERT X SERT Y			12.09	-0.85	3880.00	3708.00 3709.00	34
SERT Z (SM)			10.77 4.24	-1.81	3895.00 3972.00	3931.00 3895.00	5 8
CHEST X CHEST Y			0.08 19.06	-2.73	3900.00	3713.00 3976.00	Ť
CHEST RES			19.49	0.53	3841.00	3971.00 3930.00	2
CHEST SI HERD X			5.11 2.34	0.08	3953.00	3906.00 3713.00	3
HEAD Y HEAD Z			18.37 17.18	1.36	3892.00 3857.00	4198.00 3966.00	
HEAD RES HEAD SI			26.83 21.24		3877.00	3916.00 3998.00	15
HEAD HIC LF SHOULDER			56.50 84.93	1.30 1.47	3911.00	4013.00 4009.00	17
AT SHOULDER TOTAL SHOULDER			120.66	0.03	3912.00 3988.00	4009.00 3885.00	8
TOTAL SHO / HT			34.87 43.82	8.84	3985.00 3987.00	3884.00 3884.00	9
AT LAP BELT			77.76 0.46	19.06	3987.00 4121.00	3884.00 3888.00	18
TOTAL LAP / NT LP SEAT LNK X			1.39 -4.71	-249.57 -181.62	3796.00 4135.00	3895.00 3868.00	19
RT SEAT LNK X TOTAL SEAT X			-12.47	-430.57 -106.10	3988.00	3897.00 3612.00	35 11
SEAT LNK T LF SEAT PAN Z			424.23 518.44	6.79 3.70	3896.00 3857.00	3625.00 3603.00	13
AT SEAT PAN Z CT SEAT PAN Z			999.94	6.55 31.41	3897.00	3600.00 3600.00	
TOTAL SEAT Z / HT			11.35	0.18 50.37	3897.00 3897.00	3600.00 3600.00	
RES SERT FORCE	HT		11.63 8.50	0.30 -138.87	3842.00	3900.00	53 50
LF FOOT X			22.29 84.50	-133.67 -163.25	3842.00	3900.00 3900.00	26
CT FOOT X TOTAL FOOT X			102.96 151.23	-435.80 -24.34	3842.00 3875.00 3738.00	4016.00 3883.00	54 51
EF FOOT Y			27.47 31.27	-151.79 -34.58	4016.00 3861.00	3851.00	27
CT FOOT Y			53.85 228.41	-61.40 -36.11 5.54	3900.00	3833.00 3871.00	22 25 28
LF F001 Z			215.40 198.29	-91.07	3905.00	3852.00	<8
CT FOOT Z			500.8 646.8	7 -78.30 51.36		3989.00	
RES FOOT FORCE							

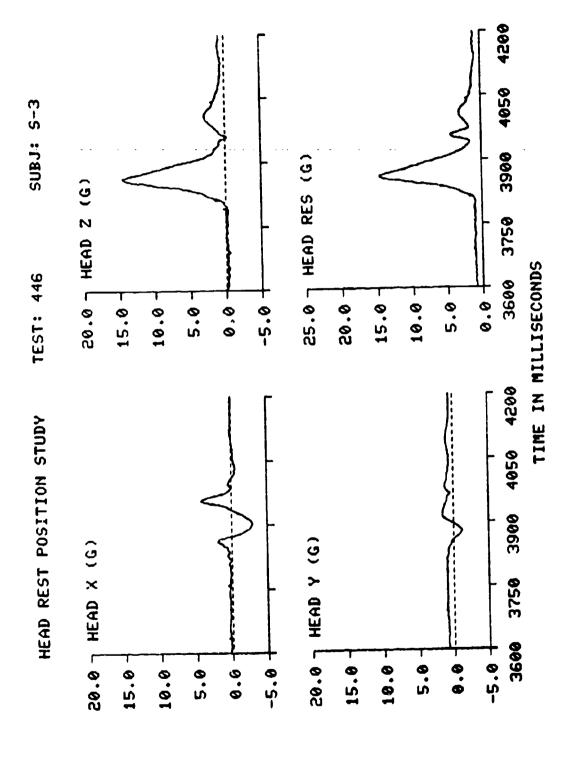
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DRTA 10		HAX	HIN	T 1	15	CH
10V EXT PHR CARRIAGE X CARRIAGE T CARRIAGE Z CARRIAGE Z (SM)		10.05 1.30 1.08 12.12 10.43	9.96 -1.04 -0.56 -0.18 -0.09	283.00 3889.00 3891.00 3881.00 3882.00	245.00 3860.00 3833.00 3630.00 3661.00	48 36 31 1
CARRIAGE VEL SERT X SERT Y SERT Z		-0.90 1.08 1.02 11.52	-25.77 -1.49 -1.20 -0.33	1194.00 3875.00 3849.00 3889.00	3843.00 3863.00 3855.00 3726.00 3710.00	29 32 33 34
CHEST X CHEST Y CHEST Y CHEST RES CHEST SI		4.82 -1.03 14.38 15.02 26.18	-1.27 -3.66 -1.09	3905.00 3960.00 3923.00 3924.00 3847.00	3944.00 3929.00 3713.00 3800.00 3959.00	5 .6 7
MEAD X HEAD Y HEAD Z HEAD RES HEAD SI		3.08 1.03 13.95 14.21 28.22	-1.75 -1.48 -0.40 0.18	3965.00 3988.00 3902.00 3903.00 3851.00	3990.00 3922.00 3988.00 3776.00 4!31.00	2 3 4
HEAD HIC LF SHOULDER BT SHOULDER TOTAL SHOULDER TOTAL SHO / HT		25.85 47.94 46.26 93.66 0.65	17.40 3.02 21.24 0.15	3879.00 3933.00 3931.00 3931.00	3944.00 4057.00 4031.00 4031.00 4031.00	16 17
LF LAP BELT AT LAP BELT TOTAL LAP TOTAL LAP / HT LF SEAT LNK X		39.09 59.29 96.61 0.68 33.17	6.46 16.22 23.00 0.16 -129.73	3963.00 3990.00 3992.00 3992.00	3890.00 3892.00 3891.00 3891.00 3897.00	8 9 18
ĀT SĒAT LNK X TOTAL SEAT X SEAT LNK T LF SEAT PAN Z		13.68 43.55 49.77 275.96 901.67	-69.01 -198.16 -31.95 -3.55 2.09	3953.00 4146.00 3976.00 3898.00 3905.00	3896.00 3896.00 3891.00 3676.00 3640.00	19 35 11
CT SEAT PAN Z TOTAL SEAT Z TOTAL SEAT Z / NT RES SEAT FORCE		864.82 1513.15 10.58 1525.28 10.67	25.66 52.61 0.97 53.41 0.37	3899.00 3898.00 3898.00 3898.00	3604.00 3604.00 3604.00 3604.00	12
RES SERT FORCE / HT LF FOOT X RT FOOT X TOTAL FOOT X		6.35 25.80 52.11 78.97	-164.53 -103.73 -201.01 -462.04	3898.00 3851.00 3850.00 3851.00	3604.00 3901.00 3900.00 3900.00	05 65 85
LF FOOT Y RT FOOT Y CT FOOT Y TOTAL FOOT Y LF FOOT Z		145.82 19.20 20.93 53.04 173.80	-19.27 -125.45 -60.94 -55.79 -11.39	3884.00 3612.00 4005.00 3922.00 3885.00	4056.00 3900.00 3894.00 3912.00 3839.00	21 27 22
AT FOOT Z CT FOOT Z TOTAL FOOT Z BES FOOT FORCE		198.83 136.97 442.15 634.53	-3.96 -85.72 -73.68 39.90	3900.00 3892.00 3892.00 5901.00	3707.00 3862.00 3838.00 4170.00	22 28 28

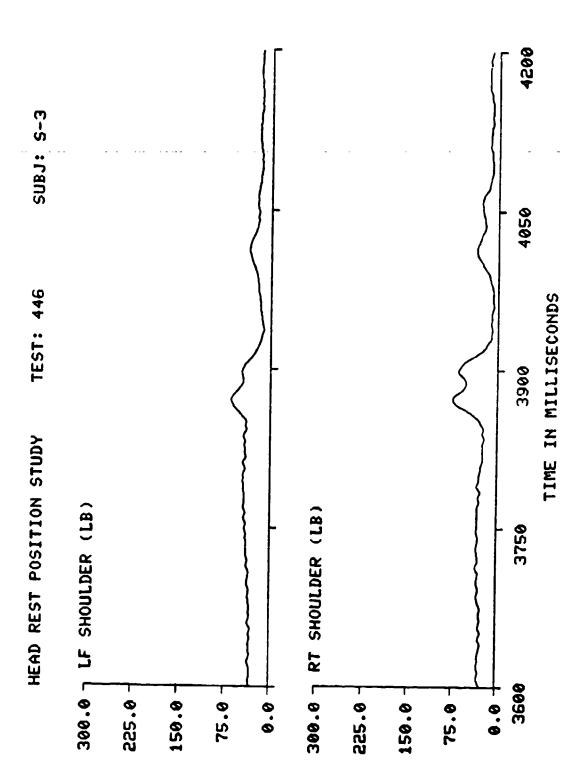
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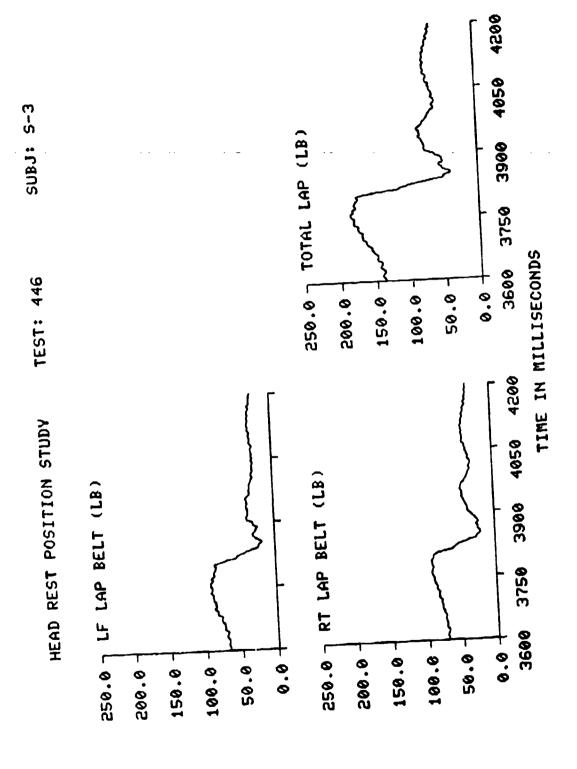


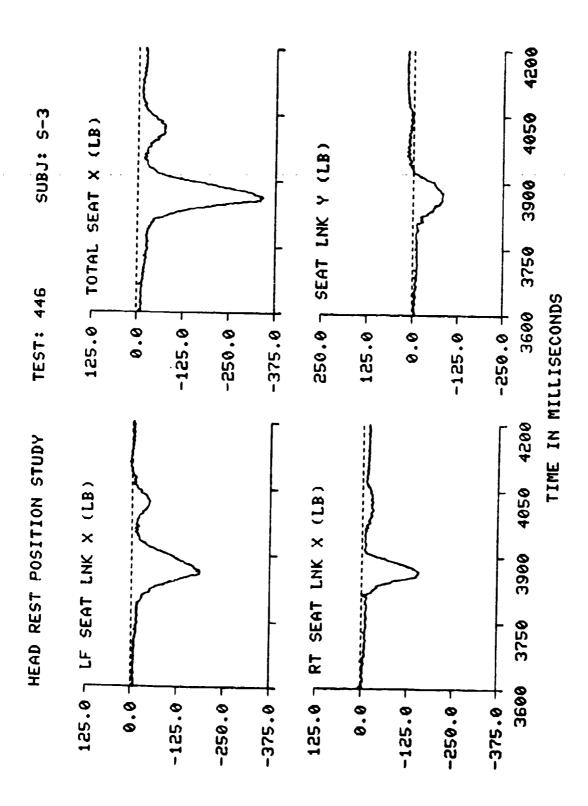




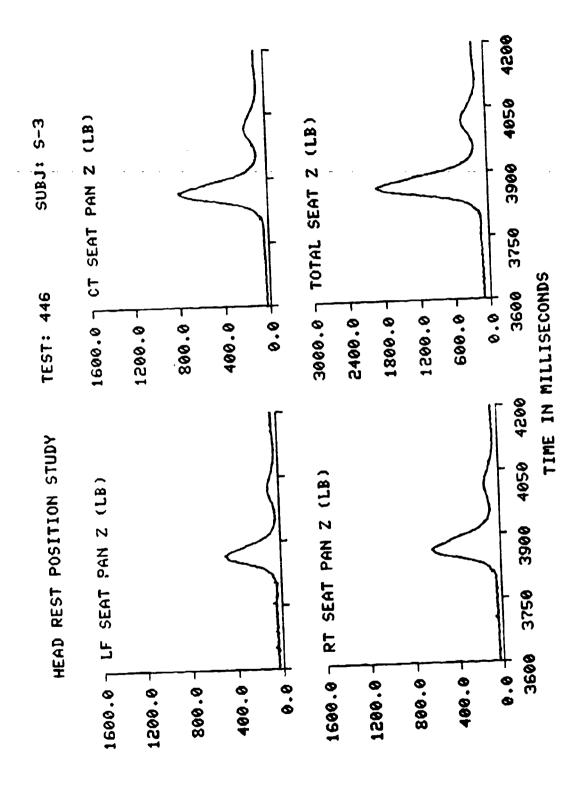


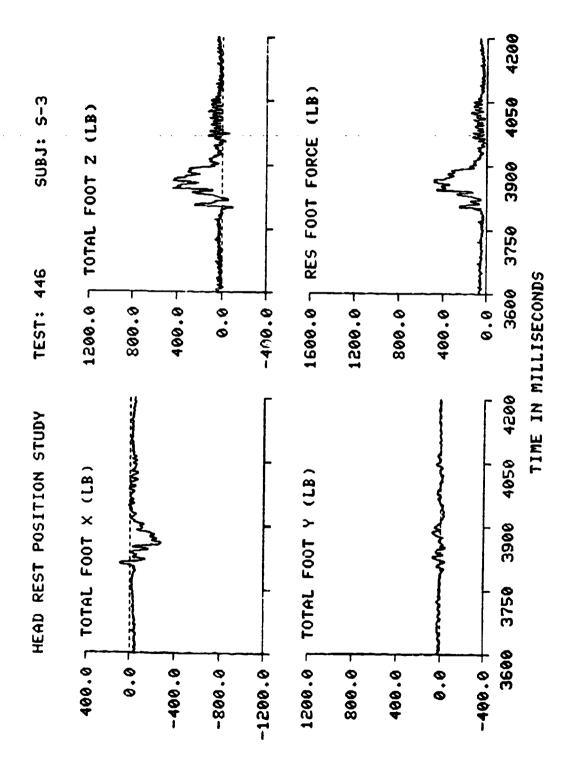






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APPENDIX C

WILCOXON ANALYSES

The electronic data from this test program were analyzed by means of the Wilcoxon paired-replicate rank test (Wilcoxon & Wilcox, 1964). A total of seven comparisons were made by this technique. The means and estimated standard deviations of each parameter in each comparison are summarized in Tables C-1 through C-7. Since the number of comparable tests in one comparison may be different from the number of comparable tests in another comparison, minor variations in the means and standard deviations in a cell of the test matrix may be noted among these tables. An asterisk designates a statistically significant trend in a parameter at the 90% confidence level for a two-tailed test. The statistically significant trends in these comparisons are summarized in the body of the report in Tables 5, 10, and 12.

The Wilcoxon analyses of parameters for which there were statistically significant differences are also presented. In these computations, the arithmetic difference between the parameter means from each condition is first computed. These differences are then rank ordered from smallest to largest, without regard to sign. An integer from 1 to n, where n is the number of pairs in the comparison, is assigned to each difference so that the smallest difference receives the rank 1 and the largest difference receives the rank n. Then, the rank integer is given the same sign as the sign of the arithmetic difference to which it corresponds. The negative integers are summed and the positive integers are summed. Finally, if either sum is greater than or equal to the critical integer sum for the specified confidence level, then the means may be considered significantly different (i.e., from two different samples).

A complete set of Wilcoxon computations for all comparisons in this test program will be maintained by the Biomechanical Protection Branch of AFAMRL until this work unit is retired. These data will eventually be recorded in a permanent data bank within the Laboratory.

TABLE C-1
COMPARISON A-B

(Peak values are tabulated for velocity, accelerations and loads.)

(n = 14) ···

CELL MATRIX RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	A MODIFIED F-111 HANDS-ON-KNEES FORWARD		MODIFIE HANDS-(Significant at 90% Confidence	
CARRIAGE ACCELERATION (G) CARRIAGE VELOCITY (ft/sec) SEAT ACCELERATION (G) CHEST ACCELERATION (G)	Mean 10.6 -25.7 10.6	St Dev 0.18 0.13 0.18	Mean 10.5 -25.7 10.6	St Dev 0.11 0.12 0.18	
-X axis +X axis +Z axis Resultant CHEST SEVERITY INDEX	-1.55 4.29 18.3 18.7 31.1	0.75 1.66 4.14 3.97 6.86	-1.45 4.21 19.5 19.8 34.1	0.80 1.46 4.23 4.11	*
HEAD ACCELERATION (G) -X axis +X axis +Z axis	-4.70 1.04 13.1	1.02 0.95 1.03	-2.04 1.97 13.1	6.84 1.29 1.16 0.98	*
Resultant HEAD SEVERITY INDEX STRAP LOADS (1b) Reflection Straps	13.3 19.7 95	1.04 2.15	13.3 20.2 94	0.92 2.14	
Inertia Reel Straps Total Shoulder Straps Total Lap Belt Crotch Strap SEAT PAN LOADS (1b)	95 181 106 96	29 54 23 60	81 165 99 112	24 48 24 81	*
-X axis +Z axis Resultant FOOTREST LOADS (1b)	-263 1640 1660	69 235 238	-250 1640 1660	72 207 210	
-X axis +Z axis Resultant	-536 541 710	149 82 165	-525 545 719	163 82 161	

TABLE C-2 COMPARISON C-D

(Peak values are tabulated for velocity, accelerations and loads.)

(n = 13)

	ν'	. 10,			
CELL MATRIX RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	C MODIFIE HANDS- FORW		O MODIFIE HANDS-1 AFT	IN-LAP	Significant at 90% Confidence
CARRIAGE ACCELERATION (G) CARRIAGE VELOCITY (ft/sec) SEAT ACCELERATION (G)	Mean 10.5 -25.8 10.6	St Dev 0.12 0.17 0.14	Mean 10.6 -25.7 10.6	St Dev 0.13 0.14 0.16	*
CHEST ACCELERATION (G) -X axis +X axis +7 axis Resultant CHEST SEVERITY INDEX	-2.17 4.32 20.3 20.6 35.4	0.95 1.23 2.96 2.89 6.15	-2.06 3.82 18.7 19.0 32.9	0.93 1.25 3.51 3.50 7.09	
HEAD ACCELERATION (G) -X axis +X axis +I axis Resultant HEAD SEVERITY INDEX	-4.90 1.14 13.3 13.4 19.6	0.95 0.92 0.92 0.92 2.24	-2.08 2.44 12.7 13.0 20.3	1.57 1.02 0.88 0.98 1.43	* *
STRAP LOADS (1b) Reflection Straps Inertia Reel Straps Total Shoulder Straps Total Lap Belt Crotch Strap	103 110 205 89 104	26 29 56 25 73	107 101 203 96 130	20 18 37 16 62	
SEAT PAN LOADS (1b) -X axis +Z axis Resultant FOOTREST LOADS (1b)	-285 1720 1740	73 223 226	-265 1690 1710	64 206 209 88	*
-X axis +Z axis Resultant	-364 452 528	91 60 91	-390 477 580	72 102	*

TABLE C-3

COMPARISON E-F

(Peak values are tabulated for velocity, accelerations and loads.)

(n = 12)

CELL MATRIX RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	E CONVENTIONAL HANDS-IN-LAP FORWARD		F CONVENTIONAL HANDS-IN-LAP AFT		Significant at 90% Confidence
CARRIAGE ACCELERATION (G) CARRIAGE VELOCITY (ft/sec) SEAT ACCELERATION (G)		St Dev 0.16 0.13 0.14	Mean 10.5 -25.7 10.7	0.11	
CHEST ACCELERATION (G) -X axis +X axis +Z axis	-2.37 3.89 20.6	1.49 3.12	-1.86 4.95 19.5 19.9	0.97 1.62 2.83 2.71	*
Resultant CHEST SEVERITY INDEX HEAD ACCELERATION (G) -X axis	20.8 41.9 -4.43	6.48 1.18	40.8 -2.63	5.47 1.66	*
+X axis +Z axis Resultant HEAD SEVERITY INDEX	14.8	1.42		1.55	*
STRAP LOADS (1b) Reflection Straps † Inertia Reel Straps †					
Total Shoulder Straps Total Lap Belt Crotch Strap † SEAT PAN LOADS (15)	144 107	39 24	137 116	33 27	
-X axis +Z axis Resultant FOOTREST LOADS (1b)	-324 1830 1860	76 254 259	-308 1790 1820	63 282 284	
-X axis +Z axis Resultant	-444 488 629	118 72 120	-430 473 603	100 59 94	

 $[\]mbox{t\ No\ comparison}$ is possible, since the conventional harness does not have reflection straps or a crotch strap.

TABLE C-4
COMPARISON A-C

. . (Peak values are tabulated for velocity, accelerations and loads.)

(n = 14)

CELL MATRIX RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	A MODIFIED F-111 HANDS-ON-KNEES FORWARD		MODIFIE HANDS- FOR	Significant at 90% Confidence	
CARRIAGE ACCELERATION (G) CARRIAGE VELOCITY (ft/sec) SEAT ACCELERATION (G) CHEST ACCELERATION (G)	Mean 10.6 -25.7 10.6	St Dev 0.18 0.13 0.18	Mean 10.5 -25.8 10.6	St Dev 0.13 0.16 0.14	*
-X axis +X axis	-1.56 4.29	0.75 1.66	-2.08 4.47	0.97 1.30	*
+Z axis Resultant	18.3 18.7	4.14 3.97	20.0 20.4	3.02 2. 91	*
CHEST SEVERITY INDEX HEAD ACCELERATION (G)	31.1	6.86	35.2	5.94	*
-X axis +X axis +Z axis Resultant	-4.70 1.04 13.1 13.3	1.02 0.95 1.03 1.04	-4.83 1.25 13.2 13.4	0.95 0.98 0.92 0.92	
HEAD SEVERITY INDEX STRAP LOADS (1b)	19.7	2.15	19.7	2.20	
Reflection Straps Inertia Reel Straps Total Shoulder Straps Total Lap Belt Crotch Strap	95 95 181 106 96	23 29 54 23 60	104 112 206 92 106	25 28 54 27 70	*
SEAT PAN LOADS (1b) -X axis	-263	69	-285	70	*
+Z axis Resultant FOOTREST LOADS (1b)	1640 1660	235 238	1730 1760	220 222	*
-X axis +Z axis Resultant	-536 541 710	149 82 165	-387 465 551	121 74 121	* * *

TABLE C-5
COMPARISON B-D

(Peak values are tabulated for velocity, accelerations and loads.)

(n = 13)

CELL MATRIX RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	B MODIFIED F-111 HANDS-ON-KNEES AFT		MODIFIE HANDS- AF	Significant at 90% Confidence	
CARRIAGE ACCELERATION (G) CARRIAGE VELOCITY (ft/sec) SEAT ACCELERATION (G) CHEST ACCELERATION (G)	-25.7 10.7	0.12 0.10	10.6 -25.7 10.6	0.13 0.14 0.16	
-X axis +X axis +Z axis Resultant CHEST SEVERITY INDEX HEAD ACCELERATION (G)	-1.51 3.96 19.6 19.9 34.1		-2.06 3.82 18.7 19.0 32.9	0.93 1.25 3.51 3.50 7.09	*
-X axis +X axis +Z axis Resultant HEAD SEVERITY INDEX STRAP LOADS (1b)	-1.91 1.94 13.2 13.5 20.2	1.23 1.20 0.90 0.83 2.21	-2.08 2.44 12.7 13.0 20.3	1.57 1.02 0.88 0.98 1.43	* *
Reflection Straps Inertia Reel Straps Total Shoulder Straps Total Lap Belt Crotch Strap	91 77 158 98 101	19 20 42 24 74	107 101 203 96 130	20 18 37 16 62	* * *
SEAT PAN LOADS (1b) -X axis +2 axis Resultant FOOTREST LOADS (1b)	-247 1620 1640	74 201 204	-265 1690 1710	64 206 209	* *
-X axis +Z axis Resultant	-508 538 701	156 81 154	-390 477 580	88 72 1 02	* * *

TABLE C-6
COMPARISON C-E

(Peak values are tabulated for velocity, accelerations and loads.)

(n = 13)

CELL MATRIX RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	C MODIFIED F-111 HANDS-IN-LAP FORWARD			Significant at 90% Confidence	
CARRIAGE ACCELERATION (G) CARRIAGE VELOCITY (ft/sec) SEAT ACCELERATION (G) CHEST ACCELERATION (G) -X axis +X axis	Mean 10.5 -25.8 10.6 -2.17 4.32		Mean 10.5 -25.8 10.6 -2.28 3.93	St Dev 0.16 0.14 0.17 0.94 1.43	
+Z axis Resultant CHEST SEVERITY INDEX HEAD ACCELERATION (G) -X axis	20.3 20.6 35.4 ~4.90	2.96 2.89 6.15	20.2 20.5 41.1 -4.44	3.31 3.23 6.75	*
+X axis +Z axis Resultant HEAD SEVERITY INDEX STRAP LOADS (1b)	13.3	0.92 0.92 0.92 2.24	1.56 14.7 15.0 24.3	1.32	* * *
Total Lap Belt Crotch Strap †	205 89	56 25	146 108	39 23	*
SEAT PAN LOADS (1b) -X axis +Z axis Resultant FOOTREST LOADS (1b)	1740	73 223 226	-319 1820 1850	75 247 253	* * *
-X axis +Z axis Resultant	-364 452 528	91 60 91	-430 476 609	123 81 136	*

 $[\]dagger$ No comparison is possible, since the F/FB-111 harness has reflection straps and a crotch strap and the conventional harness does not.

TABLE C-7
COMPARISON D-F

(Peak values are tabulated for velocity, accelerations and loads.)

(n = 12)

CELL MATRIX RESTRAINT HARNESS BRACING POSITION HEADREST POSITION	MODIFIE	IN-LAP	F CON VENT HAN DS – I AF	IONAL N-LAP	Significant at 90% Confidence
CARRIAGE ACCELERATION (G) CARRIAGE VELOCITY (ft/sec) SEAT ACCELERATION (G) CHEST ACCELERATION (G)	10.6	0.16	10.7	0.11 0.15 0.10	
-X axis +X axis +Z axis Resultant	3.70 18.5	3.61	-1.86 4.95 19.5 19.9	1.62 2.83 2.71	*
CHEST SEVERITY INDEX HEAD ACCELERATION (G) -X axis +X axis	-1.99 2.40	7.25 1.60 1.05	2.62	1.66 1.76	*
+Z axis Resultant HEAD SEVERITY INDEX STRAP LOADS (1b)	12.8 13.1 20.3		14.8 15.1 26.7	1.44 1.55 3.12	* * *
Reflection Straps † Inertia Reel Straps † Total Shoulder Straps Total Lap Belt	203 96	38 17	137 116	33 28	* *
Crotch Strap † SEAT PAN LOADS (1b) -X axis +Z axis Resultant	-268 1700 1720	67 212 214	-308 1790 1820	63 282 284	* *
FOOTREST LOADS (1b) -X axis +Z axis Resultant	-398 483 593	87 71 95	-430 473 603	100 59 94	

 $[\]dagger$ No comparison is possible, since the F/FB-111 harness has reflection straps and a crotch strap and the conventional harness does not.

DESCRIPTION OF WILCOXON ANALYSIS

A VAL is the value of the parameter in the test condition designated by FUNCTION A. B VAL is the value of the parameter in the test condition designated by FUNCTION B. A-B is the arithmetic difference between A VAL and B VAL.

The differences, A-B, are then rank ordered from smallest to largest without regard to sign. The negative differences are listed under ORD- and the positive differences are listed under ORD+.

N is the integer corresponding to the rank ordered difference, A-B, without regard to sign. N- is the integer which corresponds to a negative difference and N+ is the integer which corresponds to a positive difference.

WILCOXON ANALYSIS

ANALYSIS	OF:	CHEST	SI					
FUNCTION FUNCTION			CELL:				1AX 1AX	
5 UBJ	R VAL	8 VAL	A-8	ORO -	080 +	N	N -	N +
D-1 G-3 H10 H-2 R-1 F-3 K-1 S-3 H11 R-3 F-2 G-2	38.23 29.17 31.60 32.67 43.49 29.1 30.37	44.10 34.10 37.98 31.60 45.04 41.60 36.92 27.82 38.01	0.26 -1.27 -5.87 -5.87 -4.38 -6.07 -1.55 -1.55 -5.50 -5.64 -5.64 -6.29	0.00 0.00 -1.29 -1.55 -1.75 0.00 -4.93 0.50 -5.64 -5.87 -6.38 -11.76		1.00 2.00 3.00 4.00 5.00 7.00 9.00 10.00 11.00 12.00 14.00	0.00 3.00 4.00 5.00 7.00 9.00 10.00 11.00 12.00 13.00	1.00 0.00 0.00 0.00 6.00 0.00 0.00 0.00
MEAN A: MEAN B:	31.14 34.11	STO DEV		6.84 6.84	SUN OF N SUN OF N	PLUS :	88.00 DIFFEREN	17.00

WILCOXON ANALYSIS

ANALYSIS OF: HEAD X	
FUNCTION A • G: 10 CELL: A FUNCTION B • G: 10 CELL: B	MAX MAX
	ORD + N N - N +
H-2 2.59 3.93 -1.34 -0.67 R-1 1.75 2.38 -0.63 -0.74 F-3 1.34 3.10 -1.76 -0.79	0.00 1.00 1.00 0.00 0.59 2.00 0.00 2.00 0.00 3.00 3.00 0.00 0.00 4.00 4.00 0.00 0.00 5.00 5.00 0.00 0.00 6.00 6.00 0.00 0.00 7.00 7.00 0.00 0.00 8.00 8.00 0.00 0.00 9.00 9.00 0.00 0.00 10.00 10.00 0.00 0.00 11.00 11.00 0.00 0.00 12.00 0.00 0.00 13.00 13.00 0.00 0.00 14.00 14.00 0.00
MERN A: 1.04 STD DEV A: 0.95 MERN 8: 1.97 STD DEV B: 1.16	
	HHM SIGNIFICANT DIFFERENCE HHH
WILCOXON RHALYSIS	
ANALYSIS OF: HEAD X	
FUNCTION A - G: 10 CELL: A FUNCTION B - G: 10 CELL: B	MIN MIN
SUBJ A VAL 0 YAL A-8 0A0 -	080 + N N - N +
0-1 -4.35 -1.29 -3.06 -1.51 G-3 -5.71 -3.12 -2.59 -1.75 M10 -2.58 -0.08 -2.50 -2.04 H-2 -3.90 -1.86 -2.04 -2.40 R-1 -5.36 -3.85 -1.51 -2.41 F-9 -3.29 -0.35 -2.94 -2.50 K-1 -6.52 -4.77 -1.75 -2.59 S-9 -4.47 -2.07 -2.40 -2.74 M19 -4.67 -1.37 -3.30 -2.94 M11 -4.66 -1.64 -3.02 -3.02 R-9 -5.46 -3.05 -2.41 -3.06 F-2 -4.69 -1.95 -2.74 -3.30 R-2 -5.59 -2.07 -3.52 -3.45 G-2 -4.60 -1.15 -3.45 -3.52	0.00 1.00 1.00 0.00 9.00 2.00 2.00 0.00 0.00 3.00 3.00 0.00 0.00 4.00 4.00 0.00 0.00 5.00 5.00 0.00 0.00 6.00 6.00 0.00 0.00 7.00 7.00 0.00 0.00 8.00 8.00 0.00 0.00 9.00 9.00 0.00 0.00 19.00 9.00 0.00 0.00 17.00 11.00 0.00 0.00 12.00 12.00 0.00 0.00 13.00 12.00 0.00 0.00 13.00 13.00 0.00 0.00 14.00 14.00 0.00
MEAN A: -4.70 STO DEV A: 1.02 MEAN B: -2.04 STO DEV B: 1.29	SUM OF N MANUS: 105.00 SUM OF N PLYS: 0.00

WILCOXON ANALYSIS

RNRLTSIS	Ofi	TOTAL SHL	D REEL		
FUNCTION FUNCTION	R - G:		L: A L: B		MAX MAX
SUBJ 0-1 G-3 MJO- N-2 R-1 F-3 K-1 S-9 MJ3 H13 H13 F-2	56.47 99.70 153.36 180.98 54.44 111.94 53.54 10.66 89.03 73.93	B VAL A- 69.16 18. 98.73 5. 60.59 -4. 77.28 22. 127.97 25. 99.32 31. 68.04 -13. 106.66 5. 86.10 -32. 96.67 13. 37.31 51. 77.97 -4.	-4.04 -4.04 -7.12 0.00 12 0.00 13 0.00 13.60 0.00 0.	080 + N 0.00 1.00 0.00 2.00 5.25 3.00 5.28 4.00 0.00 5.00 13.98 6.00 13.98 6.00 13.98 6.00 22.42 8.00 22.42 8.00 25.39 9.00 31.56 10.00 0.00 11.00 32.95 12.00	2.00 0.00 0.00 3.00 0.00 4.00 5.00 0.00 0.00 6.00 0.00 7.00 0.00 8.00 0.00 9.00 0.00 10.00 11.00 0.00 0.00 12.00
B-5	106.49 93.86	62.66 43. 60.91 32.	83 0.00 95 0.00	43.83 13.00 51.72 14.00	
MERN A: MERN B:	94.71 80.67	STO DEV A: STO DEV B:	28.89 23.50	SUM OF N NINUS: SUM OF N PLUS:	19.00 86.00
				HEN STOUTE TOHU	T DIFFERENCE HWW

WILCOXON ANALYSIS

ANALYSIS	OF:	CARRIAG	EZ (SM	3				
FUNCTION FUNCTION			ELL: C				IRX IRX	
SUBJ	A VAL		A-B	ORO -	ORD +	N	N -	N +
S-3 G-3 R-3 D-2 F-3 H11 F-2 H10 H13 H-2 K-1	10.37 10.39 10.41 10.51 10.66 10.45 10.39 10.52 10.56 10.43 10.69	10.60 10.47 10.81 10.61 10.70 10.50 10.50 10.50 10.50 10.50 10.50	0.23 0.08 0.40 0.10 0.10 0.17 0.17 0.13 0.04 0.07 0.07	0.00 -0.04 -0.07 -0.08 -0.10 -0.11 -0.13 -0.17 -0.23 -0.35 -0.40	0.02 0.00 0.00 0.00 0.00 0.00 0.00 0.00	1.00 2.50 2.50 9.00 5.00 6.00 7.00 8.00 10.00 11.00 12.00	0.00 2.50 2.50 4.00 5.00 6.00 7.00 8.00 9.00 10.00 13.00	1.0C 0.00 0.00 0.00 0.00 0.00 0.00 0.00
MEAN A: MEAN B:	10.50 10.61	STO DEV A		.12	SUM OF N SUM OF N		79.00 DIFFERE	12.00 NCE MMM

.

ANALYSIS	0F:	HEAD	x					
FUNCTION FUNCTION		10 10	CELL: C				HIN Hin	
SUBJ S-3 G-3 R-3 O-1 G-2 F-3 H11 F-2 H10 H13 H-2 K-1	A VAL -4.02 -6.27 -5.39 -4.62 -3.93 -3.93 -3.47 -3.38 -5.99 -6.03	-0.47 -3.24 -3.17 -1.19 -1.97 -0.27 -0.83 -2.77 -1.13 -0.18 -4.15 -5.14 -2.52	A-B -3.55 -3.03 -2.22 -3.43 -3.68 -3.10 -1.30 -1.89 -1.89	-0.89 -1.70 -1.84 -1.97 -2.22 -2.30 -3.03 -3.10 -3.43 -3.55 -3.68 -3.78 -5.20	0RD + 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	N 2.00 3.00 4.00 5.00 6.00 7.00 9.00 10.00 11.00 12.00	N - 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00	N +
MEAN A: MEAN B:	-4.90 -2.0P	STO DEV		0.95 1.57	SUM OF N SUM OF N		91.00 -	0.00

WILCOXON ANALYSIS

ANALYSIS	OF:	HERD	X					
FUNCTION FUNCTION		10 10	CELL: C				MAX MAX	
SUBJ	A VAL	8 VAL	A-B	ORD -	ORD +	N	N -	N +
5-3 G-3 D-1 G-2 F-3 H11 F-2 H10 H13 H-2 K-1	2.17 0.65 0.70 0.09 0.54 0.56 2.77 1.95 2.09 0.32 2.16 0.53	3.29 2.59 2.87 1.93 1.08 3.65 3.43 2.73 3.94 1.51 0.97	-1.12 -2.17 -2.17 -1.84 -0.54 -0.65 -0.63 -0.63 -0.44 -0.86	-0.44 -0.54 -0.55 -0.64 0.00 -0.66 -0.86 -1.64 -1.94 -2.17 -3.09 -3.62	0.00 0.00 0.00 0.85 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.09 7.00 8.00 9.00 10.00 12.00 13.00	1.00 2.00 3.00 4.00 0.00 6.00 7.00 9.00 10.00 11.00 12.00	000000000000000000000000000000000000000
MEAN A: MEAN B:	1.14	STO DEV		0.92 1.02	SUN OF N	MINUS: PLUS :	86.00	5.00

MEAN A: -284.52 MEAN B: -265.4P

MICCORO		- -						
ANALYSI	S OF:	HEAD	2					
FUNCTION FUNCTION	N A = G: N B = G:	10 10	CELL: C			i	IRX IRX	
ŞUBJ	A VAL	B VAL	A-B	080 -	ORD +	N	N -	N +
S-3 R-3 R-1 C-3 F-1 F-1 H12 H13 K-1 R-2	13.69 13.02 13.32 13.74 12.39 13.56 12.89 14.62 14.37 13.15 11.31 12.31	13.34 11.85 11.91 12.47 12.56 12.25 14.40 13.41 14.19 12.99 11.82 11.77 12.55	0.35 1.17 1.41 1.27 -0.27 1.31 -1.51 0.18 0.16 -0.51 0.54	0.00 0.00 -0.27 0.00 -0.51 0.00 0.00 0.00 0.00 -1.51	0.16 0.18 0.00 0.35 0.00 0.54 1.17 1.21 1.27 1.31 1.41 0.00 1.66	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 3.00 5.00 0.00 0.00 0.00 0.00 0.00	1.00 2.00 0.00 9.00 10.00 11.00 0.00
MEAN A: MEAN B:	13.28 12.74	STD DE	V A: V 3:	0.92 0.88	SUM OF N	MINUS: PLUS :	20.00	71.00
	N ANALYSI	•			HHH SIG	NII ICHNI	שורדכחכו	VCC WAR
		TOTA						
FUNCTIO	N A = G: N B = G:	10 10	CELL: C				(IN (IN	
SUBJ	A VAL	8 VAL	A-B	0R0 -	0R0 +	N	N -	N +
S-3 R-3 D-1 G-2 F-3 M11 F-2 H10 M13	-311.47 -279.54 -213.48 -265.36 -163.13 -300.22 -330.65 -395.60 -266.53	-312.67 -229.75 -234.37 -234.66 -157.80 -238.38 -305.53 -332.76 -268.71	1.20 -49.79 20.89 -30.70 -5.33 -61.84 -25.12 -62.84 -24.43	0.00 -5.33 -5.85 0.00 0.00 0.00 -25.12 -30.70 -32.02 -34.37	080 + 1.20 0.00 0.00 13.85 20.89 24.43 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00	0.00 2.00 3.00 0.00 0.00 7.00 8.00 9.00	1.00 0.00 0.00 4.00 5.00 6.00 0.00 0.00

SUM OF N MINUS: SUM OF N PLUS: 16.00

MMM SIGNIFICANT DIFFERENCE MMM

75.00

72.77 64.49

STO DEV A: STO DEV B:

ANALYS1:	5 OF:	AES	FOOT FOR	RCE				
FUNCT 101	N A = G: N B = G:	10 10	CELL:	C O			ABS ABS	
SUBJ	A VAL	B VAL	A-8	ORD -	ORD +	N	N	N +
5-3 G-3 R-3 D-1 F-2 H10 M13 K-1 R-2	482.06 464.89 481.05 765.67 395.06 515.42 504.75 616.31 515.64 570.14 570.14 504.29 585.77	554.77 528.17 425.05 764.08 444.92 713.18 607.72 541.15 702.67 644.02 563.98	-72.71 -63.28 56.00 1.59 -49.86 -25.43 -25.51 -25.51 -132.53 -139.66 -53.47 21.79	0.00 0.00 0.00 -25.43 -25.51 -49.86 -53.26 -72.71 -132.53 -139.66 -148.45	1.59 8.59 21.79 0.00 0.00 0.00 0.00 0.00 0.00	1.00 3.00 3.00 4.00 5.00 6.00 7.00 8.00 10.00 11.00 12.00 13.00	N - 0.00 0.00 0.00 5.00 6.00 7.00 0.00 12.00 12.00 13.00	1.00
MEAN A: MEAN B:	528.42 580.18	STO DE	/ A: :	91.44 02.04	SUM OF N	MINUS: PLUS:	77.00	14.00
HILCOXUN	ANALYSIS				NNN SIG	NIFICANT	DIFFEREN	iCE HHH
		CHEST						
FUNCTION	8 • G:	10 10	CELL: E				MRX MAX	
SNB1	A VAL	B VAL	A-B	ORD -	ORD +	N	N -	N +
S-3 K-1 D-1	3.26 5.61	5.06	-1.80	0.00				• •
R-2 F-3 G-2 F-2 M11 M13 M-2 G-3 M10	5.70 2.58 2.87 4.61 3.21 4.89 2.83 0.93 5.51 4.62	6.50 4.82 5.08 5.73 6.67 3.74 4.24 2.06 2.55 7.52	0.17 -0.80 -2.24 -2.21 -1.12 -3.46 1.15 -1.41 -1.19 -2.90	-0.80 -1.12 -1.13 0.00 -1.41 -1.80 -2.21 -2.24 -2.90 0.00 -3.46	0.17 0.00 0.00 0.00 1.15 0.00 0.00 0.00 2.96 0.00	1.00 2.00 3.00 4.00 5.00 5.00 7.00 8.00 12.00	2.00 3.00 4.00 5.00 7.00 8.00 9.00	1.00 0.00 0.00 0.00 5.00 0.00 0.00 0.00

WILCOXON RNRLY515

ANALYSIS	OF:	HERD X			
FUNCTION FUNCTION	A = G: B = G:	10 CE	ELL: E ELL: F		MIN MIN
	A VAL	B VAL	A-B ORD -	ORD + N	N - N + 0.00 1.00 0.00 2.00 3.00 0.00 4.00 0.00 5.00 0.00 6.00 0.00 7.00 0.00 8.00 0.00 9.00 0.00 10.00 0.00 11.00 0.00
5-3 K-1	-2.25 -6.40	-2.95 -4.54	0.70 0.00 1.86 0.00	0.22 1.00 0.70 2.00	0.00 1.00 0.00 2.00
D-1 R-2	-4.56 -4.91	-0.16 -1 -1.75 -3	4.40 -0.75 3.16 -1.13	0.00 3.00 0.00 4.00	3.00 0.00 4.00 0.00
F-3 G-2	-3.43 -4.78	-0.01 -3 -3.45 -3	3.42 -1.26 1.33 -1.33	0.00 5.00 0.00 6.00	5.00 0.00 6.00 0.00
5-3 K-1 D-1 R-2 F-2 F-2 H11 H13 K-2 G-3 H10	-4.42 -4.42	-3.29 -: -0.61 -:	1.13 -1.86 3.76 -3.16	0.00 7.00 0.00 8.00 0.00 9.00	8.00 0.00 9.00 0.00
M-2 G-3	-5.57 -5.58	-4.82 -(-4.32 -)	0.75 -3.42 1.26 -3.76	0.00 10.00 0.00 11.00	10.00 0.00 11.00 0.00
M10	-2.79	-3.01	0.22 -4.40	0.00 12.00	12.00 0.00
MEAN A:	-4.43	STO DEV A	: 1.18	SUN OF N HINUS: SUN OF N PLUS:	75.00
HEAR U.	-2.03	310 024 0			DIFFERENCE NAM
MILCOXON	ANALYSIS	i -			
		HEAD SI			
FUNCTIC FUNCTION	B • C:	10 C	ELL: E ELL: F		ABS ABS
SUBJ	A VAL	B VAL	R-8 ORD ~	0A0 + N	N - N +
S-3 K-1	25.14 23.50	29.53 - 1 24.49 - 1	4.39 0.00 0.99 -0.32	0.03 1.00 0.00 2.00	0.00 1.00 2.00 0.00
D-1 R-2	25.91 23.65	25.33 28.22 ~	0.58 -0.58 4.57 0.00	0.00 3.50 0.58 3.50	3.50 0.00 0.00 3.50
F-3 G-2	24.80	28.26 ~ 27.72 ~	3.46 -0.99 4.64 -3.22 5.83 -3.85	0.00 5.00 0.00 6.00	5.00 0.00 6.00 0.00
M11 M13	21.16	31.31 -10 26.83 -1	0.15 -4.39 0.32 -4.57	0.00 8.00 0.00 9.00	8.00 0.00 9.00 0.00
H-2 G-3	18.69 24.25	19.27 - 27.47 -	0.58 -4.64 3.22 0.00	0.00 10.00 5.43 11.00	10.00 0.00 0.00 11.00
M10	27.64	27.61	0.03 -10.15	0.00 12.00	N - N + 0.00 1.00 2.00 0.00 3.50 0.00 0.00 3.50 5.00 0.00 7.00 0.00 8.00 0.00 9.00 0.00 10.00 0.00 12.00 0.00
				SUM OF N MINUS: SUM OF N PLUS :	

MMM SIGNIFICANT DIFFERENCE MAM

RNALYSIS	OFi	CARRI	RGE VEL					
FUNCTION FUNCTION	A = G:	10 10	CELL: A			1	MIN MIN	
SUBJ	A VAL	B YAL	N-B	ORD -	0R0 +	N	н -	N +
0-1 M10 M10 K-1 F-2 M11 G-3 S-3 M13 M-2 F-3	-25.61 -25.58 -25.54 -25.77 -25.72 -25.45 -25.47 -25.47 -25.47 -25.82 -25.72	8 YAL -25.62 -25.75 -25.63 -26.67 -25.68 -25.85 -25.85 -25.85 -25.85 -25.85	0.21 0.06 -0.08 0.09 0.27 -0.05 -0.03 0.17 0.12 -0.23 0.08 0.35 0.24	-0.03 -0.05 -0.00 -0.08 0.00 0.00 0.00 0.00 -0.23 0.00	0.00 0.00 0.06 0.08 0.09 0.12 0.17 0.21 0.21 0.24 0.27	1.00 2.00 3.00 4.50 4.50 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 2.00 0.00 4.50 0.00 0.00 0.00 0.00 11.00 0.00	0.00 0.00 3.00 0.00 4.50 6.00 7.00 8.00 10.00 12.00 13.00
MERN A: MERN B:	-25.66 -25.75	STO DEV	A: (D. 13 D. 16	SUN OF N SUM OF N	MINUS: PLUS:	18.50	86.50
MILCOXON	ANALYSI	3						
ANRLYSIS	0F:	CHEST	X					
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: R				MIN Hin	
SUBJ	A VAL	B VAL	A-B	080 -	080 +	N	N -	N +
0-1 M10 R-1 K-1 F-2 R-2 H11 G-3 S-3 M13 H-2 F-3	-2.61 -1.36 -0.45 -1.09 -1.13 -0.17 -1.16 -1.86 -2.29 -0.89 -1.55 -2.35	B VAL -1.60 -2.17 -0.94 -1.03 -2.56 -0.79 -3.79 -2.13 -1.93 -2.62 -1.98 -2.01 -4.10 -1.46	-1.01 0.81 0.49 -0.06 1.43 1.62 0.97 0.33 1.55 -0.89	-0.06 0.00 0.00 0.00 0.00 -0.00 -0.89 0.00 -1.01 0.00 0.00	0.00 0.33 0.33 0.49 0.52 0.81 0.00 0.097 0.00 1.18 1.43 1.55	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1,00 0,00 0,00 0,00 0,00 0,00 8,00 10,00 10,00 0,00	0.00 2.00 3.00 4.00 5.00 7.00 0.00 9.00 0.00 12.00 13.00

THE PARTY OF THE P

SIGNIFICANT DIFFERENCE

CHEST Z

MERN R: MERN B:

ANALYSIS O	F:	CHEST	7.			MAX		
FUNCTION A	- G: 10		CELL: C			MAX	N -	N +
SUBJ	A VAL	8 VAL	A-B	ORD -	ORD +	 	1.00	0.00
0-1 M10 R-1 F-2 M11 G-3 F-3 H13 M-3	13.95 19.69 15.30 18.39 24.11 11.41 18.12 14.36 20.86 26.23 14.76 19.43 21.73 17.36	16.73 17.67 16.50 18.52 22.88 18.25 18.77 22.74 21.86 25.39 16.92 25.04 20.08 19.12	2.02 -1.20 -0.23 -6.84 -0.65 -8.38 -1.00 -5.61 -5.61	-0.65 0.00 -1.00 -1.20 0.00 -1.76 0.00 -2.16 -2.78 -5.61 -6.84 -8.38	0.00 0.84 0.00 0.00 0.02 1.66 0.00 0.00 0.00	2.00 3.00 4.00 6.00 7.00 8.00 9.00 10.00 12.00 13.00	2.00 0.00 4.00 5.00 0.00 0.00 10.00 11.00 12.00 13.00	3.00 3.00 0.00 0.00 0.00 0.00 0.00 0.00
MEAN A:	18.26	STO DE	/ A:	3 02	SUM OF A	N PLUS : ~		23.00
MEAN B:	20.04	310 00			MMM \$10	GNIFICANT	DIFFERENC	E WHH
RNRLYSIS		CHES					ях	
FUNCTION	A . G:	10 10	CELL:	e C		H	AX 	N +
SHRJ	A VAL	B VAL	A-8	ORD -	ORD +		N	1.00
D-1 H10 H-1 K-2 H1-2 H1-2 S-3 H1-3 K-3	28.20 33.25 29.17 32.47 17.12 30.97 26.19 32.49 32.49 29.84 38.23 31.60	27.57 31.71 33.06 37.60 38.10 32.99 39.65 35.13 38.79 47.31 33.38 27.58	0.63 1.83 -4.93 -4.93 -15.68 -8.68 -6.32 -5.43 -17.86	0.00 0.00 0.00 0.00 -3.89 0.00 0.00 -4.93 -5.02 -6.32 -8.68 -8.94	0.43 0.63 1.54 2.37 0.00 4.85 0.00 0.00 0.00	N 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00	0.00 0.00 0.00 5.00 0.00 8.00 9.00 10.00 11.00 12.00	2.00 3.00 4.00 0.00 6.00 7.00 0.00 0.00 0.00 0.00
MERN A	31.1	4 510 3 510	DEV A: DEV B:	6.86 5.94	SUM OI	F N PLUS :	82.00	23.00
MEHN B	, ,,,,					SIGNIFICAN'	DIFFERE	NUE MMX

MMM SIGNIFICANT DIFFERENCE MMM

	UI;	TOTA	ונ אונט א	EEL				
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL:	A C		M	IRX IRX	
SUBJ	A VAL	B VAL	A-B	080 -	ORD +	N	N -	N •
D-1 M10 R-1 K-1 F-2 R-2 M11 G-3 F-3 M-2 F-3	87.60 54.47 153.36 54.44 73.93 106.49 110.66 93.86 103.98 111.94 89.03 53.54 99.70 130.98	95.09 71.71 133.12 74.81 141.31 62.10 100.75 98.47 137.25 115.46 114.87 130.38 152.73 133.82	-7.49 -15.24 -20.37 -67.38 -4.39 -4.61 -3.52 -25.84 -76.84 -53.03	080 - -2.84 -3.52 -4.61 -7.49 -0.00 -15.24 -0.00 -20.37 -25.84 -33.27 -33.27 -53.03 -67.38 -76.84	0.00 0.00 0.00 9.91 0.00 20.24 0.00 0.00 44.39 0.00	1.00 2.00 3.00 4.00 5.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 2.00 3.00 4.00 0.00 6.00 8.00 9.00 10.00 12.00 13.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
MEAN A: MEAN B:	94.71 111.56	STO DE STO DE	V A: V B:	28.89 28.45	SUM OF N	MINUS: PLUS:	82.00 DIFFEREN	23.00
	ANALYSI'	3 - 1016	AL SEAT)	(
ANALYSIS	OF:	- 1016	CELL:	A		,	11 N 11 N	
ANALYSIS	OF:	- 1016	CELL:	A	0AD +	N N	41N 41N N -	N +
ANALYSIS	OF:	- 1016	CELL:		080 + 0.00 0.00 16.13 0.00 21.47 22.45 36.80 46.51 56.42 0.00 82.99 100.73	N 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 10.00 11.00 11.00	N - 1.00 2.00 3.00 0.00 0.00 0.00 0.00 0.00 0	N +

MAH SIGNIFICANT DIFFERENCE MAH

	-					
ANALYSIS OF:	TOTAL SEAT Z			MRX		
						Al a
SUBJ fi VAL	B VAL A-B	ORD -	ORD +	H	N -	0.00
0-1 2018.27 M10 1541.13 R-1 1918.39 K-1 1960.70 F-2 1593.65 R-2 1596.30 M11 1606.59 G-2 1047.95 G-3 1616.36 S-3 1751.68 R-3 1553.97 M13 1630.50 M-2 1671.90 F-3 1534.20	8 VAL A-B 2210.54 -192.27 1612.33 -71.20 1896.12 22.27 2064.17 -103.47 1706.14 -112.49 1579.04 17.26 1760.95 -154.36 1329.03 -231.08 1841.50 -224.94 1689.28 62.40 1554.18 -0.21 1665.83 -35.33 1665.17 -43.27 1664.52 -130.32	-0.21 0.00 0.00 -35.33 -43.27 0.00 -71.20 -103.47 -112.49 -130.32 -154.36 -192.27 -224.94 -281.08	0.00 17.26 22.27 0.00 62.40 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 5.00 7.00 8.00 9.00 10.00 11.00	1.00 0.00 0.00 0.00 7.00 7.00 10.00 11.00 12.00 14.00	3.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
MERN B: 1731.3	3 510 0EV 8: 6	19.56	SUM OF N SUM OF N MAN SIG	reds .		
ANRLYSIS OF:	RES SEAT FO	RCE				
		73		Mi M		
SUBJ A VA	L B VAL A-B	ORD -	ORD +	N	N -	N +
0-1 2030.1 M10 1561.6 R-1 1951.1 K-1 1982.0 F-2 1630.6 R-2 1605. M11 1623.0 G-2 1058.1 G-3 1641. S-3 1782. R-3 1565. M13 1666. M-2 1632. F-3 1556.	G: 10 CELL: G: 10 CELL: L B VAL A-B 1 2225.09 -195.96 18 1634.33 -72.65 19:8.20 32.99 19:8.20 -117.46 19:8.20 -124.00 19:8.20 -124.00 19:8.20 -100.30 17:4.69 -160.30 17:4.69 -250.5 17:4.69 -250.5 17:4.69 -250.5 17:4.69 -250.5 17:4.69 -250.5 17:4.69 -250.5 17:4.69 -250.5 18:61.29 -250.5 18:61.29 -250.5 18:65.1570.47 -4.8 65:1570.47 -4.8 65:1570.47 -4.8 66:1590.93 -134.2	-4.82 0.00 0.00 -35.57 -53.19 0.00 -72.65 -117.46 -124.01 7 -134.28 2 -160.35 7 -195.98 9 -219.58	0.00 .7.61 .2.94 0.00 0.00 65.87 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 5.00 7.00 8.00 9.00 11.00 12.00 13.00	1.00 0.00 0.00 4.00 5.00 0.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00	0.000 30.000 0.000 0.000 0.000 0.000 0.000
MCAN A: 1663	.94 STO DEV A:	238.20	SUM OF	N MINUS: N PLUS :	94.00	11.00

MMM SIGNIFICANT DIFFERENCE MAM

MCAN A: 1663.94 STO DEV A: 238.20 MERN B: 1755.52 STO DEV B: 222.35

WILLOXON UNALISIS

MEAN A: MEAN B: 540.65 464.51 STO DEV R: STO DEV B:

		-						
ANALYS15	OF:	TOT	IL FOOT X					
FUNCTION FUNCTION	n = G: B = G:	10 10	CELL: A			M	IN IN	
SUBJ	A VAL	B VAL	A-8	OAD -	ORD +	N	N -	N +
D-10 R-1 K-2 K-2 H12 G-3 R13 K-3 M-3	-944.80 -475.94 -680.89 -508.90 -481.47 -444.18 -558.49 -558.49 -362.52 -361.98 -578.49 -635.96 -543.43	-571.22 -353.10 -677.09 -296.95 -425.15 -495.03 -334.84 -246.99 -337.72 -282.10 -300.25 -414.06 -312.68 -363.74	9-8 -373.58 -122.84 -3.89 -21:.95 -56.32 -50.85 -127.06 -311.50 -311.50 -124.68 -61.73 -164.43 -323.08 -179.69	-3.80 -0.00 -56.32 -61.73 -80.42 -124.68 -127.06 -164.43 -179.69 -211.95 -311.50 -323.98 -373.58	0.00 50.85 0.00 0.00 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 10.00 11.00 12.00 14.00	1.00 0.00 3.00 4.00 5.00 6.00 7.00 8.00 10.00 11.00 12.00 14.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
MEAN A: MEAN B:	-535.81 -386.51	STD DE	EV A: 14	8.71 1.06	SUM OF N SUM OF N	MINUS: PLUS :	103.00	2.00
					MMM SIGI	NIFICANT	DIFFEREN	CE HXX
MILCOXON	1 BNBL421	5 -						
ANALYS15	OF:	TOT	AL FOOT Z					
FUNCTION FUNCTION	1 A = G: 1 B = G:	10 10	CELL: A			HI HI	QΥ	
SUBJ	A VAL	8 VAL	A-8	OR2 -	ORD +	N	N -	N +
D-1 M10 R-1 K-1 F-2 R-1 G-2 G-3 F-3 M12	744.50 502.32 546.82 597.93 467.93 467.96 472.60 478.55 514.59 517.97	599.02 445.71 622.76 431.87 537.13 430.27 464.64 389.29 370.12 446.70 423.95 484.01 431.83	A-B 145.48 57.05 10.55 114.95 60.80 34.14 113.39 72.50 34.60 113.22 129.14 101.32		10.56 11.26 14.64 57.05 67.90 72.43 101.32 113.22 113.39 1149.14	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.00 2.00 3.00 4.00 5.00 7.00 8.00 9.00 10.00 11.00 13.60

SIGNIFICANT DIFFERENCE NAM

105.00

SUM OF N MINUS: 0.00 SUM OF N PLU": -----

81.89 73.63

ANALYSIS	OF:	RES F	OOT FORC	E				
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: A			F	RBS RBS	
SUBJ ,	A VAL	B YAL	A-B	ORD -	ORD +	N	N -	N +
0-1 M10 K-1 F-2 R11 G-3 G-3 H12 H-2 F-3	153.58 1611.03 868.36 707.32 710.80 568.89 639.29 646.32 603.53 558.65 516.49 800.50 823.69 728.44	8 YAL 765.67 515.64 838.29 616.31 585.77 504.75 395.06 462.06 481.05 570.14 504.36 515.42	387.91 95.39 30.30 239.03 94.49 -16.97 134.49 251.26 138.64 76.59 230.36 319.33 213.02	-16.97 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	0.00 30.30 35.39 76.59 94.49 95.39 138.64 2130.36 239.33 251.26 319.33 387.91	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 11.00 12.00 13.00	1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.000 2.000 9.000 5.000 6.000 9.000 10.000 12.000 13.000
MEAN A: MEAN B:	709.76 550.53	STD DEV	A: 16 B: 12	4.97 0.69	SUM OF N SUM OF N	MINUS: PLUS :	1.00	104.00
MILCOXON		-			NNN SIGI	ATT TOHIN:	Dirring	NCE AAR
		CHEST						
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: B			M	11N 11N	
5UB J	A VAL	B VAL	A-B	ORD -	ORD +	N	N -	N +
S-3 G-3 R-3 D-1 G-2 F-3 M11 F-2 M10 M13 M-2 K-1 R-2	-1.93 -2.74 -0.67 -0.96 -1.07 -1.93 -2.48 -0.97 -1.26 -1.54 -2.83 -0.85	B VAL -1.71 -3.44 -2.28 -1.67 -0.72 -2.31 -3.28 -1.70 -1.51 -1.77 -3.39 -2.35 -0.51	-0.22 0.70 1.61 0.71 -0.35 0.80 0.81 0.25 0.56 1.50	0.00 -0.22 0.00 -0.35 0.00 0.00 0.00 0.00	0.08 0.23 0.25 0.00 0.38 0.56 0.70 0.71 0.80 0.81 1.50	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 2.00 0.00 0.00 0.00 0.00 0.00 0.00	1.00 0.00 3.00 0.00 6.00 8.00 9.00 10.00 11.00 12.00
MEAN A: MEAN B:								

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HHR SIGNIFICANT DIFFERENCE PHR

ANALYSIS	OF:	HEAD	7					
FUNCTION FUNCTION	A = G: 8 = G:	10 10	CELL: C	3		4	IAX IAX	
SUBJ	A VAL	B VAL	A-8	0RD -	0A0 +	N	N -	N +
S-3 R-3 D-1 G-2 F-3 M11 F-2 M13 M-2 K-1 R-2	13.90 12.12 13.71 13.05 14.26 12.04 14.54 13.89 13.43 13.10 11.73 12.50 13.78	B VAL 13.34 11.85 11.91 12.47 12.66 12.25 14.40 13.41 14.19 12.99 11.82 11.77 12.55	0.56 0.27 1.80 0.58 1.60 -0.21 0.14 0.48 -0.76 0.11 -0.09 0.73 1.23	-0.09 0.00 0.00 -0.21 0.00 0.00 0.00 -0.76 0.00 0.00	0.00 0.11 0.14 0.00 0.27 0.48 0.56 0.58 0.73 0.00 1.23 1.60	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 0.00 0.00 4.00 0.00 0.00 0.00 0.00	0.00 2.00 3.00 0.00 5.00 7.00 8.00 9.00 11.00 12.00
MEAN A: MEAN B:	13.23 12.74	STO DEV	A: B:	0.90 0.88	SUM OF N SUM OF N	MINUS: PLUS :	15.00	76.00
HILCOXON	ANALYSI:	S .			*** 310	VII ICHNI	DITT CHEN	
ANALYSIS	OF:	HEAD	RES					
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: E	3		9	185 185	
SUBJ	A VAL	8 VAL	A-B	ORC -	GRD +	N	N -	N +
5-3 R-3 R-3 D-1 G-2 F-3 M11 F-2 M13 M-2 K-1 R-2	14.30 12.19 13.76 13.18 14.30 12.38 14.67 14.01 14.09 13.14 12.40 12.81 13.79	B VAL 13.74 11.91 12.25 12.57 12.72 12.78 14.84 13.69 14.43 13.59 11.91 11.84 12.60	0.56 0.28 1.51 0.61 1.58 -0.40 -0.17 0.32 -0.34 -0.45 0.97 1.19	-0.17 0.00 0.00 -0.34 -0.40 -0.45 0.00 0.00 0.00 0.00	0.00 0.28 0.32 0.00 0.00 0.49 0.56 0.97 1.19	1.00 2.00 3.00 4.90 5.00 6.00 7.00 6.00 10.00 11.00 12.00	1.00 0.00 4.00 5.00 6.00 0.00 0.00 0.00 0.00	0.00 2.00 3.00 0.00 0.00 7.00 8.00 9.00 10.00 12.00

MEAN A: 13.46 STO DEV A: 0.83 SUII OF N MINUS: 16.00 ------ MEAN B: 12.99 STO DEV B: 0.98 SUM OF N PLIS: ----- 75.00

ANALYSIS OF: TOTAL SHED REFL

FUNCTION FUNCTION	A = G: 1 B = G: 1	10	CELL: B			MA MA	U	
SUBJ	A VAL	B VAL	A-8	URD -	080 +	N	N -	N +
S-3 G-3 R-3 D-2 F-3 H12 H13 H1-2 K1-2	118.11 126.99 73.06 106.23 78.30 104.38 88.52 80.71 62.87 99.51 81.58 73.31 87.01	B VAL 105.59 140.36 91.14 93.91 79.75 145.78 107.26 113.07 94.47 95.32 101.27 99.04 128.23	12.52 13.37 18.08 12.32 -1.45 -1.45 18.76 -32.36 -32.36 -31.60 -4.19 -25.73 -41.22	-1.45 0.00 0.00 0.00 -13.37 -18.08 -18.76 -19.69 -25.73 -31.60 -32.36 -41.22 -41.40	0.00 4.19 12.32 12.52 0.00 0.00 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00	1.00 0.00 0.00 0.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 13.00	0.000
MEAN A:	90.81	STD DEV	A: 1	18.97	SUM OF N	MINUS:	82.00 -	9.00
MEAN B:	107.32	STO DEV	B : 1	19.71	NNN SIG	NIFICANT	DIFFEREN	
	ANALYSIS	5						
		101AL				M	AX AX	
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL:	B D	ORD +	K.	AX	N +
FUNCTION FUNCTION	A = G: B = G:		CELL:	B D	0.00 5.76 0.00 0.00 0.00 22.11 0.00 0.00 0.00 0.0	K.	AX	N

	· =	
ANALYSIS OF:	TOTAL SHOULDER	
FUNCTION A = G: FUNCTION B = G:	III LELLY U	NAX MAX
SUBJ A VAL	B VAL A-B ORD -	CRD + N N - N +
S-3 223.37 G-3 225.22 R-3 98.22 D-1 161.97 G-2 132.10 F-3 196.28 M11 182.46 F-2 136.69 M10 114.26 M13 181.73 M-2 151.28 K-1 107.22 R-2 146.92	182.50	CRD + N N - N + C.00 1.00 1.00 0.00 13.07 2.00 0.00 2.00 0.00 3.00 3.00 0.00 0.00 4.00 4.00 0.00 0.00 5.00 5.00 0.00 40.87 6.00 0.00 6.00 0.00 7.00 7.00 0.00 0.00 8.00 8.00 0.00 0.00 9.00 9.00 0.00 0.00 10.00 10.00 0.00 0.00 12.00 12.00 0.00 0.00 13.00 13.00 0.00
MEAN A: 158.29 MEAN B: 202.91	STD DEV A: 41.62 STD DEV B: 36.76	SUM OF N MINUS: 83.00 SUM OF N PLUS: 8.00
		NAM SIGNIFICANT DIFFERENCE NAM
WILCOXON ANALYSI	•	
	TOTAL SEAT Z	
FUNCTION A = G: FUNCTION B = G:	10 CELL: B 10 CELL: D	MAX MAX
SUBJ A VAL	B VAL A-B ORD -	ORO + N N - N +
S-3 1753.39 G-3 1663.42 R-3 1572.24 O-1 2006.65 G-2 1143.59 M11 1646.17 F-2 1613.10 M10 1527.30 M13 1654.81 M-2 1661.58 K-1 1824.31 R-2 1530.01	1784.78	080 + N N - N + 14.17 1.00 0.00 1.00 0.00 2.00 2.00 0.00 0.00 3.00 3.00 0.00 0.00 4.00 4.00 0.00 0.00 5.00 5.00 0.00 0.00 6.00 6.00 0.00 0.00 7.00 7.00 0.00 0.00 8.00 8.00 0.00 0.00 9.00 9.00 0.00 0.00 10.00 10.00 0.00 0.00 11.00 11.00 0.00 0.00 12.00 12.00 0.00
MEAN A: 1619.84 MEAN B: 1688.45	STD DEV A: 201.19 5 STD DEV B: 206.42	SUM OF N MINUS: 90.00 SUM OF N PLUS: 1.00

SIGNIFICANT DIFFERENCE MAN

HNHL1312 OF:	HES SEAT FORCE	
FUNCTION R = G: FUNCTION B = G:	10 CELL: B 10 CELL: D	MAX MAX
SUBJ A VAL	B VAL A-B ORO -	ORD + N N - N +
S-3 1780.42 G-3 1686.50 R-3 1591.42 D-1 2012.48 G-2 1148.93 F-3 1472.54 M11 1673.09 F-2 1645.51 M10 1543.03 M13 1693.96 M-2 1681.00 K-1 1844.09	1811.34	0RD + N N - N + 0.00 1.00 1.00 0.00 15.83 2.00 0.00 2.00 0.00 3.00 3.00 0.00 0.00 4.00 4.00 0.00 0.00 5.00 5.00 0.00 0.00 6.00 6.00 0.00 0.00 7.00 7.00 0.00 0.00 8.00 8.00 0.00 0.00 9.00 9.00 0.00 0.00 10.00 10.00 0.00 0.00 11.00 11.00 0.00 0.00 12.00 12.00 0.00
1333.00	1576.75 -55.75 -205.05	0.00 13.00 13.00 0.00
MERN A: 1639.38 MERN B: 1709.18	STD DEV A: 203.95 STD DEV B: 208.52	SUM OF N MINUS: 89.00 2.00
		MMM SIGNIFICANT DIFFERENCE MMM
WILCOXON ANALYSI	\$	
************	S - TOTAL FOOT X	
ANALYSIS OF: FUNCTION A = G:	TOTAL FOOT X 10 CELL: B	MIN MIN
ANALYSIS OF: FUNCTION A = G:	TOTAL FOOT X 10 CELL: B	MIN
ANALYSIS OF: FUNCTION A = G:	TOTAL FOOT X 10 CELL: B	

SIGNIFICANT DIFFERENCE MAN

ANALYSIS	OF:	TOTA	AL FOOT Z	!				
FUNCTION FUNCTION	A - G: B - G:	10 10	CELL:	8			HAX HAX	
SU8J	A VAL	8 VAL	A-8	ORD -	0RD +	N	N -	N +
S-3 G-3 R-9 D-1 G-2	558.45 456.19 455.63 678.79 430.54 645.09 473.72 541.41 495.17 618.26 581.84 593.68 471.45	487.39 436.65 395.33 615.05 392.13 509.57 385.85 5455.41 559.74 523.15 489.99 408.05	71.06 19.54 60.30 63.74 38.41 136.52 87.87 -3.60 39.76 58.52 58.69 103.69 63.40	080 - -3.60 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 19.54 36.41 39.76 58.52 58.69 60.30 63.74 71.06 87.87 103.69 136.52	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 2.00 3.00 4.00 5.00 7.00 9.00 10.00 11.00 13.00
MEAN A: MEAN B:	538.48 477.10	STO DE	V A: IV B:	80.93 72.43	SUM OF N	MINUS: PLUS :	1.00	90.00
					NNN SIG	NIFICANT	DIFFERE	NCE HHH
HILCOXON	ANALYSIS	S -						
		RES	FOOT FOR	RCE				
ANALYS15	Of:	-					185 185	
RNALYSIS FUNCTION FUNCTION SUBJ	0f: A = G: B = G:	RES 10 10	CELL: CELL:	8 0	0A0 +	N	1B5 N -	N +
RNALYSIS FUNCTION FUNCTION SUBJ	0f: A = G: B = G:	RES 10 10	CELL: CELL:	8 0	080 + 41.22 41.85 -2.04 51.16 76.87 81.14 82.36 113.68 106.67 207.92 222.58 305.10	N	1B5 N -	N + 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 11.00 12.00 13.00

HMM SIGNIFICANT DIFFERENCE HMM

ANALYSIS	0F:	CHES	T \$1					
FUNCTION FUNCTION			CELL:				1AX 1AX	
SUBJ	ก VAL	B VAL	A-B	0R0 -	ORD +	N	N -	N +
0-1 K-1	38.79 27.58 32.99 43.06 38.10 95.13 47.31 33.39 27.34	46.87 37.64 33.47 43.30 54.95 47.553 47.553 32.86	-8.08 -10.06 -0.48 -0.27 -16.80	-0.27 -0.48 0.00 -3.43 0.00 -4.92 -8.08 -8.15	0.00 4.68 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00	5.00 0.00 7.00 8.00 9.00 10.00	
	35.40 41.12	SID DE SID DE		6.15 6.75	SUM OF N SUM OF N	PLUS :		10.00 NCE HAR

WILCOXON ANALYSIS

ANALYS1S	OF:	HEAD :	K					
FUNCTION FUNCTION			CELL: C				NIN NIN	
SUBJ	A VAL	B VAL	A-B	ORD -	ORD +	N	N ~	N +
D-1 K-3 G-3 R-2 S-2 S-2 N13 R-10 H11	-4.62 -6.27 -3.95 -4.02 -4.75 -5.39 -5.39 -5.39 -3.93	-5.58 -3.43 -4.91 -2.25 -4.14 -4.78 -4.57 -4.57	-0.06 -0.37 -0.52 -0.52 -1.77 -0.33 -0.97 -1.04 -0.85 -0.49	-0.42 0.00 0.00 -0.52 -0.64 -0.69 -0.85	0.00 0.00 0.37 0.00 0.42 0.49 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 2.00 0.00 4.00 0.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
MERN A: MEAN B:	-4.90 -4.44	SID DEV		0.95 1.13	SUM OF N		77.00	14.00
					MMM SIG	NIFICANT	DIFFERE	NCE HHH

The second secon

ANNLYSIS OF:	HEAD Z			
FUNCTION A = G: FUNCTION B = G:				MAX MAX
SUBJ R VAL	B VAL A-B	0RU - 0	9D + N	N - N +
D-1 13.74 K-1 12.31 G-3 13.02 F-3 13.56 R-2 14.21 S-3 13.69 F-2 14.62 G-2 12.39 M13 13.15 M-2 11.31 R-3 13.32 M10 14.37 M11 12.89	12.93 -0.62 16.13 -3.11 13.87 -0.31 14.86 -0.65 15.53 -1.84 16.88 -2.26 14.05 -1.66 16.20 -3.05 13.39 -2.08	-0.31 -0.62 -0.65 -1.01 -1.05 -1.62 -1.66 -1.84 -2.08 -2.26 -3.05	0.22 1.00 0.00 2.00 0.00 3.00 0.00 4.00 0.00 5.00 0.00 6.00 0.00 8.00 0.00 9.00 0.00 10.00 0.00 11.00 0.00 12.00	0.00 1.00 2.00 0.00 3.00 0.00 4.00 0.00 5.00 0.00 6.00 0.00 7.00 0.00 8.00 0.00 9.00 0.00 10.00 0.00 11.00 0.00 12.00 0.00
MEAN A: 13.21 MEAN B: 14.71		1.32 SU	M OF N MINUS: M OF N PLUS ; * SIGNIFICANT	1.00

WILCOXON ANALYSIS

ANALYSIS O	JF:	HEAD F	RES					
FUNCTION A			CELL: C CELL: E				RBS RBS	
SUBJ	A VAL	B VAL	A-8	080 -	0RD +	N	N -	N +
D-1 K-1 G-3 F-3 R-3 R-3 F-2 M13 M-3	13.03 13.58 14.41 13.87 14.82 12.42 13.21 11.63 13.33	16.26 17.24 14.20 16.29 13.42 14.56 15.76	-1.48 -0.85 -3.14 -0.39 -0.52 -2.39 -2.42 -1.78 -3.08 -1.79 -1.23 -1.23 -0.28	-0.85 -1.23 -1.27 -1.48 -1.78 -1.79 -2.39 -2.42 -3.08		1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.000
MEAN A: MEAN B:	13.41 14.95	STO DEV STD DEV		0.92 1.37	SUM OF N SUM OF N	PLUS :	90.00 -	1.00

205.14

MEAN A:

MEAN B:

SID DEV A: SID DEV B:

MILCOXON		-						
ANALYSIS	0F:	HEAD	SI					
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: C			F	RRS IBS	
SUBJ	A VAL	B VAL	A-8	080 -	080 +	N	N -	N +
D-1 G-3 F-3 R-2 S-3 F-2 G-2 M13 M-2 R-3 M10	21.47 16.85 19.41 19.71 20.90 18.79 23.25 18.46 19.61 15.06 19.22 22.92 18.88	8 VAL 25.91 23.50 24.25 24.80 23.65 25.14 29.17 23.08 26.51 18.69 22.47 27.64 21.16	-46.849.5 -46.809.5 -52.65.969.6 -69.627.6 -46.69.627.2 -46.69.627.2	-2.28 -2.75 -3.63 -4.62 -4.62 -4.89 -5.92 -6.69	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 9.00 10.00 11.00 12.00 13.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00
		STD DE						
					HAM SIG			
HILCOXON	ANALTSI:	5						
ANALYSIS	OF:	TOTAL	SHOULDE	.R				
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: C			M	IRX IRX	
\$U8J	A VAL	B VAL	R-8	ORD -	080 +	N	N -	N +
D-1 K-1 G-3 F-3 R-2 S-3 F-2 M13 M-2	189.95 137.30 256.32 259.04 120.70 209.19 240.70 167.70 265.70 292.51	B VAI. 166.57 152.05 130.38 159.65 95.47 121.02 162.83 91.13 212.43 197.82 178,36 96.14 137.90	23.38 -14.75 125.94 99.39 25.23 88.17 77.87 75.99 53.27 94.69	-14.75 0.00 0.00 0.00 0.00 0.00 0.00	0.00 23.38 25.23 32.41 37.38 46.14 53.27 75.99 77.87 88.17	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00	1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 2.00 3.00 4.00 5.00 5.00 9.00

MAN SIGNIFICANT DIFFERENCE MAN

1.00

90.00

SUM OF N MINUS: 1.00 SUM OF N PLUS: -----

56.44 38.79

ANALYSIS	OF:	10 TRL	LRP					
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL:	C E			MAX MAX	
SUBJ 0-1 K-1 G-3 F-3 R-2 F-2 M13 M-2 M11	8 VAL 95.53 102.62 103.27 131.86 73.47 101.50 62.69 59.03 91.44 125.12 80.26	8 VAL 122.87 134.34 106.51 103.17 102.95 80.48 85.88 71.45 127.93 146.56 125.31 83.60 117.60	A-B -27.34 -31.52 -3.24 28.69 -29.48 -21.027 -10.76 -68.90 -55.127 -0.048 -37.34	080 - -0.07 -3.24 -14.48 -16.76 - 0.00 -23.07 -27.34 -0.00 -29.48 -31.52 -37.34 -55.12 -68.90	080 + 0.00 0.00 0.00 0.00 21.02 0.00 0.00 28.69 0.00 0.00 0.00	N 2.00 3.00 4.00 5.00 6.00 8.00 9.00 10.00 11.00 12.00	N - 1.00 2.00 3.00 4.00 0.00 7.00 0.00 9.00 11.00 12.00	N
MEAN A:	88.54	SID DEV	A:	24.53 23.13	SUM OF N	MINUS: PLUS :	78.00	13.00
M:LCOXON	ANALYSI	5						
ANALYSIS	OF:	TOTAL	SERT	x				
FUNCTION FUNCTION	A = C: B = C:	10 10	CELL:	C E			NIN NIM	
SUBJ	A VAL	B VAL	A-8	0R0 -	080 +	N	N -	N +
D-1 K-1 G-3 F-3 F-2 S-2 S-2 M13 K-3 M10 H11	-265.36 -389.61 -279.54 -300.22 -171.85 -3195.60 -163.13 -344.28 -267.07 -213.48 -266.53 -330.65	8 VAL -328.91 -390.53 -301.97 -319.09 -210.54 -370.49 -458.20 -166.77 -393.89 -286.57 -255.70 -322.62 -321.76	63.552 22.487 38.692 59.06641 59.06641 49.522 49.526 49.526 56.89	0.00 -8.89 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.92 0.007 8.80 20.609 20.609 20.609 20.609 63.55	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 12.00 13.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.00 0.00 3.00 4.00 5.00 6.00 6.00 10.00 11.00 12.00
		SID DEV SID DEV						

SIGNIFICANT DIFFERENCE WHA

ANALYSIS OF:

TOTAL SERT Z

FUNCTION FUNCTION	V A = G: N B = G:	10 0	ELL: C			M	AX AX	
SUBJ	A VAL	B VAL	A-8	080 -	ORD +	N	N -	N +
K-13 F-3 F-3 F-3 F-3 F-3 M13 M11 M11	2210.54 2064.17 1641.30 1664.52 1579.04 1689.28 1706.14 1329.03 1665.17 1554.18 1760.95		38.05 38.05 38.05 30.55 30.55 30.74 21.10 72.47 30.85 37.09 30.78	0.00 -57.06 -61.45 -72.47 -88.05 -90.85 -100.56 -103.65 -107.09 -142.68 -195.67	21.10 30.78 0.00 0.00 0.00 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 0.00 3.00 4.00 5.00 5.00 7.00 8.00 9.00 10.00 11.00 12.00	
MERN A: MERN B:		STO DEV						3.00
					HMM SIGN	IFICANT	DIFFERENC	E KKK
	N ANALYSI	•						
		RES SE						
FUNCTION FUNCTION	N A = G: N B = G:	10 10	CELL: C	•		M M	AY	
SUBJ	A VAL	8 VAL	A-B	080 -	ORD +	N	N -	N +
0-1 6-3 6-3 8-3 6-3 6-3 6-3 M1-3 M11	2226.09 2099.55 1861.29 1690.93 1587.72 1716.92 1754.69 1338.79 1702.18 1686.06 1570.47 1634.33 1789.99		96.67 65.12 48.94 50.67 54.36 514.35 77.86 93.54 93.54 93.54	0.00 0.00 -60.67 -65.12 -77.86 -93.54 -96.67 -108.62 -116.71 -148.94 -204.56 -304.35	19.15 23.74 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 0.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 2.00 0.00 0.00 0.00 0.00 0.00 0.00
MEAN A: MEAN B:	1743.00 1845.51	STO DEV STO DEV						

SIGNIFICANT DIFFERENCE HEN

ANALYSIS OF:	TOTAL FOOT	x				
FUNCTION R = FUNCTION B =	G: 10 CELL: G: 10 CELL:	C E		M	NIN NIN	
SUBJ A VA	L B VAL A-B	ORD -	CRD +	N	N -	N +
D-1 -571.2 K-1 -296.9 G-9 -397.7 F-3 -363.7 R-2 -495.0 S-3 -282.1 F-2 -425.1 G-2 -2414.0 M-2 -312.8 R-3 -300.2 M10 -353.1 M11 -334.8	L 8 VAL A-8 2 -713.93 142.71 5 -336.36 41.41 2 -336.34 -1.38 4 -527.61 163.87 3 -496.63 1.80 0 -295.48 13.38 5 -430.93 5.78 9 -345.34 98.36 6 -453.70 39.64 8 -507.35 194.47 5 -270.62 -29.63 0 -359.69 6.59 4 -517.70 182.86	-1.38 0.00 0.00 0.00 0.00 -29.63 0.00 0.00 0.00 0.00	0.00 1.80 5.78 6.59 13.38 0.00 39.64 41.41 98.35 142.71 163.87 182.85 194.47	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 10.00 11.00 12.00	1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 2.00 3.00 4.00 5.00 7.00 8.00 10.00 11.00 12.00
MERN R: -364. MERN B: -430.	16 STD DEV A: 30 STD DEV B:	91.10 123.03	SUM OF N SUM OF N	MINUS: PLUS :	7.00	84.60
HILCOXON ANALY	TOTAL FOOT					
FUNCTION A =	G: 10 CELL:	C F		M	AY	
SUBJ A VE	IL 8 VAL A-8	ORD -	ORD +	N	N -	N +
D-1 599.0 K-1 431.8 G-3 370.1 F-3 425.5 R-2 430.6 S-3 446. F-2 537.1 G-2 3R9.6 M-2 431.8 R-3 423.9 M10 445.	8 VAL	-4.14 0.00 -5.28 -13.59 0.00 -30.19 -35.58 -36.12 -39.05 -68.27 -76.13 0.00 -109.34	0.00 9.83 0.00 19.35 0.00 0.00 0.00 0.00 0.00 85.79 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 0.00 3.00 4.00 5.00 7.00 8.00 10.00 11.00 0.00	0.00 2.00 0.00 0.00 5.00 0.00 0.00 0.00
MEAN A: 452.	34 STO DEV A: 90 STO DEV B:	60.21 80.66	SUM OF N	MINUS: PLUS :	72.00	19.00

MMM SIGNIFICANT DIFFERENCE MAN

MERN A: MERN B:

ANALYSIS	RES FOOT FURCE							
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: C			A	85 8 5	
SUBJ	A VAL	B VAL	R-8	080 -	ORD +	N	N -	N +
D-1 K-1 G-3 F-3 R-2 S-3 F-2 M13 M-2 R-3 M10 M11	765.67 468.29 464.89 515.42 585.77 482.06 616.31 395.06 570.14 504.36 481.05 515.64 504.75	B VAL 921.60 522.58 529.58 5709.55 624.39 591.18 657.93 467.16 655.92 386.88 520.54 674.66	-155.93 -54.29 -64.90 -194.13 -38.62 -109.12 -41.62 -72.10 -101.42 -151.56 114.17 -4.90 -169.91	-4.90 -38.62 -41.62 -54.29 -64.90 -72.10 -101.42 -109.12 0.00 -151.56 -155.93 -169.91	0.00 0.00 0.00 0.00 0.00 0.00 0.00 114.17 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 0.00 10.00 11.00 12.00 13.00	
MEAN A: MEAN B:	528.42 608.75	STD DE STD DE	V A: 9 V B: 13	1.44 5.86	SUM OF N	MINUS: PLUS :	82.00 -	9.00
HILCOXON	9NALYSIS							
ANALYSIS	OF:	CHES	T X					
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL: C	1			RX RX	
SUBJ	A VAL	B VAL	A-B	080 -	ORD +	N	N -	N +
S-3 K-1 D-1 R-2 F-2 G-2 M11 M13 M-2 G-3 M10	3.68 4.87 4.49 3.64 4.14 3.30 4.31 3.49 3.71 1.54 1.49 5.70	5.06 5.44 6.50 4.80 5.73 6.74 4.20 7.52	-1.38 -0.57 -2.01 -1.18 -0.943 -0.532 -0.552 -1.82	-0.25 -0.52 -0.53 -0.57 -0.94 -1.06 -1.18 -1.38 -1.82 -2.01 -2.36 -2.43	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00	1.00 2.00 3.00 4.05 5.00 6.00 7.00 8.00 9.00 10.00	

mendam spe

3.70 STD DEV A: 1.22 4.95 STD DEV B: 1.62

SUM OF N MINUS: 78.00 ------SUM OF N PLUS: ----- 0.00

*** SIGNIFICANT DIFFERENCE ***

		-						
ANALTS15	Of:	CHES	1 51					
FUNCTION FUNCTION	A = G: B = G:	10 10	CELL:	0 r			MAX MAX	
SUBJ	A VAL	B VAL	A-8	080 -	08D +	N	N -	N +
S-3 K-1 O-1 R-2 F-3 G-2 F-2 H11 H13 H-2 G-3 H10	36.05 39.32 31.04 17.31 29.83 22.62 33.20 39.30 42.59 37.20 29.44 31.53	8 VAL 39.10 43.95 41.85 26.18 43.84 45.69 45.69 47.12 42.89 37.63	-3.05 -4.63 -10.81 -8.87 -14.01 -15.02 -12.55 -3.39 -9.92 -13.45 -6.10	0.00 -3.05 -3.39 -4.63 -6.10 -8.87 -9.92 -10.81 -12.55 -13.45 -14.01 -15.02	1.59 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00	0.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00	1.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
MEAN A: MEAN B:	32. 45 40.80	STD DE STD DE	v A: v B:	7.25 5.47	SUM OF N	MINUS: PLUS:	77.00	1.00
					MMM SIG	NIFICANT	DIFFEREN	40E PHH
HILCOXON		-	-					
		HEAD		_				
FUNCTION FUNCTION	A = G: 8 = G:	10 10	CELL:	D F			MAX	
SUBJ	A VAL	8 VAL	A-8	080 -	080 +	N	N -	N +
S-3 K-1 O-1 R-2 F-3 G-2 F+2 M11 M13 M-3 M10	13.34 11.77 12.47 12.55 12.66 13.41 14.40 12.39 11.62 11.85	8 VAL 14.55 13.33 13.68 13.95 15.93 15.14 15.39 16.03 16.37 12.72 13.28 17.32	-1.26 -1.36 -1.40 -3.648 -1.638 -1.638 -0.93 -1.43	-0.90 -1.21 -1.21 -1.40 -1.43 -1.56 -1.63 -1.98 -2.48 -3.13 -3.38	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.00 2.50 4.00 5.00 7.00 8.00 9.00 10.00 11.00	1.00 2.50 ,2.50 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
MEAN A: MEAN B:	12.81 14.81	STD DE	V A: V B:	0.88 1.44	SUM OF N	MINUS: PLUS:	78.00	0.00

SIGNIFICANT DIFFERENCE

ANALYSIS OF:

HEAD RES

EUNCTION (0	CELL: D			989 889		
FUNCTION FUNCTION	B = G: 1	0	CELL: 1	080 -	ORD +	N	N -	N +
S-3 K-1 D-1 F-3 G-2 F12 M13 M-2 G-3 M10	13.74 11.84 12.57 12.60 12.78 12.72 13.69 14.84 13.59 11.91 11.91	8 VAL 14.66 13.53 14.56 14.71 17.07 15.16 15.45 16.09 17.18 12.73 13.43 17.36	-0.92 -1.69 -1.99 -1.29 -1.29 -1.25 -3.59 -3.59 -3.52 -1.52 -2.93	-0.82 -0.92 -1.25 -1.52 -1.61 -1.69 -1.76 -1.99 -2.44 -2.93 -3.59 -4.29	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00	1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
MEAN A: MEAN B:	13.05	STO DEV	9: 8:	1.00 1.55	SUM OF N SUM OF N MMR SIGN	PLUS: -		0.00 ××× 3
ANALYSIS	. n = 6.	HEAD 10	CELL:	D F		A A	RS	
ANALYSIS	: : : : : : : : : : : : : : : : : : :	HEAD 10	CELL:	D F 0AD -	040 +	A	RS	N +
ANALYSIS FUNCTION FUNCTION SUBJ 5-3 K-1 D-1 A-2 F-3 G-2 F-2 M11 M13 M-2 G-3 M10	G UF: A P = G: A VAL 20.94 18.54 20.74 19.79 18.56 21.22 23.10 18.60 19.25 20.05 22.43	HEAD 10 B VAL 29.53 28.22	CELL: R-B -8.95 -7.48 -7.48 -8.19 -8.23 -0.42 -5.18	-0.02 -2.52 -4.79 -5.18 -5.95 -7.42 -7.48 -8.21 -8.23 -8.47 -8.59	040 + 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	N 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 11.00 12.00	N - 1.00 2.00 3.60 4.00 5.00 6.00 7.00 8.10 9.00 10.00 11.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0

WILCOXON GNALYS.3

ANALYSIS	OF:	TOTAL	SHOUL	DER				
FUNCTION FUNCTION		10 10					IAX IAX	
5-3 K-1 D-1 R-2 F-3 G-2 H11 H13 H-3 G-3	182.50 199.08 171.12 223.22 267.89 149.99 223.05 197.59 168.66 225.05	161.07 93.66 143.23 122.27 104.22 120.77 120.66 164.33 210.05		0.00 0.00 0.00 0.00 0.00 0.00 0.00	27.72 39.34 43.28 48.00 51.62 51.86 60.72 76.82 118.83 124.66	1.00 2.00 3.00 4.00 5.00 6.00 8.00 9.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00 5.00 6.00 9.00 10.00 11.00
MEAN A: MEAN B: WILCOXON	137.40	SID DEV	A: 8:	38.37 32.58	SUM OF N N SUM OF N N MMM SIGN	`LUS :		78.00 NCE +××

ANALY515	OF:	TOTAL LAP			
FUNCTION FUNCTION			-		MAX MAX
SUBJ	A VAL	B VAL A-B	080 -	ORD + N	N - N +
M-2 G-3	100.13 115.72 90.94 82.72 135.46 80.19 102.43 80.59 70.05 103.92 97.58 86.44	86.97 13.16 138.23 -22.51 125.18 -34.24 96.61 -13.89 103.87 31.59 113.47 -33.28 166.90 -64.47 77.76 -1.71 133.66 -29.74 149.46 -51.88 108.53 -22.09	-6.77 0.00 -13.89 -22.09 -22.51 -29.74 0.00 -33.28 -34.24 -51.86	0.00 2. 3.16 3. 0.00 4. 0.00 5. 0.00 6.	00 0.00 3.00 00 4.00 0.00 00 5.00 0.00 00 6.00 0.00 00 7.00 0.00 00 9.00 0.00 00 9.00 0.00 00 10.00 0.00 00 11.00 0.00
MEAN A: MEAN B:	96.01 115.67		17.18 27.49	SUM OF N MINUSUM OF N PLUS	: 11.00

1111112121	S OF:	101AL	SERT X				
FUNCTION FUNCTION	V A ± G: N B = G:	10 10	CELL: D CELL: F			11N 11N	
\$UBJ 5-3 K-1 B-2 F-3 G-2 F-2 M11 M13 M-2 G-3	8 VAL -312.67 -355.24 -234.66 -105.70 -238.38 -157.80 -332.76 -305.53 -368.71 -235.05 -229.75	B VAL -341.27 -357.27 -283.79 -198.16 -322.95 -221.80 -322.95 -310.90 -430.57 -314.03 -275.11	A-B ORD - 28.60 0.00 2.03 0.00 12.45 0.00 84.55 0.00 64.09 0.00 29.80 0.00 5.37 0.00 61.86 0.00 79.03 0.00 45.36 0.00 18.26 0.00	08D + 2.03 5.37 12.46 18.26 28.60 29.80 45.36 49.13 61.86 64.09 79.03	N 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 11.00	N - 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	N + 1.00 2.00 3.00 4.00 5.00 6.00 7.00 8.00 9.00 11.00
MEAN A:	-260.68 269.08	5TD DEV	18.26 0.00 	84.55 SUM OF N	12.00 MINUS:	0.00	12.00
MEHN B:	-308.12	\$10 DEA		NAN SIGN			
KILCOXO	N ANALYSIS	5					
01121 761		- 3010	6501.7				
		- TOTAL 10			м	ınx	
FUNCTION STATE	NA = G:	10	CELL: D			In v	
FUNCTION STATE	NA = G:	10		080 + 0.00 0.00 0.00 0.00 0.00 127.81 0.00 0.00 0.00 0.00		In v	N +

NWN SIGNIFICANT DIFFERENCE PHH

RNALYSI	5 OF:	RES	SEAT FOR	CÉ				
	N A = G: N B = G:		CELL:				MAX MAX	
		B VAL		ORD -	08D +	N	N -	N +
G-2 F-2 M11 M13	1811.34 2010.67 2169.89 1578.73 1534.18 1354.76 1667.59 1779.36 1706.49 1711.98 1711.49 1607.30		-133.93 -201.17 -122.56 53.45 -223.54 1:6.18 -169.10 -36.39 -270.76 -148.90 -52.97 -15.16	-36.39 -52.97 0.00 -122.56 -133.93 -148.90 -169.10 -201.17 -223.34	0.00 0.00 0.00 53.45 116.18 0.00 0.00 0.00 0.00	1.00 2.00 3.00 4.00	1.00 3.00 0.00 0.00 6.00 7.00 8.00 9.00 10.00	0.000 0.000 5.000 0.000 0.000 0.000
MERN A: MERN B:	1720.32 1820.70			13.71 84.45	SUM OF N		59.00	9.00

*** SIGNIFICANT DIFFERENCE ***

APPENDIX D

SUMMARY OF PHOTOMETRIC DATA

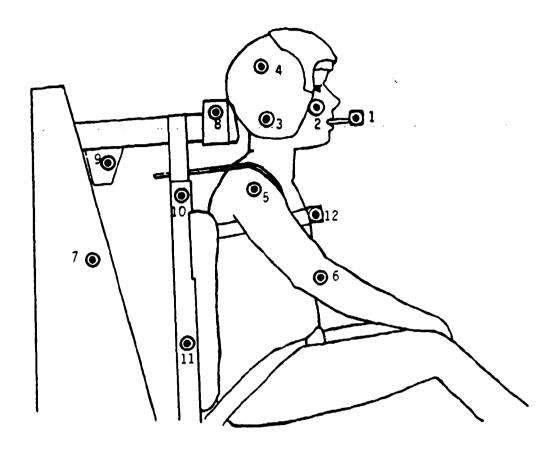
The photometric data obtained from this test program were analyzed to characterize the motions of photometric targets (fiducials) fixed to the test subject and thus describe the subject's dynamic response to impact. Reduction of the film data included digitization of target position information and computer plotting of the position-time, velocity-time, and acceleration-time history of each fiducial.

Fiducials were placed on subjects and the test fixture in accordance with the guidelines provided in "Film Analysis Guide for Dynamic Studies of Test Subjects" (SAE J138, March 1980). The positions of subject-mounted fiducials relative to reference fixture-mounted fiducials were documented for each subject prior to each test. The locations and number designations of each fiducial are shown in Figures D-1 and D-2. The distance between the "mouth pack" target (Target No. 1 in Figure D-1) and the center of the triaxial accelerometer in the mouth was four inches.

The photometric data were obtained by three 16 mm Milliken cameras, two mounted on the test carriage and one mounted off the carriage. The off-board camera and one on-board camera were positioned to provide a frontal view of the subject and the other on-board camera was positioned to provide a right lateral view of the subject. Each camera lens had a focal length of 10 mm. During the impact, the cameras were operated at 500 frames/sec.

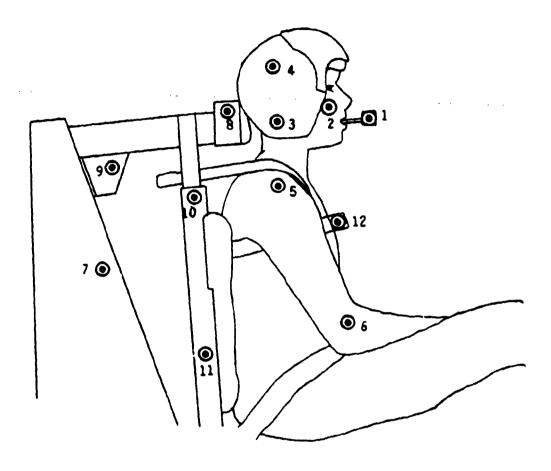
The Photo Digitizing Systems Model 200 processor consists of an Automatic Film Reader (AFR), an electronic scanning camera, and a Data General Corporation (DGC) Nova 3/12 computer. This system was utilized for target position digitization. The semi-automatic ARF is manually initialized by selecting, with a cursor, targets of interest in the first frame of data. Targets on subsequent frames are automatically scanned, acquired, and identified. The target coordinates are then digitized by the Nova computer and the digitized data are then stored on magnetic tape. The coordinate resolution of the ARF is 0.025% of the major film dimension.

These digitized data were then processed on the Control Data Corporation (CDC) Cyber 74 computer system. The computer analysis routine used to process the film data has been described elsewhere (Graf et al., 1978; Brinkley et al., 1981). The program permitted the graphic presentation of position-time, velocity-time, and acceleration-time histories of fiducials and abscissaordinate position histories as well. Typical graphic data from one cell of the experimental matrix are presented. In addition, the maximum vertical and horizontal displacements measured at the head and helmet are presented in Table D-1. As previously noted, data were not available for all tests conducted.



- Mouth Pack
- Cheek
- 3. Lower Helmet
- Upper Helmet
 Shoulder
- 6. Elbow
- Upper Frame
- 8. Front Headrest
- 9. Rear Headrest
- 10. Upper Seat Back 11. Lower Seat Back
- 12. Chest Pack

Figure D-1. Location of Fiducials for Hands-On-Knees Position.



- Mouth Pack 2. Cheek
- 7. Upper Frame
- Lower Helmet
- 8. Front Headrest Rear Headrest 9.
- Upper Helmet
- 10. Upper Seat Back
- 5. 6. Shoulder
- 11. Lower Seat Back 12. Chest Pack
- Elbow

Figure D-2. Location of Fiducials for Hands-In-Lap Position.

TABLE D-1

MAXIMUM HORIZONTAL AND VERTICAL DISPLACEMENTS (INCHES)
MEASURED AT THE HEAD AND HELMET FIDUCIALS

	OF MATRIX	A		B	
SUBJ	FIDUCIAL LOCATION	XMAX	ZMAX	XMAX	ZMAX
D-1	Cheek	1.69	1.66	0.46	1.37
	Upper Helmet	1.40	1.49	0.84	1.55
	Lower Helmet	1.60	1.39	0.51	1.62
E-1	Cheek Upper Helmet Lower Helmet				
F-3	Cheek	1.49	1.88	0.43	1.77
	Upper Helmet	1.15	2.60	0.32	2.52
	Lower Helmet	1.49	2.41	1.20	2.59
F-2	Cheek	1.06	1.66	0.86	1.63
	Upper Helmet	1.46	1.30	0.69	1.79
	Lower Helmet	1.15	1.34	1.05	1.69
G-3	Cheek Upper Helmet Lower Helmet			0.94 0.64 1.24	1.64 3.20 2.87
G-2	Cheek	1.43	2.29	1.34	2.02
	Upper Helmet	2.04	2.09	1.65	2.15
	Lower Helmet	1.59	2.00	1.22	2.22
K-1	Cheek	1.74	1.99	1.07	1.89
	Upper Helmet	2.91	1.71	1.31	1.68
	Lower Helmet	2.03	1.71	1.20	1.81
M-2	Cheek Upper Helmet Lower Helmet				
M10	Cheek	1.05	1.75	0.56	1.55
	Upper Helmet	0.95	1.13	0.37	1.81
	Lower Helmet	1.19	1.38	0.72	1.63
M11	Cheek	2.20	2.40	1.17	1.87
	Upper Helmet	3.04	1.75	1.01	2.31
	Lower Helmet	2.08	1.94	1.14	2.23
M13	Cheek	0.57	1.84	0.71	1.78
	Upper Helmet	0.50	2.42	0.68	2.50
	Lower Helmet	0.70	2.35	0.48	2.26
R-2	Cheek	1.56	2.10	0.90	1.60
	Upper Helmet	3.13	1.20	0.92	1.18
	Lower Helmet	2.06	1.39	1.12	1.36
R-3	Cheek Upper Helmet Lower Helmet				
S-3	Cheek	1.63	2.01	0.66	1.61
	Upper Helmet	1.82	2.01	0.28	2.31
	Lower Helmet	1.43	1.92	0.63	2.16

TABLE D-1 (continued)

MAXIMUM HORIZONTAL AND VERTICAL DISPLACEMENTS (INCHES)

MEASURED AT THE HEAD AND HELMET FIDUCIALS

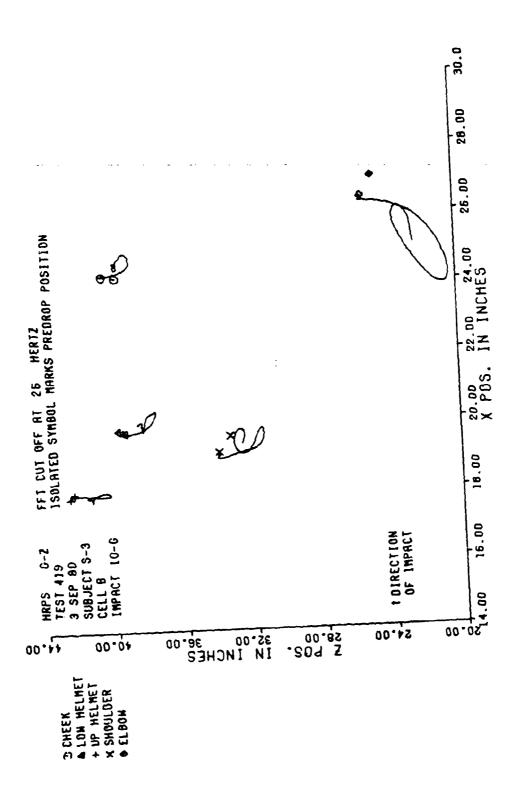
	OF MATRIX			D		
SUBJ	FIDUCIAL LOCATION	XMAX	ZMAX	XAMX	ZMAX	
	Cheek	0.98	1.35	0.40	1.51	
D-1	Upper Helmet	0.71	1.08	0.63	1.70	
j	Lower Helmet	1.04	0.94	0.55	1.66	
	Cheek	7		3.31	2.55	
E-1	Upper Helmet			4.64	2.61	
1	Lower Helmet	_1		3.56	2.66	
	Cheek	1.01	1.67	[
F-3	Upper H elme t	0.78	1.98			
	Lower Helmet	0.93	1.81			
	Cheek			0.76	1.86	
F-2	Upper Helmet	1		0.59	2.33	
	Lower Helmet		1	0.71	2.25	
	Cheek	1		1.11	1.80	
G-3	Upper Helmet	1		0.92	3.02	
	Lower Helmet			1.10	2.78	
_	Cheek	2.82	3.41	2.54	2.69	
G-2	Upper Helmet	5.03	2.28	4.18	1.94	
	Lower Helmet	3.58	2.42	2.73	2.09	
	Cheek	3.64	3.85	2.73	2.46	
K-1	Upper Helmet	6.30	3.08	3.62	2.63	
	Lower Helmet	4.87	2.21	3.07	2.87	
	Cheek	3.23	4.71			
M-2	Upper Helmet	6.59	3.63			
	Lower Helmet	4.86	2.44	0.40	1 (3	
	Cheek	1.24	1.61	0.42	1.63 1.93	
M10	Upper Helmet	1.24	1.65	0.59	1.93	
	Lower Helmet	1.24	1.69	0.66	2.07	
447.1	Cheek	1.75	2.09	0.95		
MI1	Upper Helmet	2.52	2.29	0.84	2.46	
	Lower Helmet	1.63 2.89	2.14 3.55	0.85 0.99	2.36 1.75	
M13	Cheek Upper Helmet	5.01	2.17	0.99	2.26	
LI12	Lower Helmet	3.80	2.19	1.03	2,20	
	Cheek	- 3.80	4.17	0.84	1.58	
R-2	Upper Helmet	ł		0.86	1.61	
N-2	Lower Helmet		<u>}</u>	0.96	1.63	
	Cheek	1.98	2.30	0.90	1.05	
R-3	Upper Helmet	3.60	1.89			
1,-0	Lower Helmet	2.50	1.63	1		
	Cheek	⊣ '''"	1.05	0.73	1.65	
S - 3	Upper Helmet		}	0.92	2.72	
J - J	Lower Helmet	1	ł	0.51	2.40	

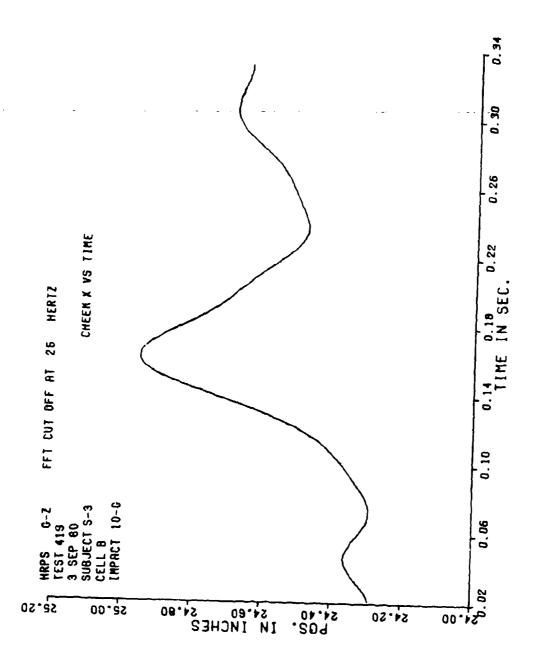
TABLE D-1 (continued)

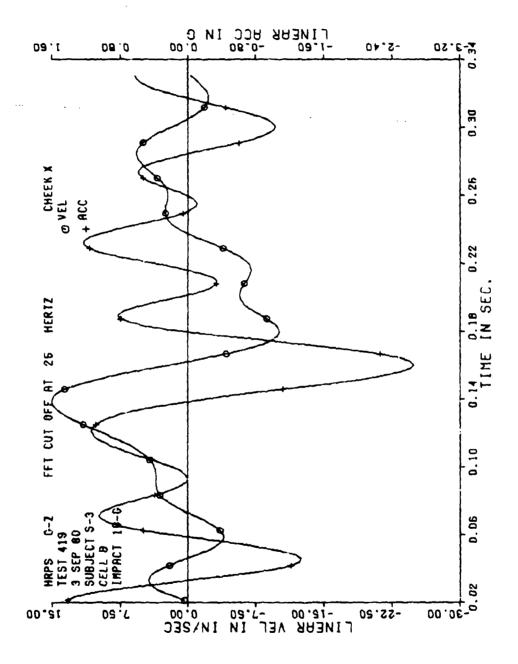
MAXIMUM HORIZONTAL AND VERTICAL DISPLACEMENTS (INCHES)

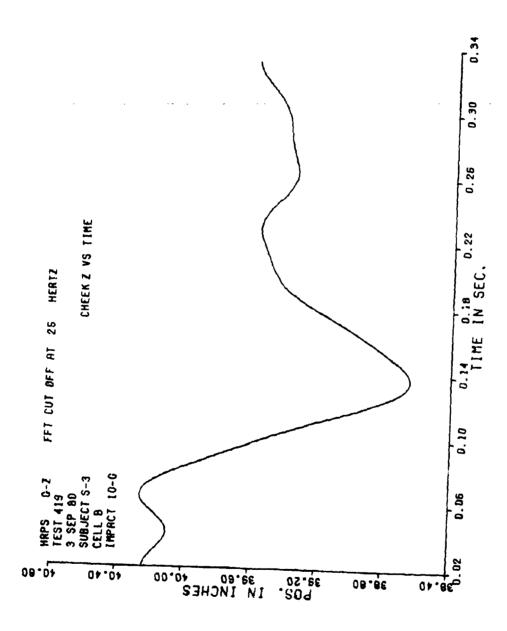
MEASURED AT THE HEAD AND HELMET FIDUCIALS

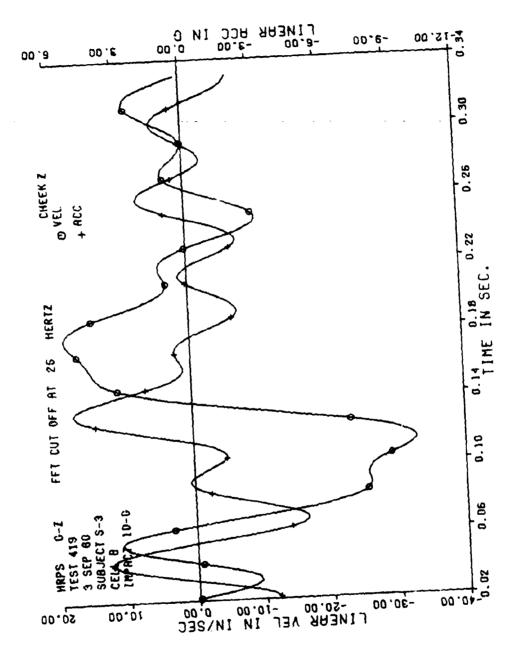
CELL	OF MATRIX	E	·		
SUBJ	FIDUCIAL LOCATION	XMAX	ZMAX	X _{MAX}	ZMAX
D-1	Cheek	1.53	2.15	1.06	1.61
	Upper Helmet	0.86	2.12	0.59	2.13
	Lower Helmet	1.32	2.11	0.75	2.09
E-1	Cheek Upper Helmet Lower Helmet	_			
F-3	Cheek	1.42	2.53	1.44	2.29
	Upper Helmet	1.92	3.10	1.70	3.95
	Lower Helmet	1.74	2.85	1.28	3.33
F-2	Cheek	1.42	2.79	0.78	1.83
	Upper Helmet	1.77	2.78	0.52	2.30
	Lower Helmet	1.48	2.83	0.94	2.08
G-3	Cheek Upper Helmet Lower Helmet			1.58 1.12 2.22	2.50 4.71 4.10
G-2	Cheek	1.39	2.00	1.67	2.68
	Upper Helmet	2.26	1.46	3.09	2.12
	Lower Helmet	1.79	1.43	2.29	2.04
K-1	Cheek Upper Helmet Lower Helmet			3.19 4.12 3.46	2.80 2.92 2.98
M-2	Cheek Upper Helmet Lower Helmet				
M10	Cheek	1.22	2.30	0.47	2.21
	Upper Helmet	1.58	2.08	0.47	2.92
	Lower Helmet	1.16	2.37	0.71	2.84
M11	Cheek	1.71	2.20	0.78	2.19
	Upper Helmet	2.45	2.92	0.61	2.91
	Lower Helmet	1.53	2.60	1.13	2.69
M13	Cheek	1.39	2.58	1.30	1.72
	Upper Helmet	2.46	2.23	0.96	2.88
	Lower Helmet	1.48	2.19	1.17	2.56
R-2	Cheek	2.16	2.81	0.72	1.98
	Upper Helmet	4.34	1.58	0.61	3.23
	Lower Helmet	2.97	2.08	1.44	2.87
R-3	Cheek Upper Helmet Lower Helmet				
5-3	Cheek Upper Helmet Lower Helmet	1.67 1.85 1.35	2.22 2.91 2.76		

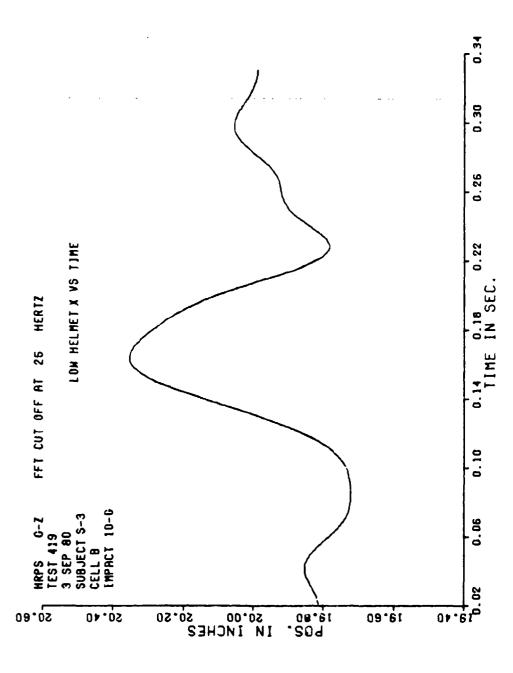






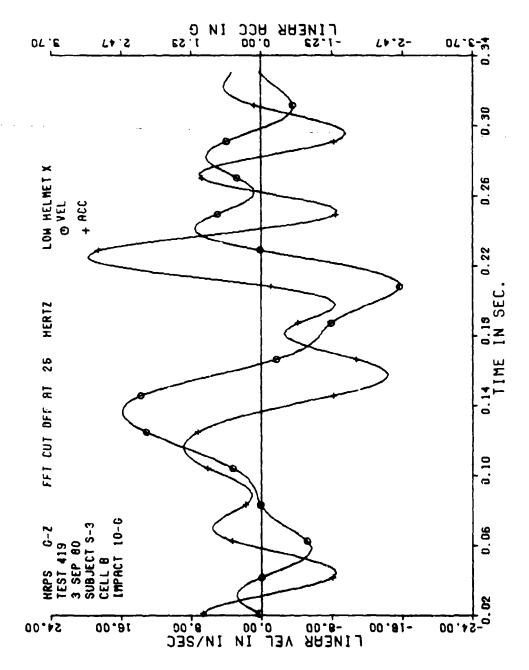


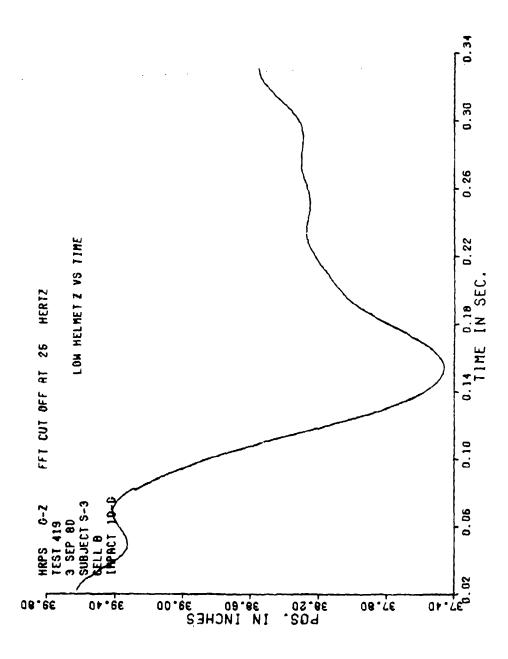




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